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# COLLOCATION FLUTTER ANALYSIS STUDY II

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VOLUME II

UNSTEADY AERODYNAMIC GENERALIZED FORCE  
PROGRAMS FOR SUBSONIC, TRANSONIC, AND SUPERSONIC FLIGHT REGIMES

APRIL 1970



MISSILE SYSTEMS DIVISION



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COLLOCATION FLUTTER ANALYSIS STUDY II

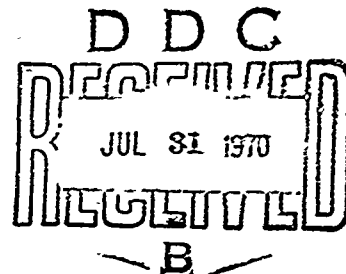
VOLUME II  
UNSTEADY AERODYNAMIC GENERALIZED FORCE PROGRAMS  
FOR SUBSONIC, TRANSONIC, AND SUPERSONIC FLIGHT REGIMES

PREPARED BY DYNAMICS & ENVIRONMENTS SECTION PERSONNEL, HUGHES  
AIRCRAFT COMPANY, MISSILE SYSTEMS DIVISION, CONTRACT NO. 00019-69-C-0427

APRIL 1970

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*Wash, D.C. 20360*



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## 1.0 INTRODUCTION

The flutter problem can be solved with either a collocation or normal-mode formulation. The collocation approach is attractive if an accurate stiffness and aerodynamic influence coefficient matrix can be formed for the system. The normal-mode method merits consideration when mode shapes and natural frequencies for the structure are known. The normal-mode method requires the aerodynamics to be presented as generalized forces. The normal-mode formulation is generally presented in the following manner

$$([\bar{M}] + [\bar{Q}] - \frac{1+ig}{\omega^2} [\omega_n^2] [\bar{M}]) \{\psi\} = 0$$

Where

$[\bar{M}]$  = Generalized Mass Matrix

$[\bar{Q}]$  = Generalized Aerodynamic Force Matrix

$g$  = Artificial Structural Damping

$i$  =  $\sqrt{-1}$

$\omega$  = Flutter Frequency

$\omega_n$  = Natural Vibration Frequency

$\psi$  = Generalized Coordinate

This volume presents three computer programs that calculate the generalized aerodynamic forces for the three flight regimes: Subsonic Flight, Transonic Flight, Supersonic Flight and may be used with the Modal Flutter Analysis Program of Vol. III. The subsonic program is based upon Kernel Function formulation. The transonic and supersonic programs are based upon the Mach Box technique.

## 2.0 UNSTEADY AERODYNAMIC GENERALIZED FORCES

The generalized force  $Q_{ij}$  is defined as the work done in mode  $i$  by the pressures due to motion of mode  $j$ . If  $z^i(x,y)$  is the deformation pattern of mode  $i$  and  $\Delta P_j(x,y)$  is the pressure distribution of mode  $j$  then

$$Q_{ij} = \int \int z^i(x,y) \Delta P_j(x,y) dx dy \quad 2.0.1$$

Oscillation of a lifting surface creates a phase lead (or lag) between the pressure and motion of the surface thereby making  $Q_{ij}$  a complex quantity.

The frequency dependency of the generalized force makes the flutter solution a trial and error procedure. Different frequencies must be tried until the flutter frequency and the generalized force frequency coincides. Fortunately, the flutter frequencies are usually near the natural frequencies. This is especially true for a stable structure with modes which remain fairly uncoupled; there is little drifting of oscillatory frequencies with the presence of aerodynamic forces.

Various lifting surface theories were employed to determine the pressure distribution  $\Delta P_j(x,y)$  for generalized force calculations. This was required to correctly account for the high degree of chordwise and spanwise deformation associated with mode shapes of low aspect ratio surfaces. Also, it was necessary to include aerodynamic interaction effects between tandem surfaces.

The methods are based on the linearized equation of fluid motion which describe the flow patterns for a compressible, inviscid, isentropic and irrotational fluid. The boundary conditions are consistent with thin wing theory. The effects of high angles of attack and missile body influence on the aerodynamics of the lifting surfaces were not considered in the analysis.

The linearized equation for time dependent disturbances is

$$\bar{\phi}_{XX} + \bar{\phi}_{YY} + \bar{\phi}_{ZZ} = M^2 \left( \bar{\phi}_{XX} + \frac{2}{U} \bar{\phi}_{XT} + \frac{1}{U} \bar{\phi}_{TT} \right) \quad 2.0.2$$

where  $\bar{\phi}$  is the perturbation velocity potential at the point  $(X, Y, Z)$ .  $M$  and  $U$  are the free stream Mach number and velocity, respectively. Imposing the requirement of harmonic motion, this time dependency can be expressed as

$$\bar{\phi} = b \phi e^{i\omega t}$$

where  $\phi$  is the nondimensional complex amplitude of the velocity potential and  $b$  is a reference semi-chord. The equation may be cast in a nondimensional form by substitution of the following dimensionless parameters:

$$x = X/b$$

$$y = Y/b$$

$$z = Z/b$$

$$k = \omega b/U$$

This yields

$$\phi_{xx} + \phi_{yy} + \phi_{zz} = M^2 (\phi_{xx} + 2ik \phi_x - k^2 \phi) \quad 2.0.3$$

It is this relationship which must be satisfied for  $M < 1$ ,  $M = 1$ , and  $M > 1$ . A brief description of the analytical techniques employed for each speed regime is presented in the following sections. The numerical and computational schemes used are similar to those which are described in detail in References 5, 6, and 7.

### 3.0 SUBSONIC UNSTEADY AERODYNAMICS PROGRAM

#### 3.1 Theoretical Derivation

Subsonic aerodynamic loads were derived by the kernel function method and the resulting loads were then used to compute generalized forces. The subsonic kernel function relationship for the downwash  $w(x,y)$  on a surface in terms of the pressure over the entire surface is

$$w(x,y) = -\frac{1}{8\pi} \iint \frac{\Delta P}{1/2\rho U^2} K(x-\xi, y-\eta) d\xi d\eta \quad 3.1.1$$

This relationship is derived by noting that the potential equation for subsonic flow,

$$(1-M^2)\phi_{xx} + \phi_{yy} + \phi_{zz} = M^2 (2ik\phi_x - k^2\phi) \quad 3.1.2$$

is satisfied at  $(x,y,z)$  by the pulsating pressure doublet

$$\phi = -A \frac{\partial}{\partial \xi} e^{-ik(x-\xi)} \int_{-\infty}^{x-\xi} \frac{1}{R'} \exp \left[ \frac{ik}{1-M^2} (\lambda - MR') \right] d\lambda \quad 3.1.3$$

where

$$R' = \sqrt{\lambda^2 + (1-M^2)(y-\eta)^2 + (z-\xi)^2} \quad 3.1.4$$

and the pressure doublet strength is given by

$$A = \frac{1}{4\pi} \left[ \frac{\Delta P(\xi, \eta)}{1/2\rho U^2} \right] d\xi d\eta \quad 3.1.5$$

The velocity normal to the lifting surface is given by

$$w(x,y) = \lim_{z \rightarrow 0} \frac{\partial \phi}{\partial z} \quad 3.1.6$$

Substituting equation (3.1.3) into the equation above and integrating over the area yields the kernel function relationship, equation (3.1.1). For tandem surfaces, the integration extends over both surfaces:

$$w(x,y) = -\frac{1}{8\pi} \int_{-s}^{+s} \int_{1.e.}^{t.e.} \frac{\Delta P_{W(\xi, \eta)}}{1/2\rho U^2} K(x-\xi, y-\eta) d\xi d\eta$$

wing

$$-\frac{1}{8\pi} \int_{-s}^{+s} \int_{1.e.}^{t.e.} \frac{\Delta P_{cs(\xi, \eta)}}{1/2\rho U^2} K(x-\xi, y-\eta) d\xi d\eta$$

control surface

3.1.7



The kernel function at any point is given by

$$K(x-\xi, y-\eta) = \lim_{\substack{\zeta \rightarrow 0 \\ z \rightarrow 0}} \left( e^{-ik(x-\xi)} \frac{\partial}{\partial z} \frac{\partial}{\partial \zeta} \int_{-\infty}^{x-\xi} \frac{1}{R^3} e^{i \left[ \frac{1}{1-M^2} (\lambda - MR') \right]} d\lambda \right) \quad (3.1.8)$$

Equation (3.1.7) then represents the integral equation wherein given the downwash  $w(x,y)$  over the wing and control surface,  $\Delta P_w$  and  $\Delta P_{cs}$  must then be determined.

The pressure distribution is approximated as the sum of a series of functions which have the proper behavior as inferred from steady state and two-dimensional solutions. The pressure on each surface can be approximated in the form

$$\Delta P \approx \frac{1}{2} \rho U^2 \frac{\sqrt{s^2 - \eta^2}}{b(\eta)} \sum_{n=0}^N \sum_{m=0}^M a_{nm} P_m(\eta) f_n(\bar{\xi}) \quad (3.1.9)$$

where

$$f_0(\bar{\xi}) = \sqrt{\frac{1 - \bar{\xi}}{1 + \bar{\xi}}} \quad f_n(\bar{\xi}) = \sqrt{1 - \bar{\xi}^2} T_{n-1}(\bar{\xi}); \quad n \geq 1$$

$$P_0(\eta) = 1.0 \quad P_m(\eta) = \eta^2 T_{m-1}(\eta); \quad m \geq 1 \quad (3.1.10)$$

$$T_0(x) = 1.0$$

$$T_1(x) = 2x$$

$$T_k(x) = 2xT_{k-1}(x) - T_{k-2}(x); \quad k \geq 2$$

$$\bar{\xi} = \frac{\xi - \bar{\xi}}{b(\eta)}$$

$$\bar{\xi} = 1/2 (\xi_{l.e.} + \xi_{t.e.})$$

$$\bar{\eta} = \frac{\eta}{s}$$

s is the starboard coordinate of the surface tip and b ( $\eta$ ) is the local semi-chord. The functions  $T_n$  are Chebyshev polynomials and are introduced for purposes of convenience.

Substituting equation (3.1.8, 3.1.9, and 3.1.10) into equation (3.1.7) yields a set of equations relating the pressure coefficients for the wing,  $a_{nm}^w$ , and the control surface,  $a_{nm}^{cs}$ , to the downwashes. In matrix notation this gives

$$\begin{Bmatrix} \{w\} \\ \{w^{cs}\} \end{Bmatrix} = \begin{bmatrix} D_{nm}^{ww} & D_{nm}^{w-cs} \\ D_{nm}^{cs-w} & D_{nm}^{cs} \end{bmatrix} \times \begin{Bmatrix} a_{nm}^w \\ a_{nm}^{cs} \end{Bmatrix} \quad (3.3.11)$$

The integrals involved in evaluating the D's were solved by the methods of Hsu (Reference 5). In this procedure the integrals are numerically evaluated using the Gauss-Mehler quadrature. Upon determining values for the D's, the pressure coefficients are found by direct inversion and the generalized forces are found by application of equation (2.0.1).

### 3.2 Program Description.

The Subsonic Generalized Force Unsteady Aerodynamics Program calculates generalized forces for up to 10 deformation modes. The computer solution, which is based upon the kernel function formulation, is applicable to a variety of configurations. The various configurations which can be analyzed are shown in Figure 3.2.1 and Table 3.2.2. The analysis includes interaction effects between tandem surfaces and wake effects on the trailing surface. The number of integration stations are chosen, and they are automatically located. The collocation stations are then interdigitated between the integration stations, according to Hsu (Reference 5), internally in the program. The solutions at the collocation stations are then matched to terms in the downwash series by a least squares method and the surface pressure are determined. The method of solution programmed does not allow for a single surface to be analyzed separately; however, an option to isolate and eliminate interference effects between the two surfaces is available. Thus, a single surface can be analyzed by using the option ISOLAT and inputting a dummy second surface.

The solution for the generalized aerodynamic forces requires the input of the deformation modes due to vibration. The program considers the modes to be expressed as analytic functions of the form:

$$w(x, y) = \sum_{m=0}^N \sum_{n=0}^m C_{(n-m), m} x^{(n-m)} y^m$$

To meet this requirement only the coefficients "c" are required as input into the program. These coefficients can be obtained in several ways, the most common way is to surface fit the modes by the least-square technique.

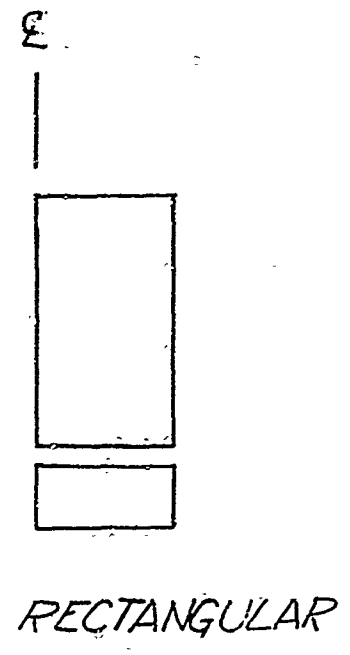
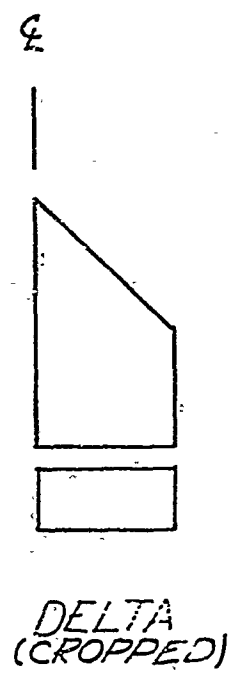
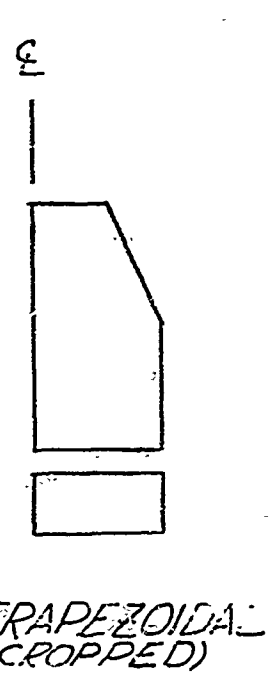
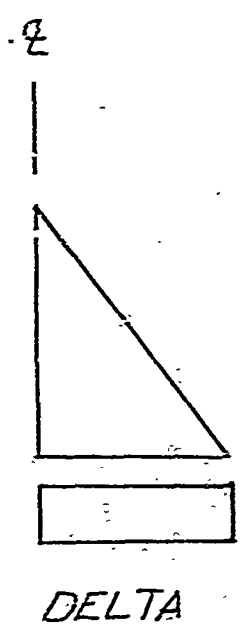
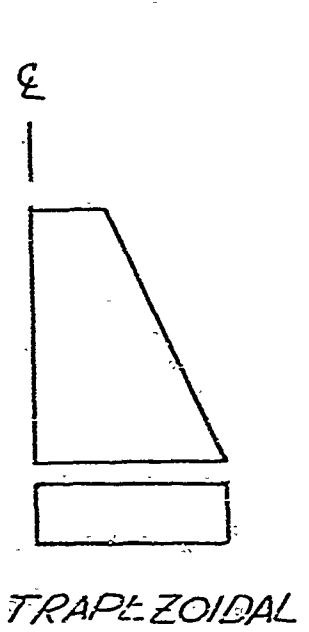


FIGURE 3.2.1  
TANDEM COPLANAR CONFIGURATIONS AT SUBSONIC  
MACH NUMBER

TABLE 3.2.2 - OPTIONAL CONFIGURATIONS

Configuration	Chordwise Coordinates	Spanwise Coordinates
Rectangular	$X(1) = 0.0$ $X(2) = 0.0$ $X(3) > 0.0$ $X(4) > X(3)$ $X(5) > X(4)$	$Y(1) = 0.0$ $Y(2) = 0.0$ $Y(3) > 0.0$
Delta	$X(1) = 0.0$ $X(2) > 0.0$ $X(3) = X(2)$ $X(4) > X(3)$ $X(5) > X(4)$	$Y(1) > 0.0$ $Y(2) = 0.0$ $Y(3) > 0.0$
Trapezoidal	$X(1) = 0.0$ $X(2) > 0.0$ $X(3) = X(2)$ $X(4) > X(3)$ $X(5) > X(4)$	$Y(1) = 0.0$ $Y(2) > 0.0$ $Y(3) > Y(2)$
Trapezoidal (Cropped)	$X(1) = 0.0$ $X(2) > X(1)$ $X(3) > X(2)$ $X(4) > X(3)$ $X(5) > X(4)$	$Y(1) = 0.0$ $Y(2) > 0.0$ $Y(3) > Y(2)$
Delta (Cropped)	$X(1) = 0.0$ $X(2) > 0.0$ $X(3) > X(2)$ $X(4) > X(3)$ $X(5) > X(4)$	$Y(1) = 0.0$ $Y(2) = 0.0$ $Y(3) > Y(2)$

### 3.3 INPUT INSTRUCTIONS

Instructions for preparing input data for the subsonic computer program are presented here. The field location and format for each input quantity is specified. Any set of units may be used for geometric dimensions and acoustic velocity as long as they are consistent, e.g., if feet is used for length then the acoustic velocity must have dimensions of feet per second.

#### 1. Streamwise Coordinates (6E12.5 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	X(1)	X(2)	X(3)	X(4)	X(5)	
Item	(1)	(2)	(3)	(4)	(5)	

- (1) X(1) Wing root leading edge streamwise coordinate (See Figure 3.3.1)
- (2) X(2) Wing tip leading edge streamwise coordinate
- (3) X(3) Wing trailing edge streamwise coordinate
- (4) X(4) Control surface leading edge streamwise coordinate
- (5) X(5) Control surface trailing edge streamwise coordinate

The technique for generating various configurations is shown in Table 3.2.1

The origin for the planform and AIC station coordinates must be at the leading edge root of the wing therefore X(1) and Y(1), described below, must always be 0.0.

#### 2. Spanwise Coordinates and Acoustic Velocity (6E12.5 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	Y(1)	Y(2)	Y(3)	SOUND	RHO	
Item	(1)	(2)	(3)	(4)	(5)	

- (1) Y(1) Wing root spanwise coordinate
- (2) Y(2) Wing leading edge spanwise coordinate
- (3) Y(3) Wing (and control surface) tip spanwise coordinate
- (4) SOUND Acoustic velocity for altitude at which analysis is performed
- (5) RHO density of fluid  $\times 1000.0$  (M/L<sup>3</sup>)

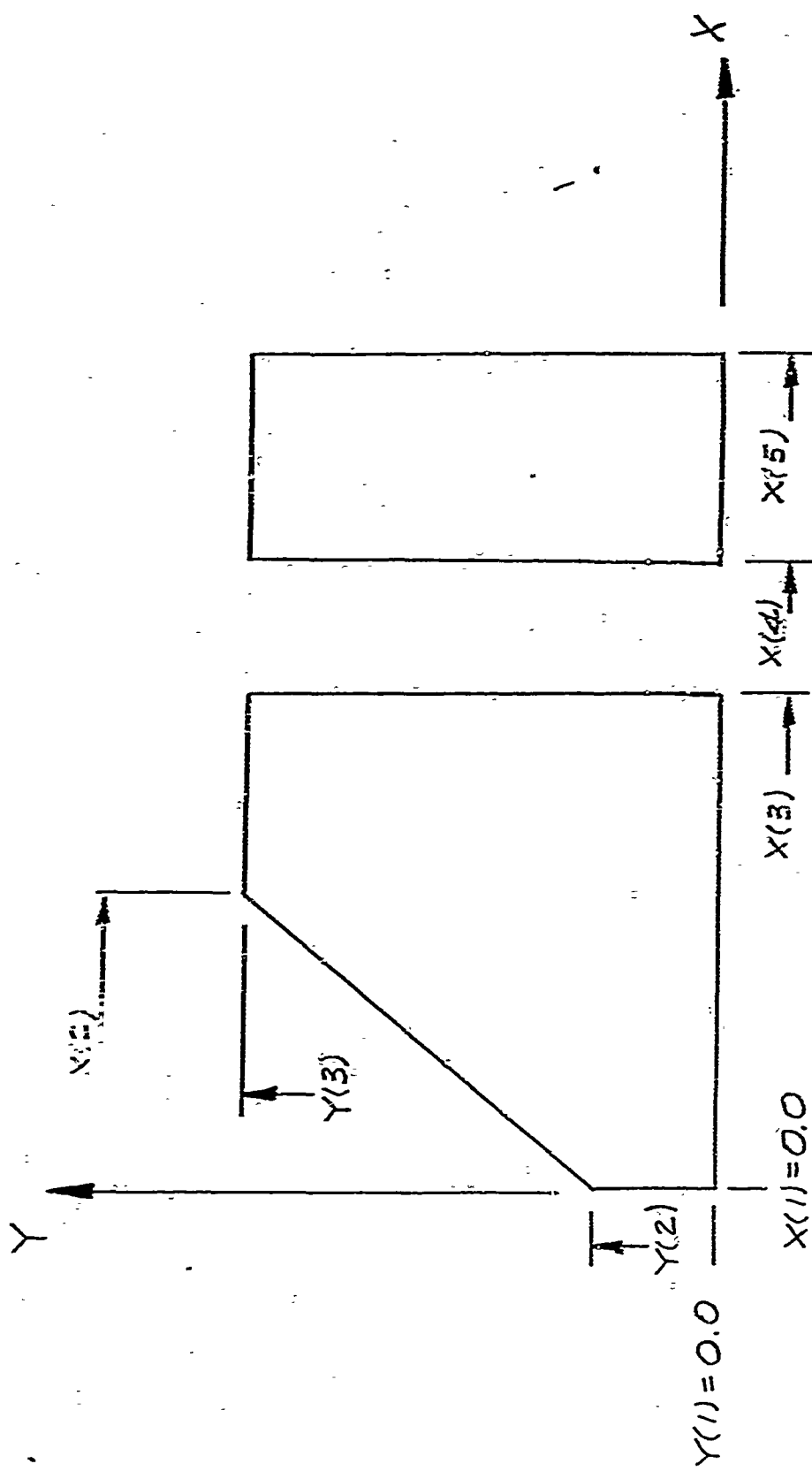


FIGURE 3.3.1  
GEOMETRY DESCRIPTION

3. General Information (6I12 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	NYACH	NFREQ	NMODES	LCOLL	LPRWSH	LPRCØ
Item	(1)	(2)	(3)	(4)	(5)	(6)

- (1) NYACH Number of Mach numbers (max 6)
- (2) NFREQ Number of frequencies at each Mach number (max 10)
- (3) NMODES Number of deformation modes (max 10)
- (4) LCOLL Print collocation stations; 1 ~ Yes; 0 ~ No
- (5) LPRWSH Print pressures and downwashes; 1 ~ Yes; 0 ~ No
- (6) LPRCØ Print pressure coefficients; 1 ~ Yes; 0 ~ No

4. General Information (6I12 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	NWCX	NWPX	NCCX	NCPX	NIØNCCX	
Item	(1)	(2)	(3)	(4)	(5)	(6)

- (1) NWCX Number of chord collocation stations - wing (max 10)
- (2) NWPX Number of chord pressure series terms - wing (max 10)
- (3) NCCX Number of chord collocation stations - control surface (max 10)
- (4) NCPX Number of chord pressure series terms - control surface (max 10)
- (5) NIØNCCX Choose a value of NIØNCCX such that  $NIØNCCX = (NWCX \text{ or } NCCX)$  equals the number of chordwise integration stations  

$$\left( \text{Max } \frac{40}{NWCX} \text{ or } \frac{40}{NCCX} \right)$$

5. General Information (6I12 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	NIY	NWCY	NPY	INWTS	ISØLAT	
Item	(1)	(2)	(3)	(4)	(5)	(6)

- (1) NIY Number of spanwise integration stations (max 11)
- (2) NWCY Number of spanwise collocation stations - wing (max 11)
- (3) NPY Number of spanwise pressure series terms (max 10)
- (4) INWTS Read downwash error weighting factors; 1 ~ Yes; 0 ~ No
- (5) ISØLAT Isolate wing and control surface; 1 ~ Yes; 0 ~ No

6. Weighting Factors (6E12.5 format) (omit these cards when INWTS = 0)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	WT(1)	WT(2)	WT(3)	WT(4)	WT(5)	WT(6)
Item	(1)	(2)	(3)	(4)	(5)	(6)

Continue on successive cards until  $WT(i) = WT(NWTS)$   
 Where  $NWTS = NWCY * NWCX + NIY * NCCX$



7. NØMIT (6I12 format) (omit these cards when NWCY = NIY)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	NØM(1)	NØM(2)	NØM(3)	NØM(4)	NØM(5)	NØM(6)
Item	(1)	(2)	(3)	(4)	(5)	(6)

Continue on successive cards until  $NØM(i) = NØM(NØMIT)$  where  $NØMIT = NIY - NWCY$ . For the solution to be carried out, NWCY must equal NIY. When an excessive number of collocation stations exist, they must be eliminated by spanwise rows. NØM(i) is the spanwise row number to be eliminated. NØMIT = NIY - NWCY is the number of spanwise rows to be eliminated.

8. Mach Numbers (6E12.5 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	FMACH(1)	FMACH(2)	FMACH(3)	FMACH(4)	FMACH(5)	FMACH(6)
Item	(1)	(2)	(3)	(4)	(5)	(6)

- (1) FMACH(1) Mach number
- (2) FMACH(2) Mach number
- · · · ·
- · · · ·
- · · · ·

(NMACH) FMACH(NMACH) Mach number

NMACH values of Mach number must be input. Mach numbers must be greater than zero and less than 0.95.

9. Frequencies (6E12.5 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	FREQ(1)	FREQ(2)	FREQ(3)	FREQ(4)	FREQ(5)	FREQ(6)
Item	(1)	(2)	(3)	(4)	(5)	(6)

- (1) FREQ(1) f(cps)
- (2) FREQ(2) f(cps)
- · · · ·
- · · · ·
- · · · ·

(NFREQ) FREQ(NFREQ)

For NFREQ 6, continue input on new card.

Repeat the following cards  $i = 1, \dots, \text{NM0DES}$

i0. Number of Deformation Mode Polynomial Coefficients to be Read for the  $i^{\text{th}}$  Mode First Surface

Format (6I12)	
Column	1-12      13-24
Name	NZC0(1,i)
Item	(1)              (2)

(1) NZC0(1,i) Number of polynomial coefficients to be read for the first surface, the  $i^{\text{th}}$  mode.

Format (6E12.5)						
Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	C0(0,0)	C0(1,0)	C0(0,1)	C0(2,0)	C0(1,1)	C0(0,2)
Item	(1)	(2)	(3)	(4)	(5)	(6)

C0(i,j) Deformation polynomial coefficients for the first surface in the order: 0,0; 1,0; 0,1; 2,0; 1,1; 2,0; etc. where the first integer is the power of "x" and the second is the power of "y"

Format (6I12)	
Column	1-12      13-24
Name	NZC0(2,i)
Item	(1)              (2)

(1) NZC0(z,i) Number of polynomial coefficients to be read for the second surface and the  $i^{\text{th}}$  mode.

Format (6E12.5)						
Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	C0(0,0)	C0(1,0)	C0(0,1)	C0(2,0)	C0(1,1)	C0(0,2)
Item	(1)	(2)	(3)	(4)	(5)	(6)

C0(i,j) Deformation polynomial coefficients for the second surface in the order: 0,0; 1,0; 0,1; 2,0; 1,1; 2,0; etc.; where the first integer is the power of "x" and the second is the power of "y"

### 3.4 SAMPLE PROBLEM

The generalized forces are calculated for the configuration below. The flight parameters and pertinent input data are presented on the first page of the computer print out.

The coefficients of the deformation modes for the forward surface are shown on the second page of the computer print out, and for the aft surface on the third page of the computer print out.

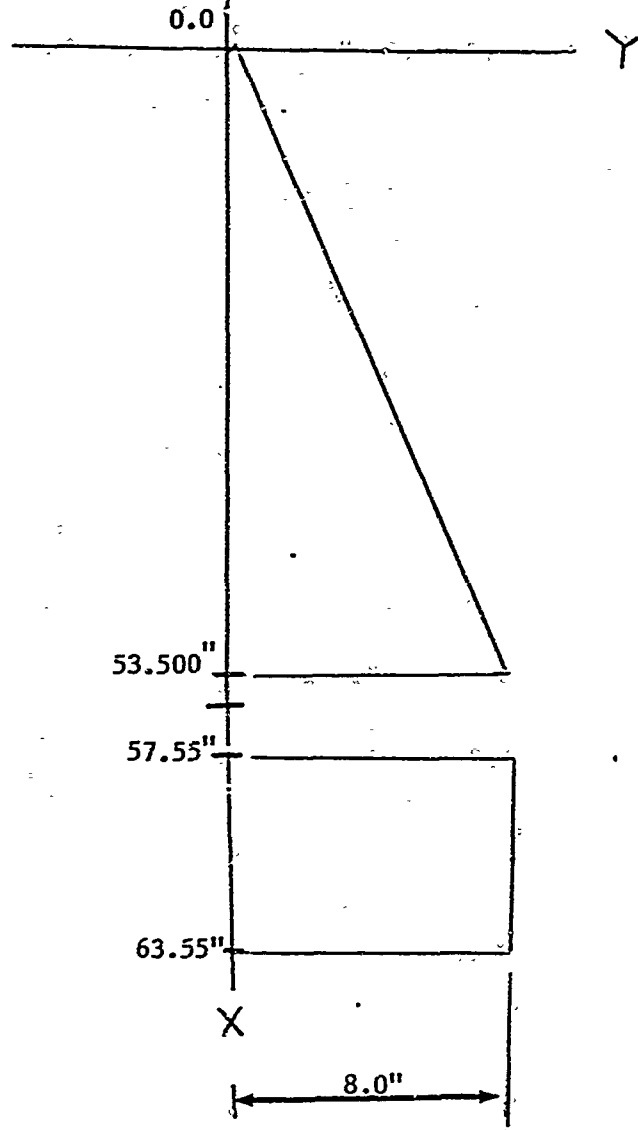


Figure 3.4.1

HAC/NAE MISSILE SUBSONIC AIRLOADS PROGRAM

FLIGHT CONDITIONS AND GEOMETRY

MACH NUMBER = 0.7500      SPEED OF SOUND = 13392.000 L/7      RHO=0.11460000E-06

	WING	TAIL
L.E. STATION (L)	0.	57.550
ROOT CHORD (L)	53.500	0.000
L.E. SPAN (L)	0.	8.000
T.E. SPAN (L)	8.000	8.000
TIP CHORD (L)	0.	6.000
TOTAL AREA (L*L)	428.000	96.000
SPAN COLL. STA.	5	5
CHORD COLL. STA.	5	4
CHORD INTG. STA.	25	20
SPAN PRES MODES	5	5
CHORD PRES MODES	5	4

MISSILE SUBSONIC AIRLOADS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (CPS) 175.00000 5 DEFLECTION MODES  
 REDUCED FREQUENCY (SEMI CHORD) 2.92843 FREE STREAM MACH NUMBER 0.750

INPUT MODE SHAPE POLYNOMIAL COEFFICIENTS FOR HING  
 REFERENCED TO THE SURFACE LEADING EDGE-CENTERLINE INTERSECTION

MODE	COEFFS.												
1	2.0521E-04	-5.1369E-03	-1.7297E-01	6.6410E-04	1.2377E-02	9.4315E-02	-4.0663E-05	3.4901E-04	-1.8280E-02	4.4315E-02	-2.7631E-05	7.0302E-04	-2.4386E-03
	1.7143E-03	-8.7203E-09	3.4448E-07	-7.6417E-06	3.2771E-05	-4.2944E-05	1.4335E-05	1.7143E-03	-8.7203E-09	3.4448E-07	-7.6417E-06	3.2771E-05	1.4335E-05
2	-2.0230E-02	6.6160E-03	5.4738E-01	5.5723E-04	-1.2727E-01	1.1243E-01	-1.1355E-04	1.1767E-02	-6.1689E-02	2.1984E-01	-3.6816E-04	3.0863E-03	-1.4335E-02
	1.2788E-02	-3.8299E-08	3.5697E-06	-3.7881E-05	2.0408E-04	-3.1845E-04	1.9772E-04	1.2788E-02	-3.8299E-08	3.5697E-06	-3.7881E-05	2.0408E-04	1.9772E-04
3	-8.8265E-03	1.5226E-03	-1.3938E 00	2.2485E-03	1.2296E-01	6.1586E-01	-2.4958E-04	2.5723E-03	-1.2793E-01	3.4273E-01	-2.4579E-04	5.1801E-03	-1.9536E-02
	1.3232E-02	-7.0847E-08	3.0849E-06	-5.6882E-05	2.4816E-04	-2.3222E-04	-7.4070E-05	1.3232E-02	-7.0847E-08	3.0849E-06	-5.6882E-05	2.4816E-04	-7.4070E-05
4	-2.3616E-03	-9.5670E-03	-1.2947E-01	8.8089E-04	2.8617E-02	5.8725E-02	-4.8745E-05	7.3151E-04	-5.9538E-02	2.1428E-01	-5.9277E-05	2.1117E-03	-6.0253E-03
	-9.4423E-03	-0.8432E-09	6.9796E-07	-1.9536E-05	4.5021E-05	1.1500E-04	1.5178E-04	-9.4423E-03	-0.8432E-09	6.9796E-07	-1.9536E-05	4.5021E-05	1.5178E-04
5	-1.8034E-04	-1.8284E-05	1.3879E-02	-1.0902E-05	-2.9642E-03	-3.9850E-04	7.7560E-07	1.4335E-04	3.0570E-04	-9.9055E-04	-3.5623E-06	1.1936E-06	-5.9706E-05
	2.6742E-04	1.1484E-10	3.0569E-08	-1.4258E-07	2.1170E-06	-1.1500E-05	1.9655E-05	2.6742E-04	1.1484E-10	3.0569E-08	-1.4258E-07	2.1170E-06	1.9655E-05

MISSILE SUBSONIC AIRLAIDS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (GHS) 175.00000 5 DEFLECTION MOVES  
 REDUCED FREQUENCY (SEMI CHORD) 2.92043 FREE STREAM MACH NUMBER 0.750

INPUT MODE SHAPE POLYNOMIAL COEFFICIENTS FOR TAIL  
 REFERENCED TO THE SURFACE LEADING EDGE-CENTERLINE INTERSECTION.

MODE	COEFFS.													
1	-2.5045E-01	1.3407E-02	-2.0109E-02	9.0702E-04	-1.5111E-03	-1.3471E-02	-4.2571E-04	-5.1564E-04	0.8247E-04	-1.6279E-03	3.9499E-05	4.6416E-05	1.1246E-06	-5.2666E-05
2	-6.0722E-02	1.3622E-02	-5.0481E-03	-5.7007E-03	1.1958E-03	-1.3226E-03	1.7459E-03	-4.4974E-04	2.4416E-05	2.8156E-04	-1.5632E-04	4.2814E-05	8.0306E-06	3.5725E-06
3	-1.6215E-02	1.1602E-02	7.1003E-03	3.8815E-04	-1.5586E-03	8.7454E-05	-2.9670E-04	4.4260E-05	1.9642E-04	2.5398E-04	3.4503E-05	-2.3779E-05	3.0552E-05	-3.5626E-05
4	1.6420E-01	-2.2355E-01	-3.9674E-02	9.4683E-02	3.2691E-02	1.8561E-02	-1.7439E-02	-8.4577E-03	-1.4563E-03	-2.6337E-05	1.0735E-03	7.1000E-04	1.5943E-04	-1.6472E-06
5	-6.0398E-01	3.1261E-01	-1.2775E-02	-4.3907E-02	1.2655E-02	-4.9283E-03	9.3476E-03	-3.2443E-03	6.1969E-04	9.6992E-04	-8.0275E-04	3.4466E-04	3.4043E-04	-1.8608E-04

MISSILE SUBSONIC AIRLOADS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (GFS) 175.0000 5 DEFLECTION MODES  
 REDUCED FREQUENCY (SEMI CHORD) 2.92843 FREE STREAM MACH NUMBER 0.750

GENERALIZED FORCES FOR WING

DEFI	LOAD	REAL PART	IMAG PART	AHS VALUE	PHASE ANGLE
1	1	1.78433E 00	-1.20375E-01	1.78839E 00	-3.859 DEG
1	2	-4.19576E 00	1.94784E 00	-4.62580E 00	155.097 DEG
1	3	9.34031E-01	-1.27098E 01	-1.27441E 01	-85.797 DEG
1	4	1.03725E 01	6.67475E 00	1.23345E 01	32.762 DEG
1	5	-5.40024E-02	6.39892E-01	6.42167E-01	94.824 DEG
2	1	-7.67248E 00	-2.67310E 00	8.12480E 00	-160.792 DEG
2	2	1.58403E 01	-6.01938E 00	1.69455E 01	-20.807 DEG
2	3	-2.68136E 01	3.94086E 01	4.75829E 01	124.299 DEG
2	4	-2.46447E 01	-3.70716E 01	4.45103E 01	-123.005 DEG
2	5	8.50254E 00	-9.48398E 00	1.27373E 01	-48.123 DEG
3	1	4.08041E 00	2.08681E 01	2.12633E 01	78.936 DEG
3	2	1.35203E 01	-2.18268E 01	2.56730E 01	-58.225 DEG
3	3	1.99015E 02	-7.14507E 00	1.99143E 02	-2.056 DEG
3	4	-9.86493E 01	1.51302E 02	1.88621E 02	123.104 DEG
3	5	-2.47112E 01	3.74600E 01	4.48771E 01	123.411 DEG
4	1	6.04738E 00	-1.57318E 01	1.68541E 01	-68.597 DEG
4	2	-3.81082E 01	2.17331E 01	4.38699E 01	150.304 DEG
4	3	-1.44431E 02	-7.27240E 01	1.61707E 02	-153.274 DEG
4	4	1.36556E 02	-6.84736E 01	1.52762E 02	-26.631 DEG
4	5	1.99313E 01	-3.99072E 01	3.67765E 01	-57.183 DEG
5	1	-1.62174E-01	-9.08498E-02	1.86062E-01	-150.773 DEG
5	2	2.15044E-01	2.21553E-01	3.11554E-01	45.326 DEG
5	3	-9.80154E-01	1.64998E 00	1.87955E 00	118.615 DEG
5	4	-6.57931E-01	-1.65552E 00	1.78147E 00	-111.674 DEG
5	5	1.48400E-03	-2.23596E-01	2.23604E-01	-89.620 DEG

MISSILE SUBSONIC AIRLOADS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (CPS) 175.00000 5 DEFLECTION MODES  
 REDUCED FREQUENCY (SPM CHORD) 2.22644 FREEL STREAM MACH NUMBER 0.750

GENERALIZED FORCES FOR TAIL

DEFL	LOAD	REAL PART	IMAG PART	AUS VALUE	PHASE ANGLE
1	1	1.68414E 01	-2.35843E 01	2.89602E 01	-54.470 DEG
1	2	-2.64020E 01	8.04695E 00	2.76019E 01	163.050 DEG
1	3	1.10991E 02	9.07857E 01	1.43392E 02	39.282 DEG
1	4	-1.18089E 02	1.10429E 01	1.18000E 02	174.857 DEG
1	5	9.33634E 01	4.66232E 01	1.04357E 02	26.536 DEG
2	1	1.08962E 00	-3.90206E 00	4.05134E 00	-74.390 DEG
2	2	-3.30264E 00	1.10511E 00	3.50889E 00	160.260 DEG
2	3	1.04867E 01	1.49847E 01	1.82097E 01	55.015 DEG
2	4	-1.60185E 01	-2.94656E 00	1.70746E 01	-170.063 DEG
2	5	1.51049E 01	-1.46806E 02	1.51049E 01	-0.056 DEG
3	1	-1.75194E 00	8.69312E 01	1.95755E 00	153.635 DEG
3	2	1.67228E 00	-5.61288E 01	1.77043E 00	-19.168 DEG
3	3	-9.53124E 00	-2.84436E 00	9.94664E 00	-163.384 DEG
3	4	5.84535E 00	-4.02413E 00	7.09660E 00	-34.545 DEG
3	5	-3.34095E 00	-6.99428E 00	7.75125E 00	-115.532 DEG
4	1	-7.04105E 00	9.69088E 00	1.21411E 01	125.446 DEG
4	2	8.45155E 00	3.31607E 01	8.45928E 00	2.450 DEG
4	3	-4.93566E 01	-2.94018E 01	5.74594E 01	-149.218 DEG
4	4	4.7750E 01	-1.16789E 01	4.91810E 01	-13.737 DEG
4	5	-4.49855E 01	-1.79246E 01	4.84258E 01	-158.275 DEG
5	1	-9.85154E 00	-3.42133E 01	3.56034E 01	-106.063 DEG
5	2	-9.00265E 00	-2.54141E 00	9.35449E 00	-164.236 DEG
5	3	1.16454E 01	9.67328E 01	9.74304E 01	83.135 DEG
5	4	-1.00822E 02	-5.30842E 01	1.13943E 02	-152.233 DEG
5	5	1.42165E 02	-9.58511E 01	1.71459E 02	-33.989 DEG



MISSILE SUBSONIC AIRLOADS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (CPS) 175.00000 5 DEFLECTION MODES  
 REDUCED FREQUENCY (SEMI CHORD) 2.92843 FUEL STREAM MACH NUMBER 0.750

GENERALIZED FORCES FOR WING + TAIL

DEFL	LOAD	REAL PART	IMAG PART	AHS VALUE	PHASE ANGLE
1	1	3.86250E 01	-2.37847E 01	3.01468E 01	-51.842 DEG
1	2	-3.05966E 01	9.99479E 00	3.21896E 01	161.911 DEG
1	3	1.11925E 02	7.80759E 01	1.36467E 02	34.099 DEG
1	4	-1.07712E 02	1.7176E 01	1.09160E 02	170.659 DEG
1	5	9.33094E 01	4.72631E 01	1.04597E 02	26.863 DEG
2	1	-6.58286E 00	-6.57516E 00	9.38412E 00	-135.034 DEG
2	2	1.25177E 01	-4.68428E 00	1.34374E 01	-21.886 DEG
2	3	-1.63268E 01	5.42933E 01	5.66951E 01	106.737 DEG
2	4	-4.14532E 01	-4.80191E 01	5.76178E 01	-136.089 DEG
2	5	2.16074E 01	-9.49866E 00	2.54467E 01	-21.918 DEG
3	1	2.32647E 00	2.17374E 01	2.10616E 01	83.871 DEG
3	2	1.51926E 01	-2.24881E 01	2.78728E 01	-55.063 DEG
3	3	1.89483E 02	-9.98943E 00	1.89747E 02	-3.018 DEG
3	4	-9.28040E 01	1.47278E 02	1.74078E 02	122.216 DEG
3	5	-2.80221E 01	3.04665E 01	4.14141E 01	132.637 DEG
4	1	-9.93673E-01	-5.84895E 00	5.92487E 00	-99.655 DEG
4	2	-2.56567E 01	2.20948E 01	3.69824E 01	143.313 DEG
4	3	-1.93708E 02	-1.82126E 02	2.19091E 02	-152.211 DEG
4	4	1.84331E 02	-8.01525E 01	2.01084E 02	-23.581 DEG
4	5	-2.50541E 01	-4.88318E 01	5.48840E 01	-117.161 DEG
5	1	-1.00139E 01	-3.43842E 01	3.57359E 01	-106.873 DEG
5	2	-8.78360E 00	-2.31966E 00	9.08479E 00	-165.285 DEG
5	3	1.07453E 01	9.83820E 01	9.89670E 01	83.767 DEG
5	4	-1.01480E 02	-5.47397E 01	1.15303E 02	-151.657 DEG
5	5	1.42167E 02	-9.60747E 01	1.71586E 02	-34.050 DEG

## 3.5 PROGRAM LISTING

S	OPTION FORTRAN	SUB78028
S	FORTRAN HLSTOU,DECK	SUB78030
S	INCODE IBMF	SUB78038
CHAIN	MAIN	SUB780340
[	COMPLEX A,AA,ANH,CZERO,GFORC,DELP,WASH,APR,DWASH,CWASH,PR	SUB780350
[	DIMENSION DWASH(90,10),PR(90,10),CWASH(90,10)	SUB780360
[	DIMENSION GFORC(10,10,3),DELP(10),WASH(10)	SUB780370
[	COMMON/C1/A(60),AA(50,60),ANH(50,10),CZERO	SUB780388
[	COMMON/C2/CLEN,SN,NIY,NWCX,NCCX,NWPX,NCPX,HKER(20),ZKER(20),NGSKRMS	SUB780398
[	COMMON/C3/NPY,SOUND,NHACH,FHACH(6),NFREQ,FREQ(10),MAUG,NIONCX,RHO	SUB78400
[	COMMON/C4/NMODES,LCOLL,LPRMSH,LPRCO,NOM(5),IIY,IIIX,NSURF,ISOLAT	SUB78410
[	COMMON/C5/FW,FC,NCOLS,NOMIT,ALPHA(10),IL(50),HCOR(6),ZCOR(6),MACH	SUB78420
[	COMMON/C6/WXCHN(11),WBCN(11),WBIN(11),WT(90),XCOLL,YCOLL,PI,U	SUB78430
[	COMMON/C7/CO(10,28,2),NZCO(10,2),EM,EK,B2,NWIX,NCIX,WBO,CBOM,NWCY	SUB78440
[	COMMON/C8/IFR,XE(5),YE(3),UX(10),UY(10),WXIMN(11),E1,E2	SUB78450
[	COMMON/C9/SIX(40,2),SCX(10,2),Y(11),ETA(11),QWY,QWX,QWCX,CXHN	SUB78460
[	COMMON/CPK/APR(90,60),IMOD,IRON	SUB78470
[	EQUIVALENCE (GFORC,AA),(A,WASH),(WASH,DELP)	SUB78480
[	EQUIVALENCE (DWASH(1,1),APR(1,51)),(PR(1,1),APR(1,11))	SUB78490
[	EQUIVALENCE (CWASH(1,1),APR(1,41))	SUB78500
[	WRITE(6,66)	SUB78510
[	66 FORMAT(1H1)	SUB78520
[	1 CALL KFDA	SUB78530
[	FA = 2*NWIX + 1	SUB78540
[	FC = 2*NCIX + 1	SUB78550
[	QWX = 2.0*PI/FW	SUB78560
[	QWCX = 2.0*PI/FC	SUB78570
[	QWY = PI/FLUAT(2*NIY)	SUB78580
[	CALL GEOM	SUB78590
[	DO 100 MACH=1,NHACH	SUB78600
[	MACH = MACH	SUB78610
[	EM = FHACH(MACH)	SUB78620
[	CALL KOUT(1)	SUB78630
[	U = EM*SOUND	SUB78640
[	IF(LCOLL.NE.0) CALL KOUT(2)	SUB78650
[	BOU = WBO/U	SUB78660
[	B2 = 1.0 - EM*EM	SUB78670
[	DO 100 IFR=1,NFREQ	SUB78680
[	IFR = IFR	SUB78690
[	EK = 2.0*PI*FREQ(IFR)*BOU	SUB78700
[	NSURF = 1 (WING) OR 2 (CONTROL)	SUB78710
[	NCX = NWCX	SUB78720
[	NOMIT = 1	SUB78730
[	MAUG = NCOLS + NMODES	SUB78740
[	DO 4 J=1,NCOLS	SUB78750
[	IL(J) = 0	SUB78760
[	DO 4 K=1,MAUG	SUB78770
[	4 AA(J,K) = CZERO	SUB78780
[	IRON = 1	SUB78790
[	DO 15 NSURF=1,2	SUB78800
[	NSURF = NSURF	SUB78810
[	CALL KOUT(6)	SUB78820
[	KOUT (6) PRINTS COEFFICIENTS OF DEFLECTION SERIES	SUB78830
[	DO 14 IY=1,NIY	SUB78840
[	IIY = IY	SUB78850
[	IF(NOMIT-NOMIT.LT.0) GO TO 7	SUB78860
[	IF(IY-NOM(NOMIT).EQ.0) GO TO 13	SUB78870
[	7 YCOLL = SN*Y(IY)	SUB78880
[	DO 12 IX=1,NCX	SUB78890
[	IIX = IX	SUB78900

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XCOLL = XS(1,NSURF,IX,IY)
CALL CORD
*** CORD FILLS OUT A ROW OF THE DOWNWASH MATRIX EACH TIME CALLED
DO 50 M = 1,NMODES
CALL ZBZX(M,SLOPE,DEFL)
MNC = NCOLS + M
50 WASH(MNC) = CMPLX(SLOPE,DEFL*EK/WBO)
DO 40 K=1,NAUG
X1 = K
IF(X.GT.NCOLS) K1 = 50 + K - NCOLS
40 APR(IROW,K1) = A(K)
DO 60 N=1,NCOLS
60 CALL CGRED(A,W,M)
DO 70 L=1,NMODES
ML = NCOLS + L
70 ALPHA(L) = SQRT(ALPHA(L)**2 + CABS(A(ML))**2)
IROW = IROW + 1
12 CONTINUE
GO TO 14
13 MOMIT = MOMIT + 1
14 CONTINUE
NCX = NCCX
15 CONTINUE
CALL XLSO
*****
IF(LPRCO.EQ.0) GO TO 17
*****
DO 16 IMOD=1,NMODES
IMOD = IMOD
16 CALL KOUT(3)
KOUT(3) PRINTS COEFFICIENTS OF PRESSURE SERIES FOR EACH MODE
*****
17 IF(LPRWSH.EQ.0) GO TO 69
*****
COMPUTE AND STORE THE PRESSURE DOWNWASHES
MOMIT = 1
IROW = 1
NCX = NCCX
DO 115 NSURF=1,2
DO 114 IY=1,NIY
IF(MOMIT.LT.MOMIT) GO TO 107
IF(IY.EQ.NOM(MOMIT)) GO TO 113
107 DO 112 IX=1,NCX
DO 140 IM=1,NMODES
A(IM) = CZERO
DO 140 JC=1,NCOLS
140 A(IM) = A(IM) + APR(IROW,JC)*ANH(JC,IM)
DO 150 IM=1,NMODES
150 CWASH(IROW,IM) = A(IM)
IROW = IROW + 1
112 CONTINUE
GO TO 114
113 MOMIT = MOMIT + 1
114 CONTINUE
NCX = NCCX
115 CONTINUE
69 CALL FORC(NWIX,NCIX,NIY,ETA,SIX,WBIN,0)
IF(LPRWSH.EQ.0) GO TO 77
CALL FORC(NWCX,NCCX,NIY,Y,SCX,WBCN,LPRWSH)
DO 99 IMOD=1,NMODES

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SUB70910
SUB70920
SUB70930
SUB70940
SUB70950
SUB70960
SUB70970
SUB70980
SUB70990
SUB71000
SUB71010
SUB71020
SUB71030
SUB71040
SUB71050
SUB71060
SUB71070
SUB71080
SUB71090
SUB71100
SUB71110
SUB71120
SUB71130
SUB71140
SUB71150
SUB71160
SUB71170
SUB71180
SUB71190
SUB71200
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SUB71410
SUB71420
SUB71430
SUB71440
SUB71450
SUB71460
SUB71470
SUB71480
SUB71490
SUB71500
SUB71510

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IMOD = IMOD
NCX = NMCX
MOMIT = 1
IROW = 1
DO 99 NSURF=1,2
NSURF = NSURF
CALL KOUT (7)
C KOUT (7) PRINTS THE HEADER FOR THE PRESSURE AND DOWNWASH ARRAYS
90 DO 98 IY=1,NIY
IF(NOMIT.LT.MOMIT) GO TO 91
IF(IY.FU.NOM(MOMIT)) GO TO 97
91 YCOLL = WBO*SN*Y(IY)
DO 96 IX=1,NCX
XCOLL = WBO*XS(1,NSURF,IX,IY)
CALL KOUT(9)
C KOUT (9) PRINTS THE X AND Y COORDINATES OF EACH COLLOCATION
C POINT, THE LOCAL PRESSURE, THE DOWNWASH CREATED THERE BY THE
C PRESSURE FIELD, AND THE DOWNWASH OF THE SURFACE AT THE POINT.
C THE DEGREE TO WHICH THE TWO SETS OF DOWNWASHES MATCH IS A MEASURE
C OF THE ACCURACY OF THE SOLUTION OF THE BOUNDARY VALUE PROBLEM.
C THE ROOT-MEAN-SQUARE OF THE ERRORS IS GIVEN IN THE ARRAY ALPHA.
96 IROW = IROW + 1
GO TO 98
97 MOMIT = MOMIT + 1
98 CONTINUE
NCX = NCCX
99 CONTINUE
C *****
77 DO 78 L=1,3
NSURF = L
78 CALL KOUT(8)
C KOUT(8) PRINTS THE GENERALIZED FORCES
100 CONTINUE
GO TO 1
END
$ FORTRAN NLST00,DECK
$ INCODE IBMF
CCONS1 CONS1
BLOCK DATA
COMPLEX A,AA,ANH,CZERO
COMMON/C1/A(60),AA(50,60),ANH(50,10),CZERO
COMMON/C2/CLEN,SN,NIY,NMCX,NCCX,NWPX,NCPX,HKER(20),ZKER(20),NGSKRNSUB70090
COMMON/C3/NPY,SOUND,NMACH,FMACH(6),NFREQ,FREQ(10),MAUG,NIONCX,RHO SUB70100
COMMON/C4/NMODES,LCOLL,LPRWSH,LPRCO,NOM(5),IY,IIX,NSURF,ISOLAT SUB70110
COMMON/C5/FW,FC,NCOLS,NOMIT,ALPHA(10),IL(50),HGOR(6),ZCOR(6),MACH SUB70120
COMMON/C6/WXCMN(11),WBCN(11),WBIN(11),WI(90),XCOLL,YCOLL,PI,U SUB70130
COMMON/C7/CO(10,28,2),NZCO(10,2),EM,EK,2,NWIX,NCIX,WBO,CBON,NWCY SUB70140
COMMON/C8/IFR,XE(5),YE(3),UX(10),UY(10),WXIMN(11),E1,E2 SUB70150
COMMON/C9/SIX(40,2),SCX(10,2),Y(11),ETA(11),QWY,QWX,QWCX,CXMN SUB70160
DATA PI/3.14159265/
DATA HGOR/0.08566225,0.18038079,0.23395697,0.23395697,0.18038079, SUB70180
10.08566225/ SUB70190
DATA ZCOR/0.05376524,0.16939531,0.38069041,0.61930959,0.83060469, SUB70200
10.96623476/ SUB70210
C ***** SUB70220
C NGSKRN SHOULD BE COMPATIBLE WITH HKER AND ZKER LISTS. SUB70230
DATA NGSKRN/8/ SUB70240
DATA (HKER(I),I=1,8)/0.05061427,0.11119052,0.15685332,0.18134189 SUB70250
X,0.18134189,0.15685332,0.11119052,0.05061427/ SUB70260
DATA (ZKER(I),I=1,8)/0.01985507,0.10166676,0.23723380,0.40828268 SUB70270
X,0.59171732,0.76276620,0.89833324,0.98014493/ SUB70280

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C	*****	SUB70290
	DATA E1/8.0000001/,E2/8.0090001/,CZERO/(0.0,0.0)/	SUB70300
	END	SUB70310
S	FORTRAN NLSTOU,DECK	SUB71870
S	INCODE IBMF	SUB71880
CKFDA	KFDA	SUB71890
	SUBROUTINE KFDA	SUB71900
	COMPLEX A,AA,ANH,CZERO	SUB71910
	COMMON/C1/A(60),AA(50,80),ANH(50,10),CZERO	SUB71920
	COMMON/C2/CLEN,SN,NIY,NWCX,NCCX,NWPX,NCPX,HKER(20),ZKER(20),NGSKRNS	SUB71930
	COMMON/C3/NPY,SOUND,NMACH,FMACH(6),NFREQ,FREQ(10),MAUG,NIONCX,RHO	SUB71940
	COMMON/C4/NMODES,LCOLL,LPRMSH,LPRCO,NOM(5),I1Y,I1X,MSURF,ISOLAT	SUB71950
	COMMON/C5/FW,FC,NCOLS,NOMIT,ALPHA(10),IL(50),HGOR(6),ZGOR(6),MACH	SUB71960
	COMMON/C6/WXCMN(11),WBCN(11),WBIN(11),WT(99),XCOLL,YCOLL,PI,U	SUB71970
	COMMON/C7/CU(10,28,2),NZCO(10,2),EM,EK,82,NWIX,NCIX,WBO,CBON,NWCY	SUB71980
	COMMON/C8/IFR,XE(5),YE(3),UX(10),UY(10),WXIMN(11),E1,E2	SUB71990
	COMMON/C9/SIX(40,2),SCX(10,2),Y(11),ETA(11),QWY,QWX,QWCX,CXMN	SUB72000
	READ(5,11)(XE(I),I=1,5)	SUB72010
	READ(5,11)(YE(I),I=1,3),SOUND,RHO	SUB72020
	RHO = RHO/1000.0	SUB72030
	READ(5,12) NMACH,NFREQ,NMODES,LCOLL,LPRMSH,LPRCO	SUB72040
	READ(5,12) NWCX,NWPX,NCCX,NCPX,NIONCX	SUB72050
	READ(5,12) NIY,NWCY,NPY,INWTS,ISOLAT	SUB72060
	NWTS = NWCY*NWCX + NIY*NCCX	SUB72070
	DO 40 I=1,NWTS	SUB72080
40	WI(I) = 1.0	SUB72090
	IF(INWTS.NE.0) READ(5,11)(WI(I),I=1,NWTS)	SUB72100
	NCOLS = NPY + (NWPX + NCPX)	SUB72110
	NCIX = NCCX*NIONCX	SUB72120
	NWIX = NWCX*NIONCX	SUB72130
	NOMIT = 0	SUB72140
	DO 4 I=1,5	SUB72142
4	NOM(I) = 0	SUB72144
	IF(NWCY.GE.NIY) GO TO 5	SUB72150
	NOMIT = NIY-NWCY	SUB72160
	READ(5,12)(NOM(I),I=1,NOMIT)	SUB72170
5	READ(5,11)(FMACH(I),I=1,NMACH)	SUB72180
	DO 7 I=1,NMACH	SUB72190
	IF(FMACH(I).LE.0.99) GO TO 7	SUB72200
	WRITE(6,13)	SUB72210
13	FORMAT(71H A MACH NUMBER GREATER THAN 0.99 HAS BEEN READ IN----	SUB72220
	1CASE TERMINATED)	SUB72230
	CALL EXIT	SUB72240
7	CONTINUE	SUB72250
	READ(5,11)(FREQ(I),I=1,NFREQ)	SUB72260
	DO 20 I = 1,NMODES	SUB72270
	DO 20 L = 1,2	SUB72280
	DO 10 K = 1,28	SUB72290
10	CU(I,K,L) = 0.0	SUB72300
	READ(5,12) NCO	SUB72310
	NZCO(I,L) = NCO	SUB72320
20	READ(5,11)(CU(I,K,L),K=1,NCO)	SUB72330
	DO 30 I=2,5	SUB72340
30	XE(I) = XE(I) - XE(1)	SUB72350
	YE(2) = YE(2) - YE(1)	SUB72360
	YE(3) = YE(3) - YE(1)	SUB72370
11	FORMAT(6E12.8)	SUB72380
12	FORMAT(6I12)	SUB72390
	IF(NCIX.GT.40.OR.NWIX.GT.40) GO TO 86	SUB72400
	IF(NWCX*NWCY+NCCX*NIY.GT.90) GO TO 86	SUB72410
	IF(NPY*(NWPX+NCPX).GT.50) GO TO 86	SUB72420

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IF(NWPX.GT.10.OR.NCPX.GT.10.OR.NPY.GT.10) GO TO 86
RETURN
86 EM = FMACH(1)
CALL KOUT(1)
CALL KOUT(5)
RETURN
END
$   FORTRAN NLSTOU,DECK
$   INCODE IBMF
CGEOM   GEOM
SUBROUTINE GEOM
COMPLEX A,AA,ANH,CZERO
COMMON/C1/A(60),AA(50,60),ANH(50,10),CZERO
COMMON/C2/CLEN,SN,NIY,NWCX,NCCX,NWPX,NCPX,HKER(20),ZKER(20),NGSKRN
COMMON/C3/NPY,SOUND,NMACH,FMACH(6),NFREQ,FREQ(10),MAUG,NIONCX,RHO
COMMON/C4/NMODES,LCOLL,LPRWSH,LPRCO,NUM(5),IIX,IIX,NSURF,ISOLAT
COMMON/C5/FW,FC,NCOLS,NOHIT,ALPHA(10),IL(50),HCDR(6),ZCDR(6),HACH
COMMON/C6/WXCHN(11),WBCN(11),WBN(11),WT(90),XCOLL,YCOLL,PI,S
COMMON/C7/CO(10,28,2),NZCO(10,2),EM,EK,K2,NWIX,NCIX,WBO,CBON,NWCY
COMMON/C8/IFR,XE(5),YE(3),UX(10),UY(10),WXIMN(11),E1,E2
COMMON/C9/SIX(40,2),SCX(10,2),Y(11),ETA(11),QWY,QWX,QWCX,CXHN
C   WBO = WING ROOT SEMI-CHORD
C   S = SEMI-SPAN
C   WTCN = WING TIP CHORD - NORMALIZED ON WBO
C   WLEN = WING TIP L.E. - NORMALIZED
C   SN = SEMI-SPAN - NORMALIZED
C   CBO = CONTROL SEMI-CHORD
C   FW = 2*NWIX+1
C   FC = 2*NCIX+1
C   WBO = XE(3)/2.0
C   CLEN = XE(4)/WBO
C   S = YE(3)
C   WTCN = (XE(3)-XE(2))/WBO
C   WLEN = XE(2)/WBO
C   SN = S/WBO
C   CBO = (XE(5)-XE(4))/2.0
C   F1=FW
C   F2 = F1*PI/2.
C   J = NWIX
C   COMPUTE CHORDWISE INTEGRATION AND COLLOCATION STATIONS
C   FIRST ON THE WING SURFACE
C   DO 5 I=1,NWIX
C   F2 = F2 -2.*PI
C   SIX(J,1) = SIN(F2/F1)
C   I1 = FLOAT(I)/FLOAT(NIONCX) + 0.99
C   SCX(I1,1) = -SIX(J,1)
5   J=J-1
C   F1=FC
C   F2 = F1*PI/2.
C   J = NCIX
C   THEN ON THE CONTROL SURFACE
C   DO 6 I=1,NCIX
C   F2 = F2 -2.*PI
C   SIX(J,2) = SIN(F2/F1)
C   I1 = FLOAT(I)/FLOAT(NIONCX) + 0.99
C   SCX(I1,2) = -SIX(J,2)
6   J=J-1
C   F1 = 4*NIY
C   F2=0.0
C   COMPUTE SPANWISE INTEGRATION AND COLLOCATION STATIONS

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SUB72430
SUB72440
SUB72450
SUB72460
SUB72470
SUB72480
SUB72490
SUB72500
SUB72510
SUB72520
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SUB72540
SUB72550
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SUB72590
SUB72600
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SUB72780
SUB72790
SUB72800
SUB72810
SUB72820
SUB72830
SUB72840
SUB72850
SUB72860
SUB72870
SUB72880
SUB72890
SUB72900
SUB72910
SUB72920
SUB72930
SUB72940
SUB72950
SUB72960
SUB72970
SUB72980
SUB72990
SUB73000
SUB73010
SUB73020

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	DO 8 I=1,NIY	SUB73030
	Y(I) = SIN(F2/F1)	SUB73040
	F2 = F2 +PI	SUB73050
	ETA(I) = SIN(F2/F1)	SUB73060
	8 F2 = F2 +PI	SUB73070
C	COMPUTE WING SEMI-CHORDS AND MID-CHORD LOCATIONS AT THE	SUB73080
C	SPANWISE COLLOCATION AND INTEGRATION STATIONS	SUB73090
	PIB = YE(2)/YE(3)	SUB73100
	POB =1.0-PIB	SUB73110
	CBON = (XE(5)-XE(4))/(2.0*WBO)	SUB73120
	CXMN = CBON +XE(4)/WBO	SUB73130
	DO 16 I=1,NIY	SUB73140
	IF(ETA(I).LE.PIB) GO TO 12	SUB73150
	F1 = WLEN*(ETA(I)-PIB)/POB	SUB73160
	IF(Y(I).LE.PIB) GO TO 13	SUB73170
	F2 = WLEN*(Y(I)-PIB)/POB	SUB73180
	GO TO 14	SUB73190
22	F1 = 0.0	SUB73200
13	F2 = 0.0	SUB73210
14	WBIN(I) = 0.5*(2.0-F1)	SUB73220
	WXIMN(I) = WBIN(I) +F1	SUB73230
	WBCN(I) = 0.5*(2.0-F2)	SUB73240
16	WXCHN(I) = WBCN(I) +F2	SUB73250
36	RETURN	SUB73260
	END	SUB73270
5	FORTRAN NLSTOU,DECK	SUB73280
5	INCODE IBMF	SUB73290
CXS	XS	SUB73300
	FUNCTION XS(L,NS,13,J3)	SUB73310
	COMPLEX A,AA,ANH,CZERO	SUB73320
	COMMON/C1/A(64),A(50,60),ANH(50,10),CZERO	SUB73330
	COMMON/C2/CLEN,SN,NIY,NWCX,NCCX,NWPX,NCPX,HKER(20),ZKER(20),NGSKRN	SUB73340
	COMMON/C3/NPY,SOUND,NMACH,FMACH(6),NFREQ,FREQ(10),MAUG,NIONCX,RHO	SUB73350
	COMMON/C4/NMODFS,ICOLL,LPRWSH,LPRCO,NOM(5),I1Y,I1X,NSURF,ISOLAT	SUB73360
	COMMON/C5/FW,FC,NCOLS,NOKIT,ALPHA(10),II(50),HGOR(6),ZCOR(6),MACH	SUB73370
	COMMON/C6/WXCHN(11),WBCN(11),WBIN(11),WI(90),XCOLL,YCOLL,PI,U	SUB73380
	COMMON/C7/CO(10,28,2),NZCO(10,2),EM,EK,R2,NWIX,NCIX,WBO,CBON,NWCY	SUB73390
	COMMON/C8/IFR,XE(5),YE(3),UX(10),UY(10),WXIMN(11),E1,E2	SUB73400
	COMMON/C9/SIX(40,2),SCX(10,2),Y(11),ETA(11),QWY,QWNX,QWCX,CXMN	SUB73410
	GO TO (10,40),L	SUB73420
10	GO TO (20,30),NS	SUB73430
20	XS = WXCHN(J3) + WBCN(J3) * SCX(13,1)	SUB73440
	RETURN	SUB73450
30	XS = CXMN + CBON * SCX(13,2)	SUB73460
	RETURN	SUB73470
40	GO TO (50,60),NS	SUB73480
50	XS = WXIMN(J3) + WBIN(J3) * SIX(13,1)	SUB73490
	RETURN	SUB73500
60	XS = CXMN + CBON * SIX(13,2)	SUB73510
	RETURN	SUB73520
	END	SUB73530
5	FORTRAN NLSTOU,DECK	SUB73540
5	INCODE IBMF	SUB73550
CBESL	BESL	SUB73560
	FUNCTION BESL(X)	SUB73570
	IF(X.GT.2.0) GO TO 50	SUB73580
	T=X/3.75	SUB73590
	T=T*T	SUB73600
	RS11=0.5+T*(0.87890594+T*(0.51498869+T*(0.15084934+T*(0.02658733+T	SUB73610
	1*(0.00301532+T*(0.00032411))))))	SUB73620
	RS11=RS11*X	SUB73630

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Y=X/2.0
BSK1=X*ALOG(Y)*BSI1+1.0
Y=Y*Y
BSK1=BSK1+Y*(0.15443144+Y*(-0.67278579+Y*(-0.18156897+Y*
1(-0.01919402+Y*(-0.00110404+Y*(-0.00004586))))))
RESL =BSK1/X
GO TO 60
50 Y=2.0/X
BSK1=1.25331414+Y*(0.23498619+Y*(-0.03655620+Y*(0.01504268+Y*
1(-0.00780353+Y*(0.00325614+Y*(-0.00068245))))))
RESL =BSK1/(SORT(X)*EXP(X))
60 RETURN
END
$   FORTRAN NLSTOU,DECK
$   INCODE IBMF
CCRNL   CRNL
COMPLEX FUNCTION CRNL(CK,X,Y,CM,B2)
COMMON/C2/CLFN,SN,NIY,NWCX,NCCX,NWPX,NCPX,HKER(20),ZKER(20),NGSKRNSUB73640
R=ABS(Y)
R2=R*R
CK1 = CK*R
G1 = 0.0
G3 = 0.0
G4 = 0.0
5   S2 = X*X + R2*R2
S = SORT(S2)
U1 = (CM*S-X)/(R2*R)
UK = CK1*U1
DO 20 I = 1,NGSKRN
UZ = U1*ZKER(I)
UZ2 = UZ**2
G=UK*ZKER(I)
F = HKFR(I)/ SORT(1.0+UZ2)*UZ*U1
G3=G3+F*COS(G)
G4=G4+F*SIN(G)
V = 1.0 - ZKER(I)**2
F = HKER(I)*2.0*V* EXP(-CK1*V)/ SORT(1.0+V)
20 G1=G1+F
G7 = G1 + G3
XS = X/S
IF(CK.NE.0.0) GO TO 22
F14 = 1.0
GO TO 23
22 F14 = CK1*RESL(CK1)
23 G1=CK1*G4-F14-XS*COS(UK)
G2=CK1*G7+XS*SIN(UK)
XK = CK*X
CU = COS(XK)
SI = SIN(XK)
CRNL = CMPLX((CU*G1+SI*G2)/R2,(CO*G2-SI*G1)/R2)
RETURN
END
$   FORTRAN NLSTOU,DECK
$   INCODE IBMF
CCORD   CORD
SUBROUTINE CORD
COMPLEX A,AA,ANM,CZERO
COMPLEX AK,H2,TRM,D1,CRNL
COMMON/C1/A(60),AA(50,60),ANM(50,10),CZERO
COMMON/C2/CLFN,SN,NIY,NWCX,NCCX,NWPX,NCPX,HKER(20),ZKER(20),NGSKRNSUB73650
COMMON/C3/NPY,SOUND,NMACH,FMACH(6),NFREQ,FREQ(10),MAUG,NIONCX,RHO SUB73660
SUB73670
SUB73700
SUB73710
SUB73720
SUB73730
SUB73740
SUB73750
SUB73760
SUB73770
SUB73780
SUB73790
SUB73800
SUB73810
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SUB73970
SUB73980
SUB73990
SUB74000
SUB74010
SUB74020
SUB74030
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SUB74060
SUB74070
SUB74080
SUB74090
SUB74100
SUB74110
SUB74120
SUB74130
SUB74140
SUB74150
SUB74530
SUB74540
SUB74550
SUB74560
SUB74570
SUB74580
SUB74590
SUB74600
SUB74610

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COMMON/C4/MNODES,LCOLL,LPRWSH,LPRCO,NOM(5),I1Y,I1X,NSURF,ISOLAT SUB74620
COMMON/C5/FW,FC,NCOLS,NOMIT,ALPHA(10),IL(50),HGOR(6),ZCOR(6),MACH SUB74630
COMMON/C6/WXCHN(11),WHCH(11),WBIN(11),WT(90),XCOLL,YCOLL,P1,U SUB74640
COMMON/C7/CO(10,28,2),NZCO(15,2),EM,EK,B2,NWIX,NCIX,WBO,CBON,NWCY SUB74650
COMMON/C8/IFR,XE(5),YE(3),UX(10),UY(10),WXIMN(11),E1,E2 SUB74660
COMMON/C9/SIX(40,2),SCX(10,2),Y(11),ETA(11),QWY,QWX,QWCX,CXMN SUB74670
THIS SUBROUTINE CONSTRUCTS A ROW OF THE DOWNWASH MATRIX SUB74680
THE PRESSURE SERIES IS A PRODUCT OF CHERYSHEV POLYNOMIALS IN THE SUB74690
NEGATIVE OF PERCENT SEMI-CHORD FROM THE MID-CHORD AND PERCENT SUB74700
SEMI-SPAN FROM THE ROOT. SUB74710
DO 6 JC=1,NCOLS SUB74720
6 A(JC) = CZERO SUB74730
IC1 = 0 SUB74740
NIX = NWIX SUB74750
QWX = -QWXX*SN**2/(8.0*PI) SUB74760
NPX = NWPX SUB74770
C THE DO 14 LOOP COMPUTES THE NON-SINGULAR PORTION OF D(N,M) SUB74780
C DUF TO BOTH SURFACES SUB74790
DO 14 MSURF=1,2 SUB74800
IF (MSURF.NE.NSURF.AND.ISOLAT.NE.0) GO TO 13 SUB74810
DO 12 IY=1,NIY SUB74820
ETA1 = SN*ETA(IY) SUB74830
E12 = ETA(IY)**2 SUB74840
IF (NPY.GT.1) CALL CHEB(NPY-1,ETA(IY),UY(2)) SUB74850
UY(1) = 1.0 -FT2 SUB74860
DO 3 K=2,NPY SUB74870
3 UY(K) = E12*UY(1)*UY(K) SUB74880
DO 10 IX=1,NIX SUB74890
XI = XS(2,MSURF,IX,IY) SUB74900
XID = XCOLL -XI SUB74910
AK = CRNL(EK,XID,YCOLL-ETA1,EK,B2) + CRNL(EK,XID,YCOLL+ETA1,EK,B2) SUB74920
IC = IC1 +1 SUB74930
H2 = AK*QWX*QWY SUB74940
IF (NPX.GT.1) CALL CHEB(NPX-1,-SIX(IX,MSURF),UX(2)) SUB74950
UX(1) = 1.0 -SIX(IX,MSURF) SUB74960
DO 4 K=2,NPX SUB74970
4 UX(K) = (1.0 +SIX(IX,MSURF))*UX(1)*UX(K) SUB74980
C ** ADD AN INCREMENT TO EACH ELEMENT OF THE ROW FOR (XI,ETA!) ** SUB74990
DO 10 NY=1,NPY SUB75000
TRM = H2 * UY(NY) SUB75010
DO 10 NX=1,NPX SUB75020
A(IC) = A(IC) +TRM*UX(NX) SUB75030
10 IC = IC+1 SUB75040
C ** IC EQUALS NPY*NWPX+1 AT THE END OF THE FIRST PASS ** SUB75050
12 CONTINUE SUB75060
13 NIX = NCIX SUB75070
QWX = -QWCX*SN**2/(8.0*PI) SUB75080
NPX = NCPX SUB75090
14 IC1 = NPY*NWPX SUB75100
IC1 = 0 SUB75110
NPX = NWPX SUB75120
XCOLS = XS(1,NSURF,I1X,I1Y) SUB75130
Y2 = Y(I1Y)**2 SUB75140
CALL CHEB(NPY-1,Y(I1Y),UY(2)) SUB75150
UY(1) = -2.0 SUB75160
DO 15 K=2,NPY SUB75170
15 UY(K) = -2.0*Y2*UY(K) SUB75180
DO 40 MSURF=1,NSURF SUB75190
C ** THIS LOOP ADDS THE CONTRIBUTION OF THE SINGULAR INTEGRAL SUB75200
C ALONG THE LINE FROM THE WING L.E. TO THE COLLOCATION POINT SUB75210
IF (MSURF.NE.NSURF.AND.ISOLAT.NE.0) GO TO 23 SUB75220

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IF(NSURF.LE.HSURF) GO TO 16
UPLIM = PI
GO TO 18
16 XI = SCX(IIX,NSURF)
UPLIM = -ATAN(SQRT(1.0-XT**2)/XT)
IF(UPLIM.LT.0.0) UPLIM=UPLIM+PI
18 QWSNG = FLOAT(2*NIY)*UPLIM/8.0
DO 22 N=1,6
IC = IC+1
C
  ** THIS LOOP CONSTRUCTS D(0,M) ,M=0,1,...,NPX-1
  VINI = UPLIM*ZCOR(N)
  C = COS(VINI)
  CALL CHEB(NPX-1, C,UX(2))
  UX(1) = 1.0 +C
  DO 19 K=2,NPX
19 UX(K) = (1.0 -C)*UX(1)+UX(K)
  ARG = EK*(XCOLS -WXCHN(IJY) +C*WBCN(IJY))
  IF(HSURF.EQ.2) ARG=EK*(XCOLS-CXMN+C*CBON)
  C1 = COS(ARG)
  S1 = SQRT(1.0 -C1**2)
  D1 = CMPLX(C1,-S1)*HCOR(N)
  DO 22 NY=1,NPY
  TRM = QWSNG*UY(NY)*D1
  DO 22 NX=1,NPX
  A(IC) = A(IC) +TRM*UX(NX)
22 IC = IC+1
23 ICI = NPY*NWPX
40 NPX = NCPX
RETURN
END
$
$
CZDZX
SUBROUTINE ZDZX(MODE,DZ,Z)
COMPLEX A,AA,ANM,CZERO
COMMON/C1/A(60),AA(50,60),ANM(50,10),CZERO
COMMON/C2/CLFN,SN,NIY,NWCX,NCCX,NWPX,NCPX,HKFR(20),ZKER(20),NGSKRNSUR
COMMON/C3/NPY,SOUND,NMACH,FMACH(6),NFREQ,FREQ(10),MAUG,NIONCX,RHO
COMMON/C4/NMODES,LCOLL,LPRWSH,LPRCO,NOM(5),IJY,IIX,NSURF,ISOLAT
COMMON/C5/FW,FC,NCOLS,NOMIT,ALPHA(10),II(50),HCOR(6),ZCOR(6),MACH
COMMON/C6/WXCHN(11),WBCN(11),WBIN(11),WI(90),XCOLL,YCOLL,PI,U
COMMON/C7/CO(10,28,2),NZCO(10,2),EK,EK2,NWIX,NCIX,WBO,CBON,NWCY
COMMON/C8/IFR,XE(5),YE(3),UX(10),UY(10),WXTMN(11),E1,E2
COMMON/C9/SIX(40,2),SCX(10,2),Y(11),ETA(11),QWY,QWXX,QWCX,CXHN
PX = XCOLL * WBO
IF(NSURF.GT.1) PX=PX-CLFN*WBO
PY = YCOLL * WBO
Z = CO(MODE,1,NSURF)
DZ = 0.0
K = 2
YX = PY/PX
PPX = PX
DO 40 N = 2,7
PXY = PPX
F = N-1
DO 30 M = 1,N
IF(K.GT.NZCO(MODE,NSURF)) GO TO 50
ZP = PXY * CO(MODE,K,NSURF)
Z = Z + ZP
DZ = DZ + ZP * F

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SUB75230  
SUB75240  
SUB75250  
SUB75260  
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SUB75420  
SUB75430  
SUB75440  
SUB75450  
SUB75460  
SUB75470  
SUB75480  
SUB75490  
SUB75500  
SUB75510  
SUB74160  
SUB74170  
SUB74180  
SUB74190  
SUB74200  
SUB74210  
SUB74220  
SUB74230  
SUB74240  
SUB74250  
SUB74260  
SUB74270  
SUB74280  
SUB74290  
SUB74300  
SUB74310  
SUB74320  
SUB74330  
SUB74340  
SUB74350  
SUB74360  
SUB74370  
SUB74380  
SUB74390  
SUB74400  
SUB74410  
SUB74420  
SUB74430  
SUB74440  
SUB74450

```

    PXY = PXY*YX
    F = F - 1.0
30  K = K + 1
40  PPX = PPX + PX
50  DZ = DZ/PX
    RETURN
    END

```

```

$   FORTRAN NLSTOU,DECK
$   INCODE  IBMF
CCGRFD  CGRED

```

```

SUBROUTINE CGRED(V,IR,IC)
COMPLEX ANM,CZERO
DIMENSION V(2,1)
COMMON/C1/A(2,60),AA(2,50,60),ANM(50,10),CZERO
COMMON/C2/CLEN,SN,NIY,NWCX,NCCX,NWPX,NCFX,HKER(20),ZKER(20),NGSKRNSUB75590
COMMON/C3/NPY,SOUND,NMACH,FMACH(6),NFREQ,FREQ(10),MAUG,NIUNCX,RHO  SUB75600
COMMON/C4/NMODES,LCOLL,LPRWSH,LPRCO,NOM(5),IIY,IIY,NSURF,ISOLAT  SUB75610
COMMON/C5/FW,FC,NCOLS,NOMIT,ALPHA(10),II(50),HCO(6),ZC(6),MACH  SUB75620
COMMON/C6/WXCMN(11),WBCN(11),WBIN(11),WI(90),XCOLL,YCOLL,PI,U  SUB75630
COMMON/C7/CU(10,28,2),NZCO(10,2),EM,EK,2,NWIX,NCIX,WBO,CBON,NWCY  SUB75640
COMMON/C8/IFR,XE(5),YE(3),UX(10),UY(10),WXIMN(11),E1,E2  SUB75650
COMMON/C9/SIX(40,2),SCX(10,2),Y(11),ETA(11),QWY,QWXX,QWCX,CXMN  SUB75660
RMN = SQRT(AA(1,IR,IC)**2 + AA(2,IR,IC)**2)
IF(AA(2,IR,IC).LE.E2) GO TO 30
CR = AA(1,IR,IC)/RMN
CI = AA(2,IR,IC)/RMN
DO 20 N=IC,MAUG
TI = CR*AA(1,IR,N) + CI*AA(2,IR,N)
AA(2,IR,N) = CR*AA(2,IR,N) - CI*AA(1,IR,N)
20 AA(1,IR,N) = TI
30 RAN = SQRT(V(1,IC)**2 + V(2,IC)**2)
IF(RAN.LE.E2) GO TO 60
RAN = SQRT(RAN**2 + RMN**2)
CR = V(1,IC)/RAN
CI = V(2,IC)/RAN
RMN = RMN/RAN
DO 50 N=IC,MAUG
AIR = RMN*AA(1,IR,N) + CR*V(1,N) + CI*V(2,N)
AII = RMN*AA(2,IR,N) + CR*V(2,N) - CI*V(1,N)
VR = RMN*V(1,N) - CR*AA(1,IR,N) + CI*AA(2,IR,N)
VI = RMN*V(2,N) - CR*AA(2,IR,N) - CI*AA(1,IR,N)
AA(1,IR,N) = AIR
AA(2,IR,N) = AII
V(1,N) = VR
50 V(2,N) = VI
60 RETURN
END

```

```

$   FORTRAN NLSTOU,DECK
$   INCODE  IBMF
CXLSO  XLSO

```

```

SUBROUTINE XLSO
COMPLEX A,AA,ANM,CZERO
COMMON/C1/A(60),AA(50,60),ANM(50,10),CZERO
COMMON/C2/CLEN,SN,NIY,NWCX,NCCX,NWPX,NCFX,HKER(20),ZKER(20),NGSKRNSUB75980
COMMON/C3/NPY,SOUND,NMACH,FMACH(6),NFREQ,FREQ(10),MAUG,NIUNCX,RHO  SUB75990
COMMON/C4/NMODES,LCOLL,LPRWSH,LPRCO,NOM(5),IIY,IIY,NSURF,ISOLAT  SUB76000
COMMON/C5/FW,FC,NCOLS,NOMIT,ALPHA(10),II(50),HCO(6),ZC(6),MACH  SUB76010
COMMON/C6/WXCMN(11),WBCN(11),WBIN(11),WI(90),XCOLL,YCOLL,PI,U  SUB76020
COMMON/C7/CU(10,28,2),NZCO(10,2),EM,EK,2,NWIX,NCIX,WBO,CBON,NWCY  SUB76030
COMMON/C8/IFR,XE(5),YE(3),UX(10),UY(10),WXIMN(11),E1,E2  SUB76040
COMMON/C9/SIX(40,2),SCX(10,2),Y(11),ETA(11),QWY,QWXX,QWCX,CXMN  SUB76050

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SUB74460  
SUB74470  
SUB74480  
SUB74490  
SUB74500  
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SUB75520  
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SUB75980  
SUB75990  
SUB76000  
SUB76010  
SUB76020  
SUB76030  
SUB76040  
SUB76050

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I1 = 1
DO 136 I=1,NCOLS
RII = CABS(AA(I1,I))
IF(RII.LE.E2) GO TO 135
IL(I) = I1
I1 = I1 + 1
GO TO 136
135 IL(I) = -1
I12 = NCOLS - 1 - (I-I1)
DO 1135 I1=I1,I12
1135 CALL CGRED(AA(I1+1,I),I1,I+1)
DO 2135 L=1,NMODES
ML = NCOLS + L
2135 ALPHA(L) = SORT(ALPHA(L)**2 + CABS(AA(I12+1,ML))**2)
136 CONTINUE
C SOLVE FOR THE COEFFICIENTS BY BACK SUBSTITUTION
140 I1 = NCOLS
DO 150 I = 1,NCOLS
DO 150 L=1,NMODES
150 ANM(I,L) = CZERO
DO 210 J=1,NCOLS
IF(IL(I1).LE.0) GO TO 210
JI = IL(I1)
DO 200 L=1,NMODES
ML = NCOLS + L
IF(I1-NCOLS) 170,190,220
170 IK = I1 + 1
DO 180 K=IK,NCOLS
180 ANM(I1,L) = ANM(I1,L) - AA(JI,K)*ANM(K,L)
190 ANM(I1,L) = (ANM(I1,L) + AA(JI,ML))/AA(JI,I1)
200 CONTINUE
210 I1 = I1 - 1
220 RETURN
END
* FORTRAN NLSTOU,DECK
$ INCODE IBMF
CCHER CHEB
SUBROUTINE CHEB(N1,X,UX)
DIMENSION UX(1)
DO 10 I=1,N1
10 UX(I) = 0.0
UX(1) = 1.0
UX(2) = 2.0*X
IF(N1.LT.3) RETURN
DO 20 I=3,N1
20 UX(I) = 2.0*X*UX(I-1) - UX(I-2)
RETURN
END
$ FORTRAN NLSTOU,DECK
$ INCODE IBMF
CFORC FORC
SUBROUTINE FORC(NWICX,NCICX,NICY,YEIA,SICX,WBICN,LPR)
COMPLEX A,AA,ANM,CZERO,GFORC,DELPH,WASH,APR,DWASH,CWASH,PR
DIMENSION YI(TA(1),SICX(1),WBICN(1))
DIMENSION DWASH(90,10),PR(90,10),CWASH(40,10)
DIMENSION GFORC(10,10,3),DELPH(10),WASH(10)
COMMON/C1/A(60),AA(50,60),ANM(50,10),CZERO
COMMON/C2/CLFN,SN,NIY,NWCX,NCCX,NWPX,NCPX,HKER(20),ZKER(20),NGSKRNSUR
COMMON/C3/NFY,SOUND,NMACH,FMACH(6),NFREQ,FREQ(10),MAUG,NIONCX,RHO
COMMON/C4/NMODES,LCOLL,LPRWSH,LPRCO,NOM(5),I1Y,I1X,NSURF,ISOLAT

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SUB76060  
SUB76070  
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SUB76650

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COMMON/C5/FW,FC,NCOLS,NONIT,ALPHA(10),IL(50),HCOR(6),ZCOR(6),MACH SUB76660
COMMON/C6/WXCHN(11),WBCN(11),WBCN(11),WT(90),XCOLL,YCOLL,PI,U SUB76670
COMMON/C7/CO(10,28,2),NZCO(10,2),EM,EK,H2,NHIX,NCIX,WBO,CBON,NWCY SUB76680
COMMON/C8/IFR,XE(5),YE(3),UX(10),UY(10),WXIHN(11),E1,E2 SUB76690
COMMON/C9/SIX(40,2),SCX(10,2),Y(11),ETA(11),QWY,QWXX,QWCX,CXMN SUB76700
COMMON/CPR/APR(90,60),IMOD,IROW SUB76710
EQUIVALENCE (GFORC,AA),(A,WASH),(WASH,DELTA) SUB76720
EQUIVALENCE (WASH(1,1),APR(1,51)),(PR(1,1),APR(1,11)) SUB76730
EQUIVALENCE (WASH(1,1),APR(1,41)) SUB76740
QWF = 0.5*RHO*(U*WBO*SN)**2 *QWY SUB76750
IF(LPR.NE.0) GO TO 2 SUB76760
DO 1 I=1,NMODES SUB76770
DO 1 J=1,NMODES SUB76780
DO 1 K=1,2 SUB76790
1 GFORC(I,J,K) = CZERO SUB76800
2 IC1 = 0 SUB76810
NICX = NWICX SUB76820
NPX = NWPX SUB76830
QWFORC = QWF*QWXX SUB76840
IROW = 1 SUB76850
LMNT1 = 4N SUB76860
IF(LPR.NE.0) LMNT1 = 10 SUB76870
DO 1000 NS=1,2 SUB76880
NSURF = NS SUB76890
PFAC = SN/CBON SUB76900
DO 900 IY=1,NICY SUB76910
YCOLL = Y-ETA(IY) SUB76920
** YCOLL, AND LATER XCOLL, ARE USED HERE TO DENOTE INTEGRATION SUB76930
STATIONS BECAUSE WE USE SUBROUTINE ZOX TO COMPUTE THE SUB76940
DISPLACEMENT THROUGH WHICH THE PRESSURE ACTS TO DO WORK SUB76950
Y2 = YCOLL**2 SUB76960
IF(NPY.GT.1) CALL CHER(NPY-1,YCOLL,UY(2)) SUB76970
UY(1) = 1.0 -Y2 SUB76980
IF(LPR.NE.0) UY(1)=SQRT(1.0-Y2) SUB76990
DO 3 K=2,NPY SUB77000
3 UY(K) = Y2*UY(1)*UY(K) SUB77010
IF(NSURF.EQ.1) PFAC=SN/WBICN(IY) SUB77020
YCOLL = SN*YCOLL SUB77025
DO 800 IX=1,NICX SUB77030
LMNT1 = SIX +LMNT1*(NSURF-1) SUB77040
XCOLL = SICX(LMNT1) SUB77050
IF(NPX.GT.1) CALL CHER(NPX-1,-XCOLL,UX(2)) SUB77060
UX(1) = 1.0 -XCOLL SUB77070
IF(LPR.NE.0) UX(1)=SQRT(UX(1)/(1.0+XCOLL)) SUB77080
DO 4 K=2,NPX SUB77090
4 UX(K) = (1.0 +XCOLL)*UX(1)*UX(K) SUB77100
IC = IC1 +1 SUB77110
DO 10 J=1,NMODES SUB77120
10 DELP(J) = CZERO SUB77130
DO 200 NY=1,NPY SUB77140
DO 200 NX=1,NPX SUB77150
DO 20 J=1,NMODES SUB77160
DELP(J) = DELP(J) +UX(NX)*UY(NY)*ANM(IC,J) SUB77170
IF(LPR.NE.0) PR(IROW,J) = DELP(J)*PFAC SUB77180
20 CONTINUE SUB77190
200 IC = IC+1 SUB77200
** IC = NPY*NWPX+1 AT THE END OF THE NS=1 PASS SUB77210
AND DP CONTAINS DELTA P/RHO AT (XCOLL,YCOLL) SUB77220
IROW = IROW + 1 SUB77230
IF(LPR.NE.0) GO TO 800 SUB77240
XCOLL = XS(2,NS,IX,IY) SUB77245

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DO 400 I=1,NMODES
CALL ZDZX(I,SLOPE,DISP)
DO 400 J=1,NMODES
400 GFORC(I,J,NS) = GFORC(I,J,NS) +QWFORC*DISP*DELP(J)*2.0
800 CONTINUE
900 CONTINUE
NICX = NCICX
NPX = NCPX
IC1 = IC-1
QWFORC = QW1 +QWCX
1000 CONTINUE
RETURN
END
$ FORTRAN NLST:U,DECK
$ INCODE IBMF
CKOUT KOUT
SUBROUTINE KOUT(IND)
COMPLEX A,AA,ANH,CZERO,GFORC,DELP,WASH,APR,DWASH,CWASH,PR
DIMENSION CARDS(25,50)
DIMENSION GFORC(10,10,3),DELP(10),WASH(10)
DIMENSION DWASH(90,10),PR(90,10),CWASH(90,10)
DIMENSION SURF(2,3),XPR(50)
COMMON/C1/A(60),AA(50,60),ANH(50,10),CZERO
COMMON/C2/CLFN,SN,NIY,NWCX,NCCX,NWPX,NCPX,HKER(20),ZKER(20),NGSKRNS
COMMON/C3/NPY,SOUND,NHACH,FMACH(6),NFREQ,FREQ(10),MAUG,NIONCX,RHO
COMMON/C4/NMODES,LCOLL,LPRWSH,LPRCO,NUM(5),I1Y,I1X,NSURF,ISOLAT
COMMON/C5/FW,FC,NCOLS,NOMIT,ALPHA(10),IL(50),HCOR(6),ZCOR(6),HACH
COMMON/C6/WXCHN(11),WBCH(11),WBIN(11),WI(90),XCOLL,YCOLL,PI,U
COMMON/C7/CO(10,28,2),NZCO(10,2),EM,EK,K2,NWIX,NCIX,WBO,CBON,NWCY
COMMON/C8/IFR,XE(5),YE(3),UX(10),UY(10),WXIH(11),E1,E2
COMMON/C9/SIX(40,2),SCX(10,2),Y(11),ETA(11),QWY,QWX,QWCX,CXHN
COMMON/CPR/APP(90,60),IMOD,IRON
EQUIVALENCE (GFORC,AA),(A,WASH),(WASH,DELP)
EQUIVALENCE (DWASH(1,1),APR(1,51)),(PR(1,1),APR(1,11))
EQUIVALENCE (CWASH(1,1),APR(1,41))
EQUIVALENCE (XPR,IL)
DATA (SURF(1,1),I=1,3)/6HWING ,RHTAIL ,11HWING + IAIL /
GO TO (10,20,30,40,50,60,70,80,90),IND
C *****
10 XY = XE(5) - XF(4)
XX = XE(3) - XF(2)
AW = 2.0*XE(3)*YE(3) - XE(2)*(YE(3)-YE(2))
AV = 2.0*XV*YE(3)
WRITE(6,11)EM,SOUND,RHO,XE(1),XE(4),XE(3),XV,YE(2),YE(3),YE(3),
1YE(3),XX,XV,AW,AT,NWCY,NIY,NWCX,NCCX,NWIX,NCIX,NPY,NPY,NWPX,NCPX
11 FORMAT(1H1//// 3IX,41HAC/NAA MISSILE SUBSONIC AIRLOADS PROGRAM
1 //37X,30HHEIGHT CONDITIONS AND GEOMETRY/1H0//15X, 13HMACH NUMBER
2 =,18.5,4X,16HSPEED OF SOUND =F10.3,4H L/T,4X,4HRHO=,E14.8//1H0/
X54X,4RHWING,18X,
3 4HTAIL///22X,16HLE. STATION (L),2F22.3//22X,16HROOT CHORD. (L),
4 2F22.3// 22X,16HLE. SPAN (L),2F22.3//22X,16HT.E. SPAN (L),
5 2F22.3// 22X,16HTIP CHORD (L),2F22.3//22X,16HTOTAL AREA (L*L)
6 2F22.3//22X,16HSPAN COLL. STA.,119,122,//22X,16HCHORD COLL. STA.
7 119,122//22X,16HCHORD INIG. STA.,119,122//22X,16HSPAN PRES MODES
8 119,122//22X,16HCHORD PRES MODES,119,122)
IF(FMACH(MACH).LE.0.95) GO TO 15
WRITE(6,14)
14 FORMAT(92H A MACH NUMBER GREATER THAN 0.95 HAS BEEN USED-----
10USE CAUTION IN APPLYING CASE RESULTS)
15 IF(NOMIT.EQ.0) RETURN

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SUB77250
SUB77260
SUB77270
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SUB77290
SUB77300
SUB77310
SUB77320
SUB77330
SUB77340
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SUB77360
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SUB77420
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SUB70370
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SUB77800
SUB77810
SUB77820
SUB77830

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WRITE(6,12)(NOH(I),I=1,NOHT) SUB77840
12 FORMAT(1H0,15X,51HTHE SPANWISE COLLOCATION STATION(S) OMITTED ON WSUB77850
1ING,9I5) SUB77860
RETURN SUB77870
C ***** SUB77880
20 NCX = NWCX SUB77890
NIX = NWIX SUB77900
DO 150 NS=1,2 SUB77910
WRITE(6,22)(SURF(I,NS),I=1,2) SUB77920
22 FORMAT(1H1,31X,42HMISSILE SUBSONIC AIRLOADS PROGRAM (CONT-D)/1H / SUB77930
1 25X,39HCOLLOCATION STATION COORDINATES ON THE 2A6/1H0,12H S STSUB77940
2A NO,7X,2HYC,8X,7X,11HXC VALUES--) SUB77950
DO 123 IY=1,NIY SUB77960
YC = WBO*SN*Y(IY) SUB77970
DO 120 IX=1,NCX SUB77980
120 XPR(IX) = WBO*XS(1,NS,IX,IY) SUB77990
123 WRITE(6,124) IY,YC,(XPR(IX),IX=1,NCX) SUB78000
124 FORMAT(1H0,112,5E17.6/(1H ,29X,4E17.6)) SUB78010
WRITE(6,105) (SURF(I,NS),I=1,2) SUB78020
105 FORMAT(1H0,24X,39HINTEGRATION STATION COORDINATES ON THE 2A6/1H0, SUB78030
112H S STA NO,7X,2HYI,8X,7X,11HXI VALUES--) SUB78040
DO 106 IY=1,NIY SUB78050
YI = WBO*SN*YTA(IY) SUB78060
DO 126 IX=1,NIX SUB78070
126 XPR(IX) = WBO*XS(2,NS,IX,IY) SUB78080
106 WRITE(6,124) IY,YI,(XPR(IX),IX=1,NIX) SUB78090
NCX = NCCX SUB78100
NIX = NCIX SUB78110
150 CONTINUE SUB78120
RETURN SUB78130
C ***** SUB78140
30 DO 34 NS = 1,2 SUB78150
WRITE(6,21) IFRQ(IFR),NMODES,EK,EH SUB78160
21 FORMAT(1H1,31X,42HMISSILE SUBSONIC AIRLOADS PROGRAM (CONT-D)//1H /SUB/8170
1 9X,27HOSCILLATORY FREQUENCY (CPS),F12.5,13X,12,17H DEFLECTION MODSUB78180
2ES/1H0,8X,30HREDUCED FREQUENCY (SEMI CHORD),F9.5,14X,23HFREE STREASUB78190
3M MACH NUMBER,F9.3/1H ) SUB78200
WRITE(6,31) IMOD SUB78210
31 FORMAT(34X,34HPRESSURE COEFFICIENTS FOR MODE NO.13//19X,1H11X,10HSUB78220
1R COEFF(I)12X,10H1 COEFF(I) 9X,9HSPAN MODE 3X,10HCHORD MODE,) SUB78230
WRITE(6,32)(SURF(KI,NS),KI=1,2) SUB78240
32 FORMAT(1H0,9X,2A6//) SUB78250
GO TO(2,3),NS SUB78260
2 NL = NWPX SUB78270
ML = NPY SUB78280
IK = 1 SUB78290
GO TO 4. SUB78300
3 NL = NCPX SUB78310
ML = NPY SUB78320
IK = NWPX*NPY+1 SUB78330
4 DO 6 IM = 1,ML SUB78340
DO 6 IN = 1,NL SUB78350
WRITE(6,33) IK,ANN(IK,IMOD),IM,IN SUB78360
33 FORMAT(1H0,119,1P2E22.5,2I13) SUB78370
6 IK = IK + 1 SUB78380
34 CONTINUE SUB78390
RETURN SUB78400
C ***** SUB78410
40 WRITE(6,41) SUB78420
41 FORMAT(1H0,20X,36HERROR IN INPUT DATA (NO TAIL) REQUIRES//,21X,19HSUB78430
1TERMINATION OF CASE) SUB78440

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CALL EXIT SUB78450
C ***** SUB78460
50 WRITE(6,51) SUB78470
51 FORMAT(1H0,20X,63HNUMBER OF COLLOCATION OR INTEGRATION STATIONS OR SUB78480
1 PRESSURE TERMS//21X,25HEXCEEDS ALLOWABLE MAXIMUM//35X,18HCASE ISSUB78490
2 TERMINATED) SUB78500
CALL EXIT SUB78510
C ***** SUB78520
60 WRITE(6,21)FRQ(IFR),NMODES,EK,EM SUB78530
WRITE(6,101) SURF(1,NSURF) SUB78540
101 FORMAT(1H0,27X,45HINPUT MODE SHAPE POLYNOMIAL COEFFICIENTS FOR ,A6SUB78550
1//22X,62HREFERENCED TO THE SURFACE LEADING EDGE-CENTERLINE INTERSESUB78560
2CTION //2X,4HMODE,20X, 7HCOEFFS.) SUB78570
DO 69 L=1,NMODES SUB78580
NTM = NZCO(L,NSURF) SUB78590
WRITE(6,66) L,(CO(L,K,NSURF),K=1,NTM) SUB78600
66 FORMAT(1H0,14,4X,1P7E13.4/(9X,1P7E13.4)) SUB78610
69 CONTINUE SUB78620
RETURN SUB78630
C ***** SUB78640
70 WRITE(6,21)FRQ(IFR),NMODES,EK,EM SUB78650
WRITE(6,35) ALPHA(IMOD) SUB78660
55 FORMAT(24X,47HRMS ERROR OF DOWNWASHES AT COLLOCATION POINTS =,1E13SUB78670
X.6) SUB78680
WRITE(6,36) IMOD SUB78690
56 FORMAT(1H0,23X,57HPRESSURES AND UPWASHES AT COLLOCATION POINTS FORSUB78700
X MODE NO.13) SUB78710
WRITE(6,32)(SURF(L,NSURF),L=1,2) SUB78720
WRITE(6,37) SUB78730
57 FORMAT(3H0,7X,1HX,8X,1HY,9X,8HR P(X,Y),5X,8HI P(X,Y),6X,
1 9HR CH(X,Y),4X,9HI CH(X,Y),6X,9HR DW(X,Y),4X,9HI DW(X,Y))
RETURN SUB78760
C ***** SUB78770
80 WRITE(6,21)FRQ(IFR),NMODES,EK,EM SUB78780
WRITE(6,61) (SURF(L,NSURF),L=1,2) SUB78790
61 FORMAT(35X,23HGENERALIZED FORCES FOR 2A//1H0,6X,4HDEFL,3X,4HLOAD,1SUB78800
10X,9HREAL PART,10X,9HIMAG PART,10X,9HABS. VALUE,10X,11HPHASE ANGLE/SUB78810
2/) SUB78820
DO 78 I=1,NMODES SUB78830
DO 78 J=1,NMODES: SUB78840
IF(NSURF.EQ.3) GO TO 76 SUB78850
G1 = REAL(GFORC(I,J,NSURF)) SUB78860
G2 = AIMAG(GFORC(I,J,NSURF)) SUB78870
GO TO 77 SUB78880
76 G1 = REAL(GFORC(I,J,1)) + REAL(GFORC(I,J,2)) SUB78890
G2 = AIMAG(GFORC(I,J,1)) + AIMAG(GFORC(I,J,2)) SUB78900
KKK=2*NMODES *****
NNN=2*J-1 *****
NNNN=2*J *****
CARDS(I,NNN)=G1 *****
CARDS(I,NNNN)=G2 *****
/7 G3 = SQRT(G1**2+G2**2) SUB78910
G4 = 0.0 SUB78920
IF(G3.NE.0.0) G4 = 57.2957795*ATAN2(G2,G1) SUB78930
WRITE(6,71) I,J,G1,G2,G3,G4 SUB78940
IF(NSURF.NE.3) GO TO 78 *****
IF(I.NE.NMODES) GO TO 78 *****
IF(J.NE.NMODES) GO TO 78 *****
PUNCH 6969, ((CARDS(I,JJ),JJ=1,KKK), I=1,NMODES) *****
6969 FORMAT(1P6F12.5)
71 FORMAT(1H0,19,17.2X,1P3E19.5,0PF16.3,4H DEG)

```



78 CONTINUE  
RETURN

SUB78960  
SUB78970

C \*\*\*\*\* SUB78980

90 WRITE(6,19) XCOLL,YCOLL,PR(IROW,IMOD),C=ASH(IROW,IMOD),  
X DWASH(IROW,IMOD)

SUB78990  
SUB79000

19 FORMAT(1H0,2X,2F9.3,2X,2E13.4,2X,2E13.4,2X,2E13.4)  
RETURN  
END

SUB79010  
SUB79020  
SUB79030

## 4.0 TRANSONIC UNSTEADY AERODYNAMICS PROGRAM

### 4.1 Theoretical Derivation

When the flight speed approaches  $M = 1.0$ , the velocity potential equation can be written as

$$\phi_{yy} + \phi_{zz} = M^2 (2ik\phi_x - k^2\phi) \quad (4.1.1)$$

which is valid if  $k \gg |M-1|$ . The linearized equation is applicable when the lifting surfaces are oscillating rapidly such that non-linear disturbances in the flow do not have time to accumulate.

Equation (4.1.1) is satisfied by a pulsating doublet which produces a velocity potential at  $(x, y, z)$  given by

$$\phi_D = \frac{1}{2} \frac{k(z-\zeta)}{(x-\xi)^2} \exp \left\{ -1/2 ik \left[ (x-\xi) + \frac{(y-\eta)^2 + (z-\zeta)^2}{(x-\xi)} \right] \right\} \quad (4.1.2)$$

where the doublet is positioned at  $(\xi, \eta, \zeta)$ . The doublet has no influence at points upstream of the line  $x = \xi$  and, consequently, the potential is zero in that region.

A solution to equation (4.1.1) may be obtained by superposition. This solution will be represented in the form

$$\phi(x, y, z) = \iint \phi(\xi, \eta) \phi_D(x, y, z, \xi, \eta, 0) d\xi d\eta \quad (4.1.3)$$

where  $\phi(\xi, \eta)$  is the doublet strength of point  $(\xi, \eta)$ .

To compute the velocity potential distribution, the wing, wake and control surface is divided into a lattice of square boxes as shown in Figure 4.1.1. The potential function is replaced by a set of point values at the box centers. The potential function and downwash value is assumed constant over each box and equal to the central value.

The problem reduces to imposing boundary conditions and determining the doublet strength for each box to satisfy the boundary conditions. The boundary value problem becomes

#### 1. Tangential Flow Condition

$$w(x, y)_{\text{wing}} = \iint_{\text{wing}} \phi(\xi, \eta) \lim_{z \rightarrow 0} \frac{\partial \phi_D}{\partial z} d\xi d\eta \quad (4.1.4)$$

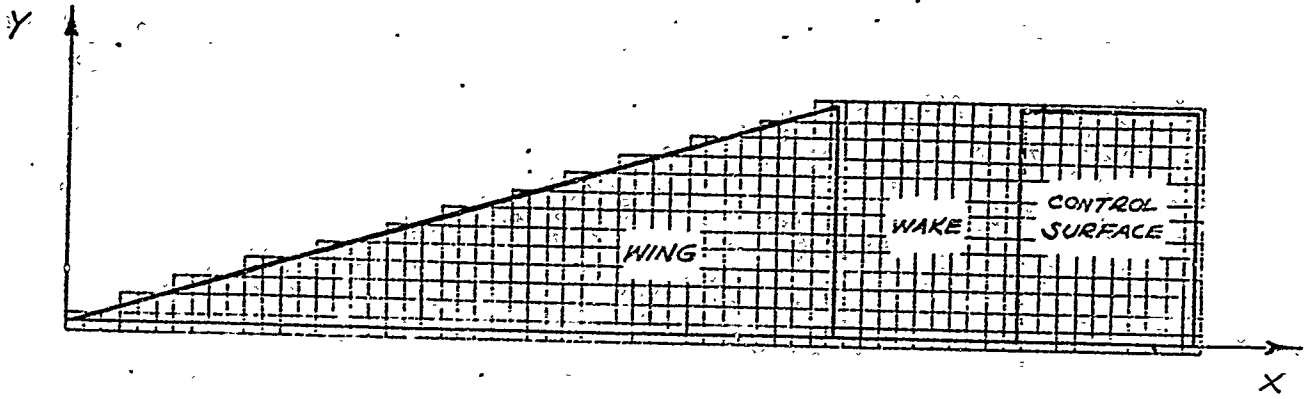


Figure 4.1.1 Sonic Box Overlay Pattern

$$w(x,y)_{\text{control surface}} = \iint_{\text{wing + wake + control surface}} \phi(\xi, \eta) \lim_{z \rightarrow 0} \frac{\partial \phi}{\partial z} d\xi d\eta \quad (4.1.5)$$

## 2. Zero Pressure Jump in Wake

$$\frac{\partial \phi}{\partial x} - ik\phi = 0 \quad (4.1.6)$$

Equation (4.1.6) is an ordinary homogeneous differential equation subjected to the condition  $\phi$  is equal to the value of the velocity potential at the wing trailing edge for  $x = x_{\text{wing t.e.}}$ . This gives the solution

$$\phi_{\text{wake}} = \phi_{\text{wing t.e.}} e^{-ik(x-x_{\text{wing t.e.}})} \quad (4.1.7)$$

Equations (4.1.4), and (4.1.5) and (4.1.7) form a system of equations from which the point values of the potential functions can be found at the box centers. The pressure distribution is then determined from the relationship

$$\Delta P(x,y) = \frac{1}{2} \rho U^2 (2 \frac{\partial \phi}{\partial x} + 2ik\phi) \quad (4.1.8)$$

and the generalized forces are found from equation (2.0.1).

## 4.2 PROGRAM DESCRIPTION

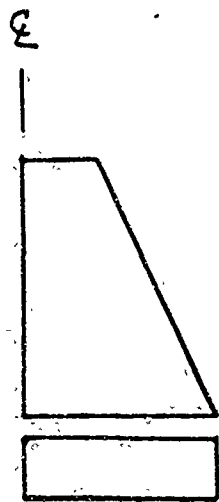
The Sonic Unsteady Aerodynamics Program calculates generalized forces for up to 10 deformation modes. The computer solution is based upon the Mach box technique. The various configurations which can be analyzed are shown in Figure 4.2.1 and Table 4.2.2. The analysis includes interaction effects between tandem surfaces and wake effects on the trailing surface. Single surfaces may be analyzed by inputting a second surface with a zero chord length.

The transonic box method calculates the unsteady potentials from which the pressure distributions may be obtained for arbitrary modes of surface motion. The method used was suggested by the successes of the supersonic box methods of Pines and others, Reference 11. The potential is generated by a doublet distribution rather than by a source distribution because the latter method would involve diaphragm regions of infinite extent, whereas the doublet distribution is confined to the wing and its wake. As with the subsonic problem, the differential equation solution is an integral equation. The integral equation is approximated numerically by a matrix equation so that the basic step in the box method is the solution of the system of simultaneous equations which determine a set of values of potential on the surface from a corresponding array of upwash values. The solution procedure obtains the velocity potential over the surface one spanwise row of boxes at a time until the trailing edge row is completed. The numerical complexity is not increased, however, by a large number of box rows over the configuration because the influence coming from more than 15 rows away has been found to be negligible. The results are valid for high reduced frequency,  $k$ , such that  $k \gg |M - 1|$  where  $M$  is the Mach number.

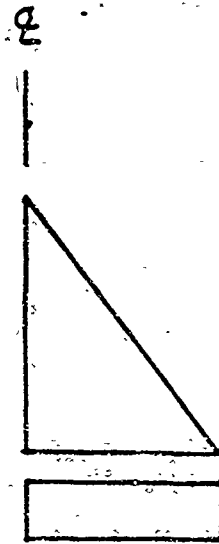
The solution for the generalized aerodynamic forces requires the input of the deformation modes due to vibration. The program considers the modes to be expressed as analytic functions of the form:

$$w(x, y) = \sum_{m=0}^N \sum_{n=0}^m C_{(n-m), m} x^{(n-m)} y^m$$

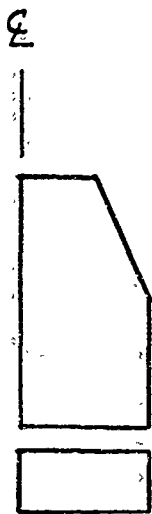
To meet this requirement only the coefficients "c" are required as input into the program. These coefficients can be obtained in several ways, the most common way is to surface fit the modes by the least-square technique.



TRAPEZOIDAL



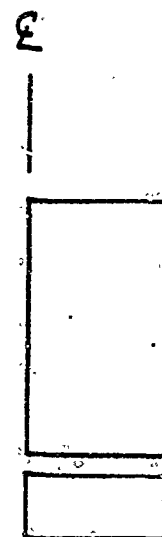
DELTA



TRAPEZOIDAL  
(CROPPED)



DELTA  
(CROPPED)



RECTANGULAR

FIGURE 4.2.1  
TANDEM COPLANAR CONFIGURATIONS AT SONIC  
MACH. NUMBER.

TABLE 4.2.2 OPTIONAL CONFIGURATIONS

CONFIGURATION	CHORDWISE COORDINATE	SPANWISE COORDINATE
RECTANGULAR	$X(1) = 0.0$	$Y(1) = 0.0$
	$X(2) = 0.0$	$Y(2) = 0.0$
	$X(3) > 0.0$	$Y(3) > 0.0$
	$X(4) \geq X(3)$	
	$X(5) \geq X(4)$	
DELTA	$X(1) = 0.0$	$Y(1) = 0.0$
	$X(2) > 0.0$	$Y(2) = 0.0$
	$X(3) = X(2)$	$Y(3) > 0.0$
	$X(4) \geq X(3)$	
	$X(5) \geq X(4)$	
TRAPEZOIDAL	$X(1) = 0.0$	$Y(1) = 0.0$
	$X(2) > 0.0$	$Y(2) > 0.0$
	$X(3) = X(2)$	$Y(3) > Y(2)$
	$X(4) \geq X(3)$	
	$X(5) \geq X(4)$	
TRAPEZOIDAL (CROPPED)	$X(1) = 0.0$	$Y(1) = 0.0$
	$X(2) > X(1)$	$Y(2) > 0.0$
	$X(3) > X(2)$	$Y(3) > Y(2)$
	$X(4) \geq X(3)$	
	$X(5) \geq X(4)$	
DELTA (CROPPED)	$X(1) = 0.0$	$Y(1) = 0.0$
	$X(2) > 0.0$	$Y(2) = 0.0$
	$X(3) > X(2)$	$Y(3) > Y(2)$
	$X(4) \geq X(3)$	
	$X(5) \geq X(4)$	

### 4.3 INPJI INSTRUCTIONS

Instructions for preparing input data for the transonic computer program are presented here. The field location and format for each quantity is specified. Any set of units may be used for geometric dimensions and acoustic velocity as long as they are consistent, e.g., if inches is used for length, then the acoustic velocity must have dimensions of inches per second. The required data and the sequence in which the information is entered is as follows:

#### 1. Streamwise Coordinates (6E12.5 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	X(1)	X(2)	X(3)	X(4)	X(5)	
Item	(1)	(2)	(3)	(4)	(5)	

- (1) X(1) Wing root leading edge coordinate (See Figure 4.3.1)
- (2) X(2) Wing tip leading edge coordinate
- (3) X(3) Wing trailing edge coordinate
- (4) X(4) Control surface leading edge coordinate
- (5) X(5) Control surface trailing edge coordinate

A single surface, the wing, may be analyzed by setting X(4) and X(5) equal to X(3). The various configurations are generated as shown in Table 4.2.1. The origin for the planform and AIC station coordinates must be at the leading edge root of the wing, therefore X(1) and Y(1), described below, must always be zero.

#### 2. Spanwise Coordinates and Acoustic Velocity (6E12.5 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	Y(1)	Y(2)	Y(3)	SOUND	RHO	
Item	(1)	(2)	(3)	(4)	(5)	

- (1) Y(1) Wing root spanwise coordinate
- (2) Y(2) Wing leading edge spanwise coordinate
- (3) Y(3) Wing (and control surface) tip spanwise coordinate
- (4) SOUND Speed of sound at altitude for which analysis is performed
- (5) RHO density of fluid \* 1000.0 (M./L<sup>3</sup>)



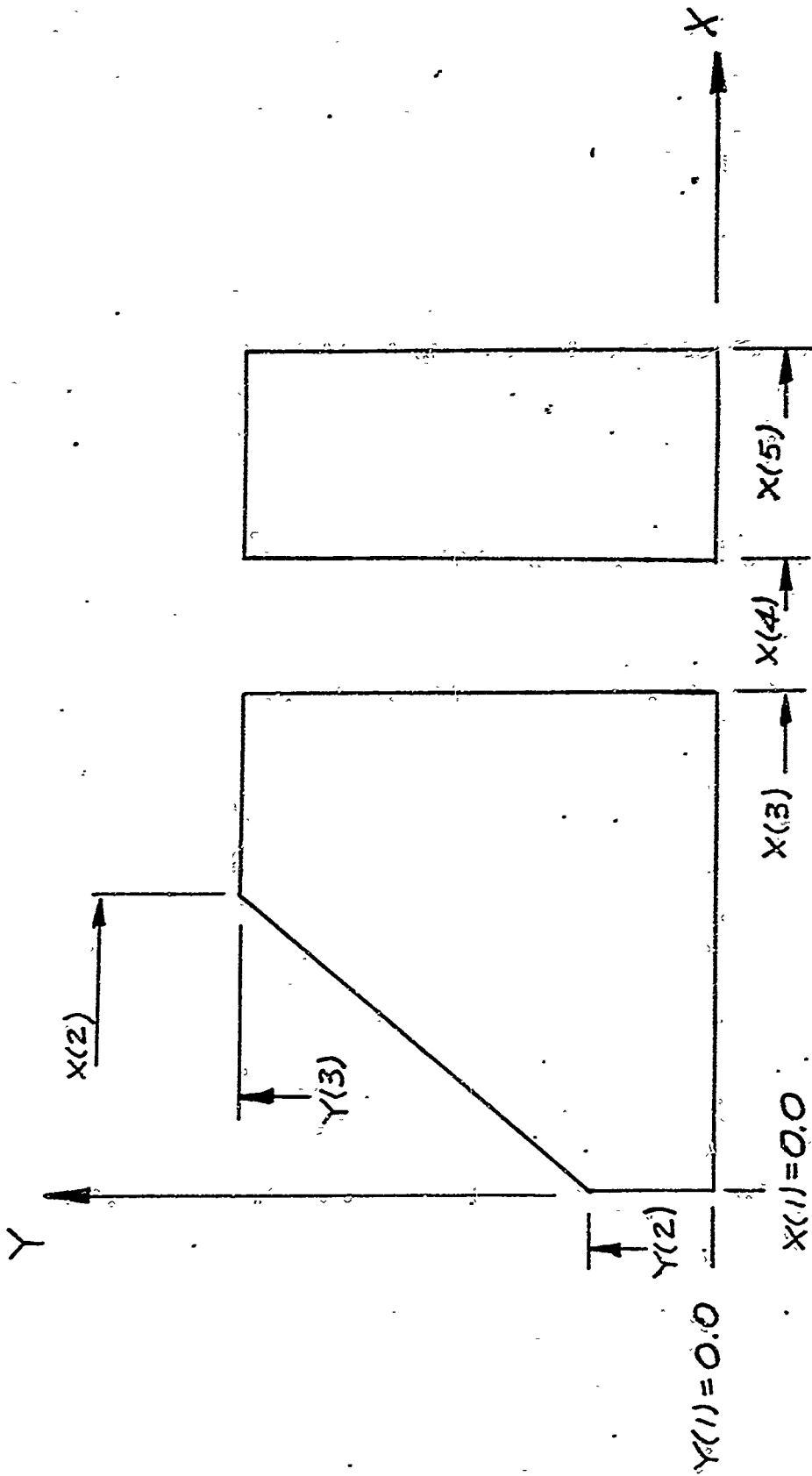


FIGURE 4.3.1  
GEOMETRY DESCRIPTION

3. General Information (6I12 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	NMACH	NFREQ	NMODES	NBW	LVPIC	LSSVP
Item	(1)	(2)	(3)	(4)	(5)	(6)

- (1) NMACH Number of Mach numbers (max 6)
- (2) NFREQ Number of input frequencies (max 10)
- (3) NMODES Number of input modes (max 10)
- (4) NBW Number of chordwise wing boxes (max 10)
- (5) LVPIC Print velocity potential influence coefficients; 0 ~ No, 1 ~ Yes
- (6) LSSVP Print upwashes; 0 ~ No, 1 ~ Yes

4. Mach Numbers (6E12.5 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	FMACH(1)	FMACH(2)	FMACH(3)	FMACH(4)	FMACH(5)	FMACH(6)
Item	(1)	(2)	(3)	(4)	(5)	(6)

- (1) FMACH(i) Mach numbers for which the analysis is to be performed.

5. Frequency (6E12.5 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	FREQ(1)	FREQ(2)	FREQ(3)	FREQ(4)	FREQ(5)	FREQ(6)
Item	(1)	(2)	(3)	(4)	(5)	(6)

- (1) FREQ Frequencies for which the analysis is to be performed. Continue on next card for FREQ(i) 6.

6. Deformation Modes. Repeat the Following Cards NMODES Times

(6I12) Format

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	NTM1(i)	NFI				
Item	(1)	(2)				

- (1) NTM1(i) Number of deformation mode coefficients for the wing, mode i
  - (2) NFI Compute generalize forces; 0 ~ No, 1 ~ Yes
- If NFI = 0 the program will compute the VPIC's and stop.

(6E12.5) Format

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	CØ(1)	CØ(2)	CØ(3)	CØ(4)	CØ(5)	CØ(6)
Item	(1)	(2)	(3)	(4)	(5)	(6)

(1) CØ(1)

i = 1, NTM deformation polynomial coefficients to be input in the following order: 0,0; 1,0; 0,1; 2,0; 1,1; 0,2; 3,0; where the first integer is the power of "x" and the second is the power of "y". Continue on successive cards until all polynomial coefficients are input.

(6I12) Format

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	NIM	NFI				
Item	(1)	(2)				

(1) NIM2(1)

Number of deformation mode coefficients for the control surface, mode (i)

(2) NFI

Compute generalized forces; 0 ~ No; 1 ~ Yes. If NFI = 0, the program will compute the VPIC's and stop.

(6E12.5) Format

Column	1-12	13-24	25-36	37-48	49-60	
Name	CØ(1)	CØ(2)	CØ(3)	CØ(4)	CØ(5)	
Item	(1)	(2)	(3)	(4)	(5)	

CØ(i)

i - 1, NTM deformation polynomial coefficients to be input in the following order: 0,0; 1,0; 0,1; 2,0; 1,1; 0,2; 3,0; etc. where the first integer is the power of "x" and the second is the power of "y". Continue on successive cards until all polynomial coefficients are input.

#### 4.4 SAMPLE PROBLEM

The generalized forces are calculated for the configuration below. The flight parameters and pertinent input data are presented on the first page of the computer print out.

The coefficients of the deformation modes for the forward surface are shown on the third page of the computer print out, and for the aft surface on the fifth page of the computer print out.

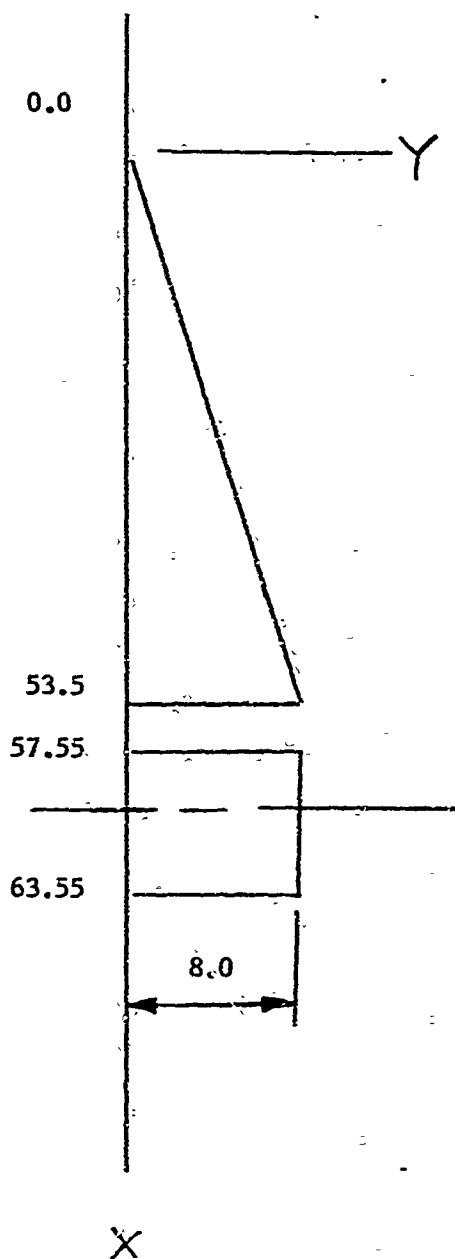


FIGURE 4.4.1

HAC/NAA MISSILE TRANSONIC AIRLOADS PROGRAM

FLIGHT CONDITIONS AND GEOMETRY

MACH NUMBER = 1.00000      SPEED OF SOUND = 13392.000 L/T      RHQ=0.11460000E-06

	WING	TAIL
L.E. STATION (L)	0.	57.550
ROOT CHORD (L)	53.500	6.000
L.E. SPAN (L)	0.	8.000
T.E. SPAN (L)	8.000	6.000
TIP CHORD (L)	0.	6.000
TOTAL AREA (L+L)	428.000	96.000
CHORDWISE BOXES	49	5
SPANWISE BOXES	7	7

TOTAL CHORDWISE BOXES = 53      BOX CHORD = 1.20225E 00 L      BOX SPAN = 1.20225E 00 L



MISSILE TRANSONIC AIRLOADS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (GPS) 110.00000 53 BOXES IN CHORD DIRECTION  
 REDUCED FREQUENCY (SEMI CHORD) 1.38055 FREE STREAM MACH NUMBER 1.000

INPUT MODE SHAPE POLYNOMIAL COEFFICIENTS FOR WING  
 REFERENCED TO THE SURFACE LEADING EDGE-CENTERLINE INTERSECTION

MODE	COEFFS,
1	4.6476E-03 2.1714E 00 -1.1796E-02 1.1765E-01 -2.3426E 00 1.3893E-03 -5.7624E-02 7.9094E-01 -2.5125E 00 -4.5847E-05 2.4591E-03 -3.5940E-02 1.4666E-01 -9.2425E-02 4.4647E-07 -2.7338E-05 4.4296E-04 -2.5737E-03 7.8341E-03 -1.7714E-02
2	1.4724E-03 -1.5229E-02 1.3060E-04 1.4047E-03 2.5887E-02 -1.7714E-09 1.0010E-03 -1.8106E-02 -5.8051E-08 1.4540E-05 -1.7126E-04 1.5541E-03 1.0317E-09 -1.6695E-07 2.2909E-06 -1.3876E-05 -3.8650E-05 2.1062E-04
3	1.8600E-03 -4.0090E-01 2.8499E-03 5.4255E-02 5.2506E-01 -3.2033E-04 1.7053E-01 5.3718E-01 1.0353E-05 -6.0834E-04 7.9328E-03 -3.2827E-02 -1.0013E-07 6.6433E-06 -9.9828E-05 5.9923E-04 -1.9292E-03 4.73643E-03
4	6.2155E-03 -1.0847E 00 2.4746E-03 9.3898E-02 4.8655E-01 -2.3470E-04 1.1654E-01 3.2703E-01 7.1836E-06 -2.3984E-04 5.1428E-03 -2.1053E-02 6.7781E-08 3.0791E-06 -6.1616E-05 3.4012E-04 -8.7292E-04 1.4206E-03
5	9.1320E-04 1.8393E-03 -6.5138E-04 1.7097E-02 -8.4167E-02 6.8571E-05 3.8491E-02 -1.3252E-01 2.1796E-06 1.3006E-04 -1.7763E-03 7.4320E-03 2.0953E-08 -1.3987E-06 2.1637E-05 -1.2205E-04 3.2906E-04 -7.4633E-04

MISSILE TRANSONIC AIRLOADS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (CPS) 110.00000 53 BOXES IN CHORD DIRECTION  
 REDUCED FREQUENCY (SEMI CHORD) 1.38055 FREE STREAM MACH NUMBER 1.000

GENERALIZED FORCES FOR WING

DEFL	LOAD	REAL PART	IMAG. PART	ABS VALUE	PHASE ANGLE
1	1	3.16858E 02	-1.37658E 02	3.4549E 02	-23.482 DEG
1	2	-5.52591E-01	2.6677E 00	2.72440E 00	101.703 DEG
1	3	-5.62170E 01	2.07533E 01	5.99254E 01	159.738 DEG
1	4	-8.10722E 00	3.26216E 01	3.36139E 01	103.957 DEG
1	5	1.18660E 01	-6.65916E 00	1.34328E 01	-28.719 DEG
2	1	-2.44226E 00	2.26683E 00	3.32234E 00	137.133 DEG
2	2	8.84216E-01	-2.39821E-01	9.16162E-01	-15.175 DEG
2	3	-5.69430E 00	2.64395E 00	6.27818E 00	155.094 DEG
2	4	-1.55191E 00	-2.19162E 00	2.68545E 00	-125.303 DEG
2	5	2.87546E-01	-2.50006E-02	2.88631E-01	-4.969 DEG
3	1	-6.65830E 01	2.52397E 01	7.12063E 01	159.240 DEG
3	2	-7.04967E 00	-1.50816E 00	7.20919E 00	-167.923 DEG
3	3	7.38453E 01	-1.35683E 01	7.50815E 01	-10.411 DEG
3	4	2.91514E 01	1.99798E 01	3.53412E 01	34.426 DEG
3	5	-7.90048E 00	-2.3443E-01	7.90395E 00	-178.300 DEG
4	1	1.59553E 01	2.36006E 01	2.86879E 01	55.939 DEG
4	2	-2.71097E 00	3.8801E 00	4.73326E 00	124.942 DEG
4	3	3.77450E 00	-3.69283E 01	3.71207E 01	-84.164 DEG
4	4	-2.14405E 01	-1.64663E 01	2.70339E 01	-112.476 DEG
4	5	2.92952E 00	5.23504E 00	6.02850E 00	60.271 DEG
5	1	6.76158E 00	-7.51507E 00	1.01092E 01	-48.021 DEG
5	2	5.48742E-01	-3.20824E-01	6.35646E-01	-30.313 DEG
5	3	-4.27173E 00	4.95884E 00	6.54506E 00	130.743 DEG
5	4	4.30316E 00	2.14755E 00	4.80928E 00	26.522 DEG
5	5	1.87838E-01	-9.0241E-01	9.2178E-01	-78.242 DEG



MISSILE TRANSONIC AIRLOADS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (CPS) 110.00000 53 BOXES IN CHORD DIRECTION  
 REDUCED FREQUENCY (SEMI CHORD) 1.38055 FREE STREAM MACH NUMBER 1.000

INPUT MODE SHAPE POLYNOMIAL COEFFICIENTS FOR TAIL  
 REFERENCED TO THE SURFACE LEADING EDGE-CENTERLINE INTERSECTION

COEFFS.

MODE	COEFFS.	COEFFS.	COEFFS.	COEFFS.	COEFFS.	COEFFS.	COEFFS.	COEFFS.	COEFFS.	COEFFS.	COEFFS.	COEFFS.
1	-1.0091E-00	3.6669E-02	2.0342E-02	2.5379E-02	2.2663E-03	-6.3951E-03	-3.9767E-03					
	-2.0287E-03	9.8702E-04	1.1172E-03	1.9252E-04	3.7068E-04	-2.0327E-04	1.7562E-06					
	-6.7077E-05											
2	-1.2752E-01	8.2139E-02	-8.3996E-02	-1.7451E-02	-2.6948E-02	-2.0262E-02	1.2913E-03					
	7.7354E-03	1.6668E-03	2.9726E-03	3.1356E-05	-2.7508E-04	-5.4809E-04	1.6180E-05					
	-1.0213E-04											
3	-8.3787E-02	4.9086E-02	-8.5200E-03	-1.6733E-02	-1.4954E-03	-1.2620E-03	4.0742E-03					
	1.5179E-05	2.7897E-04	2.8296E-04	-3.1325E-04	4.5623E-06	-6.0549E-07	-1.7126E-05					
	-1.9476E-05											
4	-7.2257E-03	8.2141E-03	-4.9131E-03	-1.1390E-03	-2.5330E-04	7.4449E-04	9.5326E-05					
	1.7613E-05	-3.0224E-06	-2.4853E-04	1.6233E-07	1.5745E-05	-2.1877E-05	1.2826E-05					
	1.7159E-05											
5	5.8014E-01	1.5199E-01	2.4793E-02	8.4246E-02	5.0903E-03	-1.8510E-02	-1.9336E-02					
	-9.6255E-05	4.2392E-05	3.4434E-03	1.3989E-03	-1.1667E-04	5.2220E-05	-1.5344E-05					
	-2.0522E-04											

MISSILE TRANSONIC AIRLOADS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (CPS) 110.0000 53 BOXES IN CHORD DIRECTION  
 REDUCED FREQUENCY (SEMI CHORD) 1.38055 FREE STREAM MACH NUMBER 1.000

GENERALIZED FORCES FOR TAIL

DEFL	LOAD	REAL PART	IMAG PART	ABS VALUE	PHASE ANGLE
1	1	3.20570E 02	-1.64106E 02	3.60133E 02	-27.109 DEG
1	2	1.78757E 02	-1.52739E 02	2.35104E 02	-47.507 DEG
1	3	1.35618E 02	-3.12913E 01	1.39181E 02	-12.993 DEG
1	4	1.40816E 02	-6.58142E 01	1.55437E 02	-25.050 DEG
1	5	1.03474E 03	-7.16951E 01	1.03722E 03	-3.964 DEG
2	1	1.65340E 02	-8.80348E 01	1.87316E 02	-28.033 DEG
2	2	1.24794E 02	-9.42639E 01	1.56393E 02	-37.065 DEG
2	3	8.75103E 01	-1.55398E 01	8.86793E 01	-10.069 DEG
2	4	9.66705E 01	-3.27417E 01	1.02045E 02	-18.711 DEG
2	5	5.96996E 02	6.51462E 00	5.97032E 02	0.625 DEG
3	1	1.17162E 01	-2.23677E 01	2.52681E 01	-67.376 DEG
3	2	1.64673E 00	-1.09465E 01	1.10696E 01	-81.445 DEG
3	3	1.07777E 01	-6.32983E 00	1.24990E 01	-30.426 DEG
3	4	1.24434E 01	-6.77398E 00	1.41673E 01	-28.560 DEG
3	5	8.18177E 01	-4.11626E 01	9.19887E 01	-26.707 DEG
4	1	1.29545E 00	-4.67734E 00	4.85333E 00	-74.518 DEG
4	2	8.41320E 01	-2.50315E 00	2.64076E 00	-71.422 DEG
4	3	2.58365E 00	-1.28241E 00	2.88441E 00	-26.398 DEG
4	4	3.05965E 00	-1.28912E 00	3.32013E 00	-22.847 DEG
4	5	1.71697E 01	-7.84607E 00	1.88775E 01	-24.559 DEG
5	1	1.23287E 02	-1.61959E 02	2.03545E 02	-127.279 DEG
5	2	1.78991E 02	5.78304E 00	1.79084E 02	178.149 DEG
5	3	-2.08674E 00	-5.89137E 01	5.89507E 01	-92.029 DEG
5	4	3.43775E 00	-3.42119E 01	3.4382E 01	-84.262 DEG
5	5	1.29038E 02	-5.72898E 02	5.87251E 02	-77.507 DEG

MISSILE TRANSONIC AIRLOADS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (CPS) 110.00000 53 BOXES IN CHORD DIRECTION  
 REDUCED FREQUENCY (SEMI CHORD): 1.38059 FREE STREAM MACH NUMBER 1.000

GENERALIZED FORCES FOR WING + TAIL

DIFFL	LOAD	REAL PART	IMAG PART	ABS VALUE	PHASE ANGLE
1	1	6.37428E 02	-3.01764E 02	7.05249E 02	-25.333 DEG
1	2	1.78204E 02	-1.50041E 02	2.32957E 02	-40.096 DEG
1	3	7.94010E 01	-1.05381E 01	8.00972E 01	-7.560 DEG
1	4	1.32709E 02	-3.31926E 01	1.36797E 02	-14.042 DEG
1	5	1.04641E 03	-7.83542E 01	1.04934E 03	-4.282 DEG
2	1	1.62898E 02	-8.57680E 01	1.84097E 02	-27.767 DEG
2	2	1.25678E 02	-9.45007E 01	1.57243E 02	-36.940 DEG
2	3	8.18160E 01	-1.28959E 01	8.28261E 01	-8.957 DEG
2	4	9.51186E 01	-3.49333E 01	1.01331E 02	-20.166 DEG
2	5	5.97284E 02	6.48962E 00	5.97319E 02	0.623 DEG
3	1	5.48668E 01	2.85198E 00	5.49409E 01	177.024 DEG
3	2	5.40294E 00	-1.24546E 01	1.35761E 01	-113.452 DEG
3	3	8.46230E 01	-1.98982E 01	8.69310E 01	-13.232 DEG
3	4	4.15948E 01	1.32068E 01	4.36411E 01	17.615 DEG
3	5	7.39172E 01	-4.13970E 01	8.47200E 01	-29.251 DEG
4	1	1.72507E 01	1.89236E 01	2.56064E 01	47.648 DEG
4	2	1.86965E 00	1.37685E 00	2.32192E 00	143.631 DEG
4	3	6.35815E 00	-3.82107E 01	3.87361E 01	-80.553 DEG
4	4	1.63808E 01	-1.77554E 01	2.55560E 01	-135.992 DEG
4	5	2.01593E 01	-2.61103E 00	2.03276E 01	-7.380 DEG
5	1	1.15525E 02	-1.69474E 02	2.05669E 02	-124.511 DEG
5	2	1.78442E 02	5.46221E 00	1.78526E 02	178.247 DEG
5	3	6.35847E 00	-5.39549E 01	5.43263E 01	-96.721 DEG
5	4	7.74090E 00	-3.20643E 01	3.29855E 01	-76.427 DEG
5	5	1.29226E 02	-5.73801E 02	5.88172E 02	-77.309 DEG

4.5 PROGRAM LISTING

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* FORTRAN NLIST00,DECK SON70030
CISIS CSIS SON70050
BLOCK DATA SON70060
COMPLEX CZERO,PHI,PHITE,DPHI,SPHI SON70070
COMMON/C3/C(10,25,2),N1(10,2),NF(10,2),NTMAX(2),FN(28),DXE(6),TP SON70080
COMMON/C7/CZERO,PHI,PHITE,DPHI,SPHI SON70090
COMMON/C8/R00 SON70100
DATA CZERO/(0.0,0.0)/,TP1/6.2831853/,FN/0.,1.,0.,2.,1.,0.,3.,2., SON70110
1 1.,0.,4.,3.,2.,1.,0.,5.,4.,3.,2.,1.,0.,6.,5.,4.,3.,2.,1.,0./ SON70120
END SON70130
* FORTRAN NLIST00,D-CK SON70140
CPAIN MAIN SON70160
COMPLEX VPI,DS,DJ,0,PHIW,CK,CZERO,PHI,PHITE,DPHI,SPHI,ASU,EXF SON70170
DIMENSION ASQ(40,40) SON70180
COMMON/C1/K:OX(2000),XF(5),YE(3),AR(3),X1,X2,X3,X4,Y1,Y2,BETA,NBS SON70190
COMMON/C2/AN,MACI,FACH(6),NREQ,FREQ(10),NMODE,NSURF,LVPIC,LSSVP SON70200
COMMON/C3/C(10,25,2),N1(10,2),NF(10,2),NTMAX(2),FN(28),DXE(6),TP SON70210
COMMON/C4/VPI(20,15),DS(2000),DQ(28,2),Q(10,10,3),PHIW(50),CK(40) SON70220
COMMON/C5/MOB(100),HBL(100),FC,IFR,XL,NS,NIM,K,J,QR,QI,QAB,QAN SON70230
COMMON/C6/X,Y,DX,DY,EN,EK,EKB,EKR,NP,PP,NB,KBOX,KODE,MODE,NBW,NBT SON70240
COMMON/C7/CZERO,PHI,PHITE,DPHI,SPHI SON70250
COMMON/C8/R00 SON70260
1 CALL MAIN SON70270
DO 3000 MACI=1,MACI SON70280
FR = FACH(MACI) SON70290
IF(ABS(EN-1.0).GT.0.05) GO TO 1000 SON70300
CALL CDEF SON70310
CALL POUT(1) SON70320
TPU=TP1/(AS*F1) SON70330
RFR = FR SON70340
DO 900 IFR =1,NREQ SON70350
FK=FRFO(IFR)*TPU SON70360
IF(FK.EQ.0.) GO TO 900 SON70370
FRF =FK*RFI SON70380
FRD =FK*X1/2.0 SON70390
CALL POUT2H SON70400
IF(LVPIC.NE.0) CALL POUT(2) SON70410
ARG=FK*FX SON70420
EXF=CMPLX(COS(ARG),-SIN(ARG)) SON70430
DO 500 MODE=1,NMODE SON70440
DO 10 J=1,5 SON70450
10 DQ(J,1)=CZERO SON70460
IF(MODE,1).EQ.0) GO TO 210 SON70470
X=0.5*OX SON70480
NR=J SON70490
IF(LSSVP.NE.0) CALL POUT(3) SON70500
DO 200 NP=1,NR SON70510
NR=NOR(NP) SON70520
Y=0.0 SON70530
KODE = KBOX(NR) SON70540
NS =1 SON70550
GO TO (12,11,12,11,11,120),KODE SON70560
11 NS =2 SON70570
12 DO 20 MP=1, NR SON70580
SPHI = CZERO SON70600
IF(MP.GT.1) CALL PHIR SON70610
CALL WASH SON70620
CK(MP)=DS(NR) SON70630
DS(MP) = DS(NR) - SPHI SON70640
Y = Y+BY SON70650

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20 NB = NB+1
   NB = NB-MB
   DO 30 IU=1,MB
   DO 30 JU=1,MB
   IJU = IABS(10-JU)+1
25 ASQ(IU,JU) = VPIC(IJU,1)
   IF(JU.FO.1) GO TO 30
   IJU=IU+JU-1
   ASQ(IU,JU)=ASQ(IU,JU)+VPIC(IJU,1)
30 CONTINUE
   ISQ = MSIMEC(40,MB,1,ASQ,DS(NB))
   IF(1SQ.FO.1) GO TO 39
   CALL POUT(8)
   GO TO 900
39 CONTINUE
   Y = 0.0
   IF(OP.NE.1) GO TO 50
   DO 45 MP=1,MB
45 DS(MP) = DS(MP)*2.0*3.1415927
50 CONTINUE
   IF(KODE.NE.4) GO TO 80
   DO 60 MP=1,MB
   DS(MP) = PHIW(MP)*(DS(NB)-PHIW(MP))*2.0*3.1415927
60 NB=MB+1
   NB=NB-MB
80 CONTINUE
   DO 100 MP=1,MB
   IF(KODE.EQ.3) PHIW(MP)=DS(NB)*EXF
   IF(OP.FO.NBOX-1) PHIW(MP)=DS(NB)
   PHIEF = DS(NB)
   IF(MP.FO.NBOX) PHIEF = PHIEF+(PHIEF-PHIW(MP))*DXE(5)
   PHI = DS(NB)
   IF(ISSVP.NE.0) CALL POUT(4)
   CALL DQIJ
   NB = NB + 1
100 Y=Y+DY
   GO TO 200
120 DO 130 MP=1,MB
   DS(MP)=PHIW(MP)
   PHIF(MP) = EXF*PHIW(MP)
   CK(MP)=CZERO
   IF(ISSVP.NE.0) CALL POUT(4)
130 NB = NB+1
200 X = X+DX
210 DO 400 MO = 3,4MODE
   DO 300 NS=1,NSURF
   Q(MODE,MO,NS)=CZERO
   NTM=NT(MO,NS)
   DO 300 N=1,IM
300 Q(MODE,MO,NS)=Q(MODE,MO,NS)+CU(MO,N,NS)*DQ(N,NS)
   Q(MODE,MO,3) = CZERO
400 Q(MODE,MO,3)=Q(MODE,MO,1)+Q(MODE,MO,2)
500 CONTINUE
   DO 800 NS=1,3
   CALL POUT(6)
   DO 700 J=1,MODE
   DO 700 K=1,MODE
   QR = FG*REAL(Q(K,J,NS))
   QI = FG*AIMAG(Q(K,J,NS))
   CAP=SQR(QI**2+QR**2)

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SON71270

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      QAN=0.0
      IF (QAB.NE.0.0) QAN=57.29578*ATAN2(QI,QR)
700  CALL PCUL(7)
      IF(NSURF.EQ.1) GO TO 900
800  CONTINUE
900  CONTINUE
1000 CONTINUE
      GO TO 1
      END
*      FORTRAN NLSTOU,DECK
CHAIN      DAIN
SUBROUTINE DAIN
COMMON/C1/KNOX(2000),XE(5),YE(3),AR(3),X1,X2,X3,X4,Y1,Y2,BETA,NBS
COMMON/C2/AS,FMACH,FMACH(6),NFREQ,FREQ(10),NMODE,NSURF,LVPIC,LSSVP
COMMON/C3/CI(10,28,2),NI(10,2),NF(10,2),NIMAX(2),FN(28),DXE(6),TPI
COMMON/C6/X,Y,DX,DY,EM,EK,EKB,EKR,NP,PP,NB,NBOX,KODE,MODE,NBW,NBT
COMMON/C8/RHO
      READ(5,11) (XF(I),I=1,5)
      READ(5,11) (YE(I),I=1,3),AS,RHO
      RHO = RHO/100.
      READ(5,12) FMACH,NFREQ,NMODE,NBW,LVPIC,LSSVP
      READ(5,11) (FMACH(I),I=1,NMACH)
      READ(5,11) (FREQ(I),I=1,NFREQ)
      NSURF=2
      IF(YF(4).LT.XF(5)) GO TO 10
      NSURF=1
      XF(4)=XL(3)
      XF(5)=XE(3)
10  NIMAX(1)=0
      NIMAX(2)=0
      DO 30 MODE=1,NMODE
      DO 30 I=1,NSURF
      DO 20 J=1,2
20  CO(MODE,J,1)=0.
      READ(5,12) TM,NFI
      NI(MODE,I)=TM
      NIMAX(I)=MAX0(NIMAX(I),NTM)
      NF(MODE,I)=FI
30  READ(5,11) (CO(MODE,J,1),J=1,NTM)
11  FORMAT(6E12.8)
12  FORMAT(6I12)
      RETURN
      END
*      FORTRAN NLSTOU,DECK
CCCCF      CODE
SUBROUTINE CCF
COMMON/C1/KNOX(2000),XF(5),YE(3),AR(3),X1,X2,X3,X4,Y1,Y2,BETA,NBS
COMMON/C2/AS,FMACH,FMACH(6),NFREQ,FREQ(10),NMODE,NSURF,LVPIC,LSSVP
COMMON/C3/CI(10,28,2),NI(10,2),NF(10,2),NIMAX(2),FN(28),DXE(6),TPI
COMMON/C5/MR(100),NBL(100),FU,IFR,XL,NS,NTM,K,J,QR,QI,QAB,QAN
COMMON/C6/X,Y,DX,DY,EM,EK,EKB,EKR,NP,PP,NB,NBOX,KODE,MODE,NBW,NBT
COMMON/C8/RHO
      BETA = EM
      X1 = XF(3) - XF(1)
      X2 = XF(3) - XF(2)
      X3 = XE(4) - XF(1)
      X4 = XF(5) - XF(4)
      X5 = XE(5) - XF(1)
      Y1 = YE(2) - YE(1)
      Y2 = YE(3) - YE(1)

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IF(X2.GT.X1.OR.X1.GT.X3.OR.X3.GT.X5.OR.X2.LT.0.0) GO TO 50
IF(Y1.GT.Y2.OR.Y1.LT.0.0) GO TO 50
TWL = 0.0
IF(Y2.NE.Y1) TWL = (X1 - X2) / (Y2 - Y1)
AR(1) = (Y2*(X2+X1) - Y1 * (X2-X1))
AR(2) = Y2*X4*2.0
AR(3) = -AR(1) + AR(2)
10 DX = X1/(FL. AT(NBW) -0.5)
IF (100.0* DX .GT. X5) GO TO 20
15 NBW = NBW-1
GO TO 10
25 DY = DX/BETA
YH1 = Y1/DY
YH2 = Y2/DY
XN1 = YH2 - (X1-X2) / DX
XN2 = YH2 + X5/DX
XNIF = X3/DX
XNTE = X5/DX
NBWX = XNTE + 0.5
NBS = Y2/DY + 1.0
NBT = X4/DX + 0.5
DXF(1) = 1.0
DXF(2) = 1.0
DXF(3) = 0.5
DXF(4) = A1 * T(XNLE + 1.5) - XNLE
DXF(5) = XNIF - FLUAT(NBWX-1)
DXF(6) = 0.0
X = 0.5 * DX
NB = 0
KODE = 1
DO 40 NP = 1, NB * X
XN = FLUAT(NP) - 0.5
YH = YH2
IF (TWL .GT. 0.0) YH = AMIN1(YH, YN1+XN/(TWL/BETA))
MH = IFIX(YH)+1
28 MUR(NP) = MH
IF(MB.GE.40) GO TO 15
IF (NP .EQ. NBW) KODE = 3
IF (NSURF .EQ. 1) GO TO 29
IF (X .GT. X1) KODE = 6
IF (X .GT. X3) KODE = 4
IF (X .GT. X3+DX) KODE = 2
IF (NP .EQ. NBWX) KODE = 5
29 IF(MB+MB.GE.2000) GO TO 15
NBI(NP) = NB
DO 30 MP = 1, MB
NB = NB + .1
30 KBOX (NB) = K0F
40 X = X+DX
QOPHO = 0.5*(AS*E4)**2
FO = -S.0*DX*DY*OORF0/EM*RHU
RETURN
50 CALL EXPI
RETURN
END

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9 FORTRAN NLSTOU, DECK  
CPGT2H PGT2H

SUBROUTINE F0121  
COMPLEX VPR, DS, DQ, U, PHIW, CK, CEX  
COMMON/C4/VPR(30,15), DS(2000), DQ(28,2), O(10,10,3), PHIW(50), CK(40)

COMMON/C5/MOR(J=0),NBL(100),FU	IFR,XL,NS,NTM,K,J,OR,OT,QAB,QAN	SON72510
COMMON/C6/X,Y,DX,DY,EH,EK,EKB,EKR,NP,PP,ND,NBOX,KODE,MODE,NBW,NBT		SON/2520
COMMON/C8/R=0.		SON72530
K=2*MOR(NBOX)		SON72540
N=MIND(NBOX,15)		SON72550
DK=DKB		SON72560
DK2=DK**2		SON72570
K1=K-1		SON72580
DKR=DK2/8.0		SON72590
DK4=2.0*DKB		SON72600
DK12=DK2/12.0		SON72610
CH=0.5		SON72620
DM=DK*0.5		SON72630
DM=0.5*DM		SON/2640
DD=2.0*DK		SON72650
DDM=DD		SON72660
D1=0.25*DK2		SON/2670
B5=DK2/24.0		SON72680
B6=1.0		SON/2690
B1=0.0		SON/2700
B4=2.0/DM		SON72710
B2=B5/K4-DM		SON/2720
B3=-0.5*B5		SON72730
B7=DM*B4+B5		SON72740
B4=DKB*B4		SON72750
B4=2.0*B4		SON72760
CN=1.0		SON72770
C3=0.0		SON/2780
C4=0.0		SON72790
C7=0.0		SON72800
CR=0.0		SON72810
DO 2 J=1,N		SON72820
A1=DM/CH		SON72830
C1=CM* COS(A1)		SON/2840
C2=-CM* SIN(A1)		SON72850
CALL CSIN(A1,C5,C6)		SON72860
C5=CM*C5		SON72870
C6=-CM*C6		SON72880
C9=C1-C3		SON72890
C10=C2-C4		SON72900
C11=C5-C7		SON/2910
C12=C6-C8		SON72920
VRF=B3*(C9-B4*(C10-B5*(C3-B1*(C11-B2*(C12		SON72930
VIM=B4*(C9+B3*(C10-B5*(C4+B2*(C11-B1*(C12		SON/2940
VPIC(I,J)=C*PI*(VRF,VIM)		SON72950
23 C3=C1		SON72960
C4=C2		SON72970
C7=C5		SON72980
CH=C6		SON72990
B1=B1-B1		SON/3000
B3=B3-B3		SON73010
B4=B4-B4		SON/3020
B4=B4+DD4		SON73030
CN=(CN+2.0		SON73040
2 CGN=1/NOE		SON73050
CM=C,M+1.0		SON73060
DM=DM+DDM		SON73070
3 DDM=DDM+DD		SON73080
DO 5 J=1,N		SON73090
DO 4 I=1,M1		SON/3100



```

3 K=M-1
4 VPIC(K+1,J)=VPIC(K+1,J)-VPIC(K,J)
5 VPIC(1,J)=2.0*VPIC(1,J)
  CM=0.0
  DM=0.0
  DDM=DK
  DO 12 I=1,M
  C7=0.0
  C8=0.0
  C9=0.0
  C10=0.0
  P1=0.0
  P2=0.0
  CN=1.0
  R6=0.5*DK12
  DO 10 J=1,N
  A1=CM/CN
  A2=DM/CN
  IF (A1-0.2) 7,7,8
7 R1=2.0-A1**2/3.0
  R2=-DK/(6.0*CN)
  GO 10 9
8 B3= SIN(A1)/A1
  R1=2.0*B3
  B2=(B3- COS(A1))/A2-DH/CN*B3
9 B5= COS(A2)/CN
  B4= SIN(A2)/CN
  C3=B1*B3+B2*B4
  C4=B2*B3-B1*B4
  B5=DM*CN
  C1=1.5*C4-2.0*C3
  C2=-2.0*C4+1.5*C3
  C5=C1-C7
  C6=C2-C8
  P3=P2-R6*CN
  P4=B3+2.0*DM12*(C1-1.0)
  VRE=C5-P1*C6+P3*C7-P4*C9
  VIM=C6+P1*C5+P3*C4-P4*C10
  VPIC(1,J)=VPIC(1,J)+CMPLX(VRE,VIM)
  P1=P1+DH
  P2=P2+CN*DK4
  CN=CN+2.0
  C7=C1
  C8=C2
  C9=C3
  C10=C4
  R6=B5+DK12
10 CONTINUE
  CM=CM+DK
  DM=DM+DDM
12 DDM=DDM+DD
  D3=DK/(2.0*3.14159265)
  A1=0.0
  DO 14 J=1,N
  CEX=D3*CMPLX(SIN(A1), COS(A1))
  DO 13 I=1,M
13 VRE=C(1,J)+CEX*VPIC(I,J)
14 A1=A1+DH
  RETURN
  END

```

```

SON73110
SON73120
SON73130
SON73140
SON73150
SON73160
SON73170
SON73180
SON73190
SON73200
SON73210
SON73220
SON73230
SON73240
SON73250
SON73260
SON73270
SON73280
SON73290
SON73300
SON73310
SON73320
SON73330
SON73340
SON73350
SON73360
SON73370
SON73380
SON73390
SON73400
SON73410
SON73420
SON73430
SON73440
SON73450
SON73460
SON73470
SON73480
SON73490
SON73500
SON73510
SON73520
SON73530
SON73540
SON73550
SON73560
SON73570
SON73580
SON73590
SON73600
SON73610
SON73620
SON73630
SON73640
SON73650
SON73660
SON73670
SON73680
SON73690
SON73700

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9      FORTRAN NLSTOU, DECK
CCSIA      CSIN
SUBROUTINE CSIN(X), U, S)
C          SINE AND COSINE INTEGRAL SUBROUTINE
C
C          C AND S ARE THE INTEGRALS OVER T FROM 1 TO INFINITY OF
C          COS(XT)/T AND SIN(XT)/T
C
      SG=1.0
      X=XI
      IF (X) 1,2,2
1      SG=-SG
      X=-X
2      X2=X*X
      IF (X-1.0) 3,3,4
C
C          FOR ABS(X) LESS THAN 1 A SERIES EXPANSION IS USED
C
3      V=((X2/98.0-0.6)*.05*X2+1.0)*X2/18.0-1.0)*X+1.57079633
      L=((X2/45.0-1.0)*X2/24.0+1.0)*X2/4.0-.577215665-ALOG(X)
      GO TO 5
C
C          FOR ABS(X) GREATER THAN 1 APPROXIMATIONS OF HASTINGS ARE USED
C
4      P=((X2+19.194119)*X2+47.411538)*X2+8.493336)/(((X2+21.361055)
1      *X2+70.375496)*X2+30.038227)*X)
      Q=((X2+21.383724)*X2+49.719775)*X2+5.089504)/(((X2+27.177958)
1      *X2+119.918932)*X2+76.707876)*X)
      CO=COS (X)
      SI=SIN (X)
      I=0*CO-P*SI
      V=P*CO+Q*SI
5      S=V*SG
      RETURN
      END
9      FORTRAN NLSTOU, DECK
CWASH      WASH
SUBROUTINE WASH
COMPLEX VPIC, DS, DQ, Q, PHIW, CK
COMMON/C1/KI OX(2000), XE(5), YE(3), AR(3), X1, X2, X3, X4, Y1, Y2, BETA, NBS
COMMON/C3/C(10,28,2), NI(10,2), NF(10,2), NIMAX(2), FN(28), DXE(6), TPI
COMMON/C4/VPIC(40,15), DS(2000), DQ(28,2), Q(10,10,3), PHIW(50), CK(40)
COMMON/C5/MOR(140), NBL(100), FQ, IFR, XL, NS, NIM, K, J, OR, OI, OAB, OAN
COMMON/C6/X, Y, DX, DY, EM, EK, EKB, EKR, NP, PP, NR, NBOX, KODE, MODE, NBW, NBT
COMMON/C8/RHO
XP = X
IF (NS.F0.2) XP = X - X3
NTM = NI(MODF, NS)
7 = CO(MODE, 1, NS)
DZ = 0.0
IF (NTM.F0.1) GO TO 70
K = 1
IF (XP.E0.0.0) GO TO 50
PX = XP
YX = Y/XP
DO 40 N=2,7
PXY = PX
DO 30 M = 1, N
K = K + 1
IF (K.GI.NIM) GO TO 20
SON73710
SON73730
SON73740
SON73750
SON73760
SON73770
SON73780
SON73790
SON73800
SON73810
SON73820
SON73830
SON73840
SON73850
SON73860
SON73870
SON73880
SON73890
SON73900
SON73910
SON73920
SON73930
SON73940
SON73950
SON73960
SON73970
SON73980
SON73990
SON74000
SON74010
SON74020
SON74030
SON74040
SON74050
SON74060
SON74070
SON74090
SON74100
SON74110
SON74120
SON74130
SON74160
SON74150
SON74160
SON74170
SON74180
SON74190
SON74200
SON74210
SON74220
SON74230
SON74240
SON74250
SON74260
SON74270
SON74280
SON74290
SON74300
SON74310
SON74320

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```

ZP=PX*Y*CO(MODE,K,NS)
7=7+ZP
DZ=DZ+EX(K)*ZP
30 PXY=PXY*YX
40 PX=PX*XP
20 DZ=DZ/XP
GO TO 70
50 PX=1.0
DO 60 N=2,7
K=K+N
KK=K-1
IF(KK.LE.NT) DZ=DZ+PX*CO(MODE,KK,NS)
PX=PX*Y
IF(K.GT.NTM) GO TO 70
60 7=7+PX*CO(MODE,K,NS)
70 GO TO (80,90),NS
80 DS(MR) = CMPLX(DZ, EK*Z)
RETURN
90 DS(MR) = CMPLX(-Z, EK*Z)
RETURN
END
$
FORTRAN NLSTOU,DECK
CPHIB PHIB
SUBROUTINE PHIB
COMPLEX VPIC,DS,DU,U,PHIW,CK,CZIRO,PHI,PHITE,DPHI,SPHI
COMMON/C4/VPIC(40,15),DS(2000),DU(28,2),U(10,10,3),PHIW(50),CK(40)
COMMON/C5/MOR(100),LUL(100),FU,IFR,XL,NS,NTM,K,J,QR,QI,QAB,QAN
COMMON/C6/X,Y,PA,JY,EM,EK,EKB,EKR,NP,MP,NB,NBUX,KUDE,MODE,NBW,NBT
COMMON/C7/CZIRO,PHI,PHITE,DPHI,SPHI
COMMON/C8/REO
NU=MNO(NP,15)
DO 20 I=2,NU
NU=NP-I+1
JR=NOB(NU)
NJ=NBL(NU)+1
DO 20 J=1,NJ
K=1+IABS(MP-J)
DPHI=VPIC(K,I)
IF(J.EQ.1) GO TO 10
K=MP+J-1
DPHI=DPHI+VPIC(K,I)
10 SPHI=SPHI+DPHI*IS(N,J)
20 NJ=NJ+1
RETURN
END
$
FORTRAN NLSTOU,DECK
MSIMEC MSIMEC
FUNCTION MSIMEC(M,N,L,A,B)
COMPLEX A,B,C
DIMENSION A(M,1),B(N,1)
DO 30 J=1,N
C=0.0
DO 10 J=1,N
10 C=AMAX1(C,ABS(REAL(A(J,J))),ABS(AIMAG(A(J,J))))
IF(C.EQ.0.0) GO TO 100
DO 20 J=1,N
20 A(I,J)=A(I,J)/C
DO 30 J=1,1
30 B(I,J)=B(I,J)/C
IF(N.EQ.1) GO TO 205

```

SON74330  
SON74340  
SON74350  
SON74360  
SON74370  
SON74380  
SON74390  
SON74400  
SON74410  
SON74420  
SON74430  
SON74440  
SON74450  
SON74460  
SON74470  
SON74480  
SON74490  
SON74500  
SON74510  
SON74520  
SON74530  
SON74540  
SON74560  
SON74570  
SON74580  
SON76460  
SON74600  
SON74610  
SON74620  
SON74630  
SON74640  
SON74650  
SON74660  
SON74670  
SON74680  
SON74690  
SON74700  
SON74710  
SON74720  
SON74730  
SON74740  
SON74750  
SON74760  
SON74770  
SON74780  
SON74790  
SON74810  
SON74820  
SON74830  
SON74840  
SON74850  
SON74860  
SON74870  
SON74880  
SON74890  
SON74900  
SON74910  
SON74920  
SON74930  
SON74940

```

NM = N - 1
DO 200 J = 1, NM
C = 0.0
K = 0
DO 40 I = J, N
D = A**S, REAL(A(I, J)) + ABS(AIMAG(A(I, J)))
IF (D .GE. D) GO TO 10
K = I
C = D
40 CONTINUE
IF (C .EQ. 0.0) C .LT. 1.E-7) GO TO 1000
IF (K .EQ. J) GO TO 70
DO 50 JJ = J, K
G = A(J, JJ)
A(J, JJ) = A(K, JJ)
50 A(K, JJ) = G
DO 60 JB = 1, L
G = R(J, JJ)
R(J, JJ) = R(K, JJ)
60 R(K, JJ) = G
70 G = 1.0/A(J, J)
JP = J + 1
DO 80 JJ = JP, N
80 A(J, JJ) = A(J, JP) * G
90 DO 100 JJ = 1, I
100 R(I, JJ) = R(J, JJ) * G
DO 200 I = 1, N
IF (I .EQ. J) GO TO 200
G = A(I, J)
DO 110 JJ = JP, N
110 A(I, JJ) = A(I, JJ) - G * A(J, JJ)
DO 120 JJ = 1, I
120 R(I, JJ) = R(I, JJ) - G * R(J, JJ)
200 CONTINUE
205 G = A(N, N)
IF (ABS(REAL(G)) + ABS(AIMAG(G)) .LT. 1.E-7) GO TO 1000
DO 210 J = 1, N
210 R(N, J) = R(N, J) / G
IF (C .EQ. 1) GO TO 230
DO 220 I = 1, NM
DO 220 JJ = 1, I
220 R(I, JJ) = R(I, JJ) - A(I, N) * R(N, JJ)
230 MSINFC = 1
RETURN
1000 MSINEC = 2
RETURN
END
* FOOTRAN NLS TOU, D, CK
C0C1J D01J
SUBROUTINE TQ1J
COMMON VPI, DS, D, U, PHI, CK, CZERO, PHI, PHIE, DPHI, SPHI
COMMON/C1/KOXY(2000), XF(5), YE(3), AR(3), X1, X2, X3, X4, Y1, Y2, BETA, NIS
COMMON/C3/C(10, 2), NI(10, 2), NF(10, 2), NTMAX(2), FN(28), DXE(6), IP
COMMON/C4/VPIL(40, 15), DS(2000), DQ(28, 2), Q(10, 10, 3), PHIW(50), CK(40)
COMMON/C5/MOR(100), DPL(100), FQ, IFR, XL, NS, NIM, K, J, QR, QJ, QAB, QAN
COMMON/C6/X, Y, DX, DY, EM, EK, EKB, EKR, NP, MP, NB, KBOX, KODE, MODE, NBW, NBI
COMMON/C7/CZERO, P, I, PHIE, DPHI, SPHI
COMMON/C8/R, O
DPHI = PHI * XF(5) / F
IF (MP .EQ. 1) DPHI = 0.5 * DPHI
SON/4950
SON/74960
SON/74970
SON/74980
SON/74990
SON/75000
SON/75010
SON/75020
SON/75030
SON/75040
SON/75050
SON/75060
SON/75070
SON/75080
SON/75090
SON/75100
SON/75110
SON/75120
SON/75130
SON/75140
SON/75150
SON/75160
SON/75170
SON/75180
SON/75190
SON/75200
SON/75210
SON/75220
SON/75230
SON/75240
SON/75250
SON/75260
SON/75270
SON/75280
SON/75290
SON/75300
SON/75310
SON/75320
SON/75330
SON/75340
SON/75350
SON/75360
SON/75370
SON/75380
SON/75390
SON/75400
SON/75410
SON/75420
SON/75440
SON/75450
SON/75460
SON/75470
SON/75480
SON/75490
SON/75500
SON/75510
SON/75520
SON/75530
SON/75540
SON/75550

```

```

XP = X
IF(NS.EQ.2) XP = X - X3
PX = XP
K = 1
NIM = NIMAX(NS)
DQ(1,NS) = DQ(1,NS) + DPHI*CMPLX(0.0,-EK)
IF(NTH.EQ.1) GO TO 50
IF(XP.EQ.0.0) GO TO 30
YX = Y/XP
DO 20 N = 2,7
Z = PX
DO 10 M = 1,N
K = K + 1
IF(K.GT.NIM) GO TO 50
DQ(K,NS) = DQ(K,NS) + DPHI*Z*CMPLX(FN(K)/XP,-EK)
10 Z = Z*YX
20 PX = PX*XP
GO TO 50
30 PX = 1.0
DO 40 R = 2,7
K = K + N
KK = K - 1
IF(KK.LE.0) DQ(KK,NS) = DQ(KK,NS) + DPHI*PX
PX = PX*Y
IF(KK.GT.NIM) GO TO 50
40 DQ(KK,NS) = DQ(KK,NS) + DPHI*CMPLX(0.0,-EK*PX)
50 IF(MODF.NE.3) GO TO 90
DPHI = DPHI/DF(K)
R = 1
YX = Y/XP
PX = 1.0/DF
DO 60 M = 1,7
Z = PX
DO 60 N = 1,7
DQ(M,NS) = DQ(M,NS) - DPHI*Z
K = K + 1
IF(K.GT.NIM) GO TO 80
60 Z = Z*YX
70 PX = PX*XP
80 ARG = EK*(X3 - X1)
DPHI = -DPHI*CMPLX(COS(ARG),-SIN(ARG))
X1 = 0.0
CALL QEGF
90 IF(MODF.NE.5) RETURN
XE = X4
IF(MP.EQ.1) PHIDF = 0.5*PHIDE
DPHI = PHIDF
CALL QGFE
RETURN
END

```

SON75560  
SON75570  
SON75580  
SON75590  
SON75600  
SON75610  
SON75620  
SON75630  
SON75640  
SON75650  
SON75660  
SON75670  
SON75680  
SON75690  
SON75700  
SON75710  
SON75720  
SON75730  
SON75740  
SON75750  
SON75760  
SON75770  
SON75780  
SON75790  
SON75800  
SON75810  
SON75820  
SON75830  
SON75840  
SON75850  
SON75860  
SON75870  
SON75880  
SON75890  
SON75900  
SON75910  
SON75920  
SON75930  
SON75940  
SON75950  
SON75960  
SON75970  
SON75980  
SON75990  
SON76000  
SON76010  
SON76020  
SON76030  
SON76040  
SON76050  
SON76060  
SON76080  
SON76090  
SON76100  
SON76110  
SON76120  
SON76130  
SON76140  
SON76150  
SON76160

```

$ FORTRAN INLSHOW,DECK
CCEGF QGFE
SUBROUTINE QGFE
COMMON/CPIC/US,DS,DS,DPHIW,CK,CZERO,PHI,PHIDE,DPHI,SPHI
COMMON/CA/VPIC(60,45),DS(2000),DO(28,2),Q(40,10,3),PHIW(50),CK(40)
COMMON/CS/MIC(100),NLC(100),FIO , IIR,XL,NS,NIM,K,J,QR,WI,QAB,QAN
COMMON/CC/X,Y,DX,DY,EN,EK,ENB,ENR,NP,IP,NB,KROX,KUDE,MODE,NBW,NBT
COMMON/CC7/CZERO,PHI,PHIDE,DPHI,SPHI
COMMON/CC8/RI,IP
IPX=1.0/DF

```

```

IF(XL.FU.0.0) GO 10 30
YX=Y/XL
K=1
DO 20 N=1,7
PY=FX
DO 10 M=1,N
DQ(K,2) = DQ(K,2) - DPHI*PY
IF(K.EQ.NTM) RETURN
K=K+1
10 PY=PY*YX
20 PX=PX*XL
RETURN
30 K = 0
DO 40 N = 1,7
K = K + N
IF(K.GT.NTM) RETURN
DQ(K,2) = DQ(K,2) - DPHI*PX
40 PX = PX*Y
RETURN
END
*
* CONTROL PRINTOUT, DECK
*
*
SUBROUTINE FOUT(I,IO)
COMPLEX VPI,DS,DQ,DPHIW,CK,CZERO,PHI,PHITE,DPHI,SPHI
DIMENSION S(3,3),SURF(2,3),COD(7),C(50)
DIMENSION CARDS(27,50)
COMMON/C1/K,DX(2000),XE(5),YE(3),AR(3),X1,X2,X3,X4,Y1,Y2,BETA,NBS
COMMON/C2/AS,MAC,SMACH(6),NFREQ,FREQ(10),NMODE,NSURF,LVPIC,LSVPS
COMMON/C3/CD(10,2),NI(10,2),NF(10,2),NTMAX(2),FN(28),DXE(6),TP
COMMON/C4/VITC(80,15),DS(2000),DQ(28,2),Q(10,10,3),PHIW(50),CK(40)
COMMON/C5/MOB(100),NRL(100),FO,IFR,XL,NS,NTM,K,J,QR,QI,QAB,QAN
COMMON/C6/X,Y,DX,DY,EM,EK,EKB,EKR,NP,RP,NB,NBOX,KUDE,MODE,NBW,NBT
COMMON/C7/CZFN,PHI,PHITE,DPHI,SPHI
COMMON/C8/R=0
DATA (SW(1,1),I=1,6)/26HMAP OF SONIC BOX OVERLAY ,
1 26HON WING, TAIL AND WAKE ,
2 26H (S) - WING ,
3 26H (S) - TAIL ,
4 26H (,) - WAKE ,
5 26H /
DATA (SURF(1,1),I=1,3)/8HWING ,8HTAIL ,11HWING + TAIL /
DATA COD/1HS,1HT,1HS,1HX,1HS,1H,,1H./
GO TO (10,20,30,40,50,60,70,80),IND
10 WRITE(6,11) EM,AS,PHI, XE(1),XE(4),X1,X4,Y1,Y2,Y2,Y2,X2,X4,
IAR(1),AR(2),NBW,NBT,NBS,NBS
11 FORMAT(1H)////3 X,43HMAC/NAA MISSILE TRANSONIC AIRLOADS PROGRAM
1 //37X,30HIGHLIGHT CONDITIONS AND GEOMETRY/1H0//15X, 13HMACH NUMBERS
2 =,18.5,4X,16H SPEED OF SOUND =F10.3,4H L/T,4X,4HRHO=,E14.8//1H0/
X54X,4HWING,1HX,
3 4HTAIL//22X,15H H.T. STATION (L),2F22.3//22X,16HROOT CHORD (L),
4 2F22.3// 22X,15H H.E. SPAN (L),2F22.3//22X,16HTOTAL E. SPAN (L),
5 2F22.3// 22X,15H TIP CHORD (L),2F22.3//22X,16HTOTAL AREA (L*L),
6 2F22.3// 22X,16HCHORDWISE BOXES ,I19,I22//
7 22X,16HSPANWISE BOXES ,I19,I22)
WRITE(6,12) BOX,DX,DY
12 FORMAT(1H0//,11X,25HTOTAL CHORDWISE BOXES =,13, 5X,11HBOX CHORD =,
1 1P1F12.5,2F1, 5X,10HBOX SPAN =,1P1F12.5,2H L/ )
WRITE(6,91)
NB = 1
DO 17 NP = 1,4RDX

```

SON76170  
SON76180  
SON76190  
SON76200  
SON76210  
SON76220  
SON76230  
SON76240  
SON76250  
SON76260  
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SON76280  
SON76290  
SON76300  
SON76310  
SON76320  
SON76330  
SON76340  
SON76350  
SON76360  
SON76370  
SON76390  
SON76400  
SON76410  
SON76420  
\*\*\*\*\*  
SON76430  
SON76440  
SON76450  
SON76460  
SON76470  
SON76480  
SON76490  
SON76500  
SON76510  
SON76520  
SON76530  
SON76540  
SON76550  
SON76560  
SON76570  
SON76580  
SON76590  
SON76600  
SON76610  
SON76620  
SON76630  
SON76640  
SON76650  
SON76660  
SON76670  
SON76680  
SON76690  
SON76700  
SON76710  
SON76720  
SON76730  
SON76740  
SON76750  
SON76760

```

PB = HGB(NP)
DO 13 MP = 1, MB
K = KROX(NP)
C(MP) = COD(X)
13 NB = NB + 1
IF(NP.GT.6) GO TO 15
WRITE(6,14) (SH(I,MP), I=1,5), (C(MP), MP=1, MB)
14 FORMAT(10X, 5A6, 50A1)
GO TO 17
15 WRITE(6,16) (C(MP), MP=1, MB)
16 FORMAT(40X, 50A1)
17 CONTINUE
GO TO 1000
20 WRITE(6,51) FREQ(IFR), NBOX, EKR , EM
WRITE(6,21) C, M, EKR
21 FORMAT(1H , 28X, 48HPIANAR VELOCITY POTENTIAL INFLUENCE COEFFICIENTSSON76920
1 /1H0, 30X, 3H MACH NO. =, F8.5, 10X, 6HKBAR =, F9.5/1H0, 13X, 1HJSON76930
2 10X, 5HNUBAR, 5X, 5H MUBAR, 11X, 14HREAL VPIC(J, I), 8X, 14HIMAG VPIC(J, I)SON76940
3 /1H )
SON/6950
JBOX = 2*MOM(NBOX)-1
IBOX = MIN0(NBOX, 15)
DO 22 I = 1, IBOX
DO 22 J = 1, JBOX
BARMU = I - 1
BARMU = J - 1
22 WRITE(6,23) I, J, BARMU, BARMU, VPIC(J, I)
23 FORMAT(9X, 2I6, 4X, 2F10.1, 2X, 1P2E22.5)
SON/6960
GO TO 1000
30 WRITE(6,51) FREQ(IFR), NBOX, EKR , EM
WRITE(6,31) C, M, EKR
31 FORMAT(1H , 21X, 29HUPPER VELOCITY POTENTIALS AND SURFACE UPWASHES FSON77070
(COR MODE NO., 13/ 1H0, 9X, 1HN, 6X, 1HM, 5X, 2HNB, 7X, 10HR PHI(N, M), 7X, 10HISON77080
2 PHI(N, M), 10X, 9HR W(N, M), 8X, 9HI W(N, M)/1H )
SON/7090
GO TO 1000
40 SPH1 = DS(NB)/E4
WRITE(6,41) MP, M, NB, SPH1, CK(MP)
41 FORMAT(4X, 3I7, 1P2E17.5, 3X, 1P2E17.5)
SON/7100
GO TO 1000
60 IF(NS.EQ.3) GO TO 100
50 WRITE(6,51) FREQ(IFR), NBOX, EKR , EM
51 FORMAT(1H1, 33X, 43HMISSILE TRANSONIC AIRLOADS PROGRAM (CONT-D)//1H0SON77170
1 8X, 27HOSCILLATORY FREQUENCY (CPS), F12.5, 14X, 12, 25H BOXES IN CHORDSON77180
2 DIRECTION /1H0, 8X, 30HREDUCED FREQUENCY (SEMI CHORD), F9.5, 14X, SON77190
3 23HFREE STREAM MACH NUMBER, F9.3, /1H )
SON/7200
WRITE(6,101) SURF(1, NS)
SON/7210
101 FORMAT(28X, 45HINPUT MODE SHAPE POLYNOMIAL COEFFICIENTS FOR , A6/ SON77220
1 22X, 62HREFERENCE TO THE SURFACE LEADING EDGE-CENTERLINE INTERSECSON77230
2 ION //2X, 4HMODE, 20X, 7HCUEFFS.)
SON/7240
DO 102 I=1, NMODE
NIM=NT(1, NS)
SON/7250
102 WRITE(6,103) I, (CO(I, J, NS), J=1, NIM)
SON/7260
103 FORMAT(1H0, 14, 4X, 1P7E13.4/(9X, 1P7E13.4))
SON/7270
100 WRITE(6,51) FREQ(IFR), NBOX, EKR , EM
SON/7280
WRITE(6,61) (SURF(I, NS), I=1, 2)
SON/7290
61 FORMAT(1H , 35X, 23HGENERALIZED FORCES FOR , 2A6/1H0, 6X, 4HDEFL, 3X, SON77310
1 4HLOAD, 10X, 9HREAL PART, 10X, 9HIMAG PART, 10X, 9HABS VALUE, 10X, SON77320
2 11HPHASE ANGLE //)
SON/7330
GO TO 1000
SON/7340
70 WRITE(6,71) J, K, JR, Q1, QAB, QAN
SON/7350
KKK=2*NMODE
*****

```

NNN=2*K	*****
NNN=NNN-1	*****
CARDS(J,NNN)=0R	*****
CARDS(J,NNN)=0I	*****
IF (NSURF .EQ. 1) GO TO 667	
IF (NS.NE.3) GO TO 1000	*****
667 IF (J.NE.NMODE) GO TO 1000	*****
IF (K.NE.NMODE) GO TO 1000	*****
KKK=2*NMODE	*****
PUNCH 666, ((CARDS(II,JJ),JJ=1,KKK),II=1,NMODE)	*****
666 FORMAT(6E12.5)	*****
71 FORNAT(1H0,19,17,2X,1P3E19.5,0PF16.3,4H DEG)	SON77380
GO TO 1000	SON77370
80 WRITE(6,91)	SON77380
WRITE(6,81) FRE,(IFR)	SON77390
81 FORNAT(1H0////////24X,56HUNABLE TO OBTAIN COMPLEX SIMULTANEOUS EQUA	SON77400
1IONS SOLUTION//31X,42HCOMPUTATIONS FOR THIS FREQUENCY TERMINATED,/	SON77410
2/45X, 6HFRE. =,19.3)	SON77420
91 FORNAT(1H1,30X,13HMISSILE TRANSONIC AIRLOADS PROGRAM (CONT-D)//)	SON77430
1:000 RETURN	SON77440
END	SON77450



## 5.0 SUPERSONIC UNSTEADY AERODYNAMICS

### 5.1 Theoretical Derivation

For Mach numbers greater than 1.0, the linearized flow equation becomes a hyperbolic differential equation:

$$(M^2 - 1) \phi_{xx} - \phi_{yy} - \phi_{zz} = -M^2 \left[ 2ik \phi_x - k^2 \phi \right] \quad (5.1.1)$$

The equation only has solutions within characteristic regions called Mach cones. Linearized supersonic flow theory has led to closed-form solutions for many types of lifting surfaces in steady flow. These solutions are easily derived because the influence of a small perturbation is confined to its downstream or aft Mach cone. Conversely, the only disturbances that can influence a particular point are confined to its upstream or fore Mach cone.

Equation (5.1.1) is satisfied by a pulsating source. The source, placed at  $(\xi, \eta, \zeta)$ , emanates spherical disturbances and has a velocity potential induced at  $(x, y, z)$  given by

$$\phi_s = A(\xi, \eta, \zeta) G(x - \xi, y - \eta, z - \zeta) \quad (5.1.2)$$

where

$$G(x - \xi, y - \eta, z - \zeta) = -\frac{1}{\pi R} \exp[-ik(x - \xi)] \cos\left[\frac{\bar{k}}{M} R\right] \quad (5.1.3)$$

$$R = \sqrt{(x - \xi)^2 - (M^2 - 1)[(y - \eta)^2 + (z - \zeta)^2]} \quad (5.1.4)$$

$$\bar{k} = k M^2 / (M^2 - 1) \quad (5.1.5)$$

and  $A(\xi, \eta, \zeta)$  = source strength

This type of disturbance has no influence outside the downstream Mach cone and is discontinuous at the point  $(\xi, \eta, \zeta)$ . To provide the necessary antisymmetry of disturbances associated with lifting surfaces, we place a pair of sources on either side of the  $z = 0$  plane and require the lower source strength to be equal in magnitude but opposite in sense to the upper source strength.

Applying this source superposition technique to the wing, wake and control surface, the entire  $z = 0$  plane is covered above and below with source sheets. The strength of the opposing sheets are equal in magnitude but opposite in sense;  $A(\xi, \eta, 0^+) = -A(\xi, \eta, 0^-)$ . The strength distribution has been shown by Garrick and Rubinow (Reference 8) to be equal everywhere to the local downwash. Using this condition, we have

$$A(\xi, \eta, 0^+) = w(\xi, \eta, 0^+) \quad (5.1.6)$$

The velocity potential at  $(x, y, 0^+)$  can be written as

$$\phi = \iint w(\xi, \eta) G(x - \xi, y - \eta) d\xi d\eta \quad (5.1.7)$$

The range of integration extends over the region contained in the fore Mach cone of the point.

In the wake region between the wing and control surface, the downwash must be determined to satisfy the continuous pressure condition. This is the same relationship given by Equation (4.1.7) in the transonic unsteady aerodynamics discussion. Substituting Equation (5.1.7) in the wake condition gives

$$\iint w(\xi, \eta) G(x - \xi, y - \eta) d\xi d\eta = \phi_{\text{wing t.e.}} \left[ \exp-ik(x - x_{\text{wing t.e.}}) \right] \quad (5.1.8)$$

This relationship which requires knowledge of the upstream downwash within the fore Mach cone to solve for the local downwash.

The preceding discussion applies only to lifting surfaces with supersonic leading edges. When the leading edges are supersonic, the fluid flow over the top and bottom of the lifting surfaces are completely isolated from one another. To treat the problem of subsonic leading edges, the concept of a diaphragm of unknown downwash is added to the planform. The diaphragm region is between the Mach envelope and subsonic edge. The diaphragm downwash is found by applying the condition of zero pressure:

$$0 = \iint w(\xi, \eta) G(x - \xi, y - \eta) d\xi d\eta \quad (5.1.9)$$

The downwash of the diaphragm creates an additional contribution to the pressure profile over the planform.

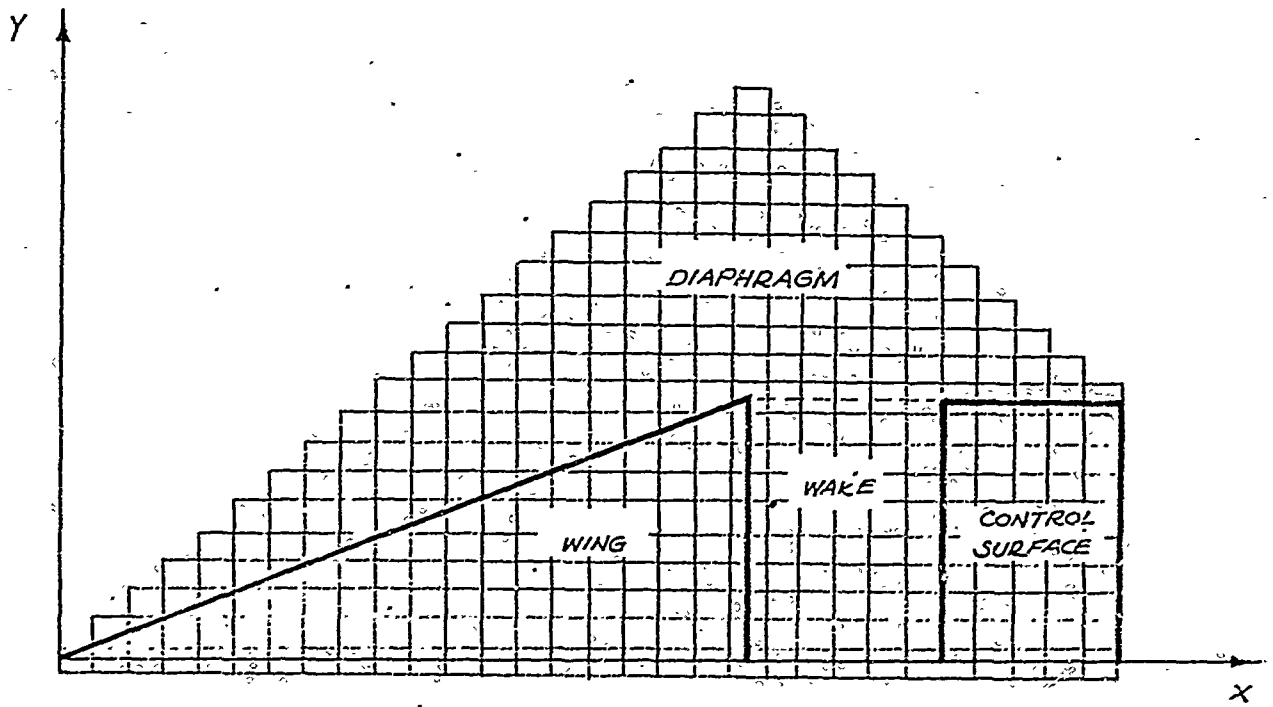


Figure 5.1.1 Mach Box Overlay Pattern

The velocity potential distribution is found by the so called Mach box method. The wing, control surface, wake and diaphragm regions are covered with a grid of rectangular boxes of length  $\Delta$ . The width of the boxes is set equal to  $\Delta / \sqrt{M^2 - 1}$  thus making the box diagonals parallel to the Mach lines. The source strength (downwash) is assumed constant over each box and equal to the value at the box center. A typical Mach box overlay is shown in Figure (5.1.1).

From the conditions imposed on the planform, the downwash can be numerically evaluated for the diaphragm and wake boxes and the velocity potential profile can be established for any deformation mode. The pressure can then be calculated from Equation 4.1.8 and generalized forces can be evaluated with Equation 2.0.1.

## 5.2 PROGRAM DESCRIPTION

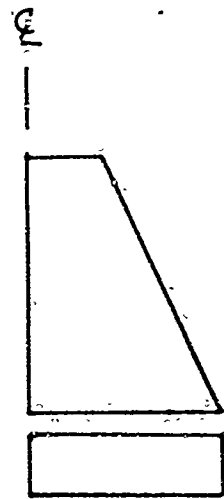
The Supersonic Unsteady Aerodynamics Program calculates generalized forces for up to 10 deformation modes. The computer solution is based upon the Mach box technique. The various configurations which can be analyzed are shown in Figure 5.2.1 and Table 5.2.1. The analysis includes interaction effect between tandem surfaces and wake effects on the trailing surface. Single surfaces may be analyzed by inputting a second surface with a zero chordlength.

The supersonic Mach box method uses source superposition method to approximate the aerodynamic forces on an oscillating thin planar surface. The diaphragm concept was employed to handle subsonic leading edges and gaps between the aerodynamic surfaces. For purposes of calculating pressures, it was assumed that the source strength over the area of each box is a constant value which satisfies the condition of tangential flow at the center of the box. The Mach box procedure is basically the same as the method of Pines, et al, Reference II, differing only in that the surface and diaphragm is overlaid with a grid of rectangular boxes, the diagonals of which are parallel to Mach lines. As in the subsonic and transonic cases, the potential equation is written as an integral equation (this time relating the downwash to the source strengths) and approximated by a matrix equation. The numerical difficulties are primarily ones of computer logic since the zones of influence of a given Mach box is limited to the region within the aft Mach lines. The matrix formulation leads to a partitioned form since there are two boundary conditions to be matched. The first boundary condition is the downwash on the surface, and the second is that there be no pressure difference off of the surface in the diaphragm regions. The zero pressure conditions leads to a relationship between the diaphragm potentials and the surface potentials, and the surface downwash condition then leads to the surface potentials. The surface pressures then follow from the surface potentials.

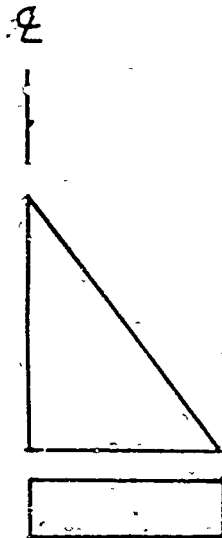
The solution for the generalized aerodynamic forces requires the input of the deformation modes due to vibration. The program considers the modes to be expressed as analytic functions of the form:

$$w(x, y) = \sum_{m=0}^N \sum_{n=0}^m c_{(n-m), m} x^{(n-m)} y^m$$

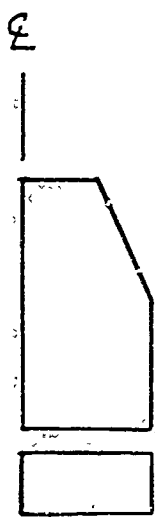
To meet this requirement only the coefficients "c" are required as input into the program. These coefficients can be obtained in several ways, the most common way is to surface fit the modes by the least-square technique.



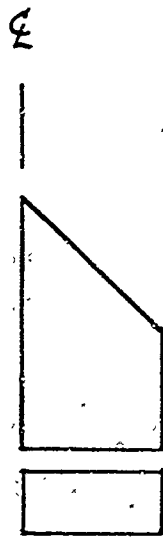
TRAPEZOIDAL



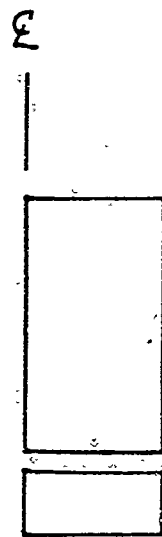
DELTA



TRAPEZOIDAL  
(CROPPED)



DELTA  
(CROPPED)



RECTANGULAR

FIGURE 5.2.1  
TANDEM COPLANAR CONFIGURATIONS AT SUPERSONIC  
MACH NUMBER

TABLE 5.2.1- OPTIONAL CONFIGURATIONS

CONFIGURATION	CHORDWISE COORDINATE	SPANWISE COORDINATE
RECTANGULAR	$X(1) \neq 0.0$ $X(2) = 0.0$ $X(3) > 0.0$ $X(4) \geq X(3)$ $X(5) \geq X(4)$	$Y(1) = 0.0$ $Y(2) = 0.0$ $Y(3) > 0.0$
DELTA	$X(1) = 0.0$ $X(2) > 0.0$ $X(3) = X(2)$ $X(4) \geq X(3)$ $X(5) \geq X(4)$	$Y(1) = 0.0$ $Y(2) = 0.0$ $Y(3) > 0.0$
TRAPEZOIDAL	$X(1) = 0.0$ $X(2) > 0.0$ $X(3) = X(2)$ $X(4) \geq X(3)$ $X(5) \geq X(4)$	$Y(1) = 0.0$ $Y(2) > 0.0$ $Y(3) > Y(2)$
TRAPEZOIDAL (CROPPED)	$X(1) = 0.0$ $X(2) > X(1)$ $X(3) > X(2)$ $X(4) \geq X(3)$ $X(5) \geq X(4)$	$Y(1) = 0.0$ $Y(2) > 0.0$ $Y(3) > Y(2)$
DELTA (CROPPED)	$X(1) = 0.0$ $X(2) > 0.0$ $X(3) > X(2)$ $X(4) \geq X(3)$ $X(5) \geq X(4)$	$Y(1) = 0.0$ $Y(2) = 0.0$ $Y(3) > Y(2)$

### 5.3 INPUT INSTRUCTIONS

Instructions for preparing input data for the supersonic computer program are presented here. The field location and format for each quantity is specified. Any set of units may be used for geometric dimensions and acoustic velocity as long as they are consistent, e.g., if inches is used for length, then the acoustic velocity must have dimensions of inches per second. The required data and the sequence in which the information is entered is as follows:

#### 1. Streamwise Coordinates (6E12.5 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	X(1)	X(2)	X(3)	X(4)	X(5)	
Item	(1)	(2)	(3)	(4)	(5)	

- (1) X(1) Wing root leading edge coordinate (see Figure 5.3.1)
- (2) X(2) Wing tip leading edge coordinate
- (3) X(3) Wing trailing edge coordinate
- (4) X(4) Control surface leading edge coordinate
- (5) X(5) Control surface trailing edge coordinate

A single surface, the wing, may be analyzed by setting X(4) and X(5) equal to X(3). The various configurations are generated as shown in Table 5.2.1. The origin for the planform and AIC station coordinates must be at the leading edge root of the wing, therefore X(1) and Y(1) described below, must always be zero.

#### 2. Spanwise Coordinates and Acoustic Velocity (6E12.5 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	Y(1)	Y(2)	Y(3)	SOUND	RHØ	
Item	(1)	(2)	(3)	(4)	(5)	

- (1) Y(1) Wing root spanwise coordinate
- (2) Y(2) Wing leading edge spanwise coordinate
- (3) Y(3) Wing (and control surface) tip spanwise coordinate
- (4) SOUND Speed of sound at altitude for which analysis is performed
- (5) RHØ Density of fluid \* 1000.0 (M./L<sup>3</sup>)



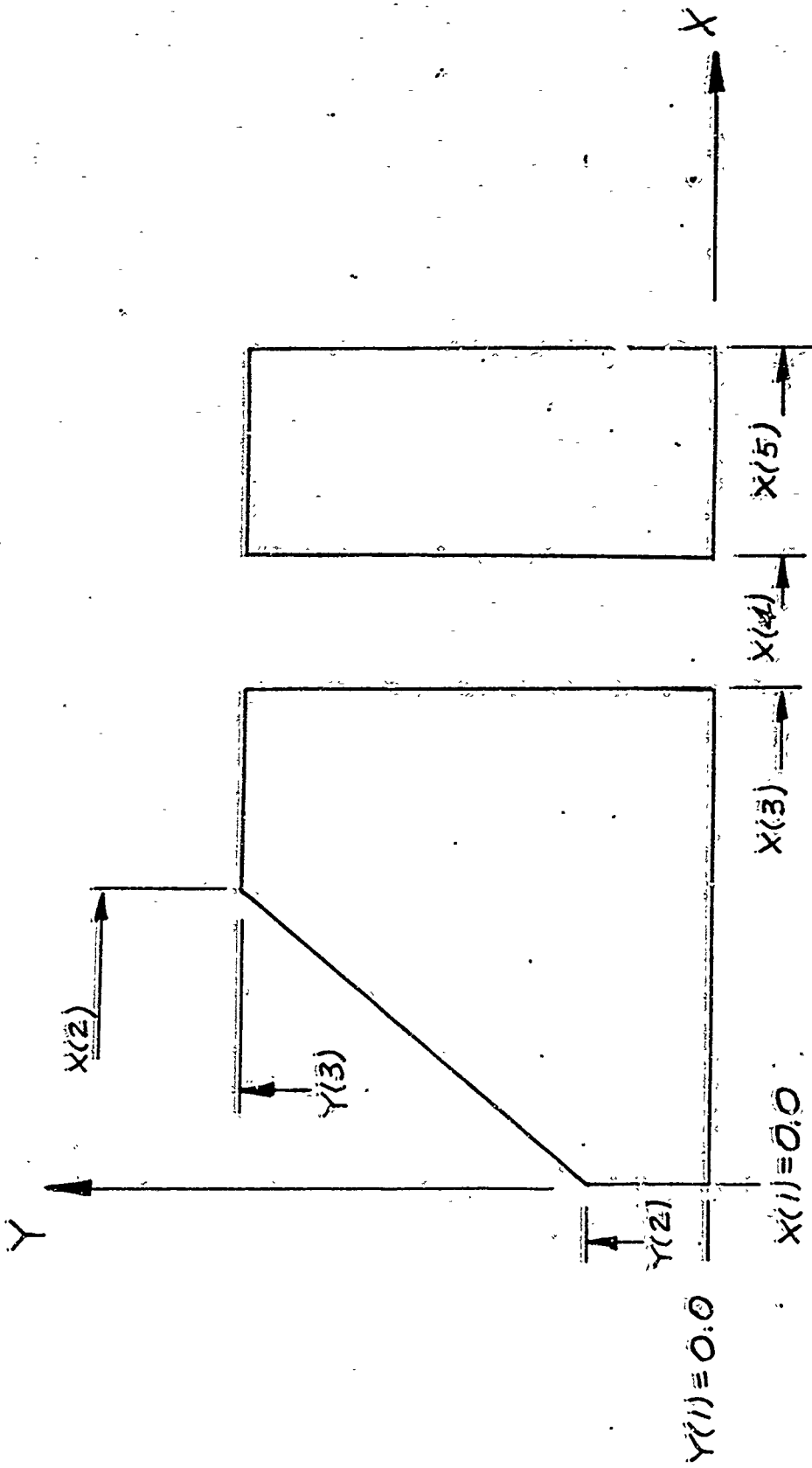


FIGURE 5.3.1  
GEOMETRY DESCRIPTION

3. General Information (6I12 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	NMACH	NFREQ	NMODES	NBW	LVPIC	LSSVP
Item	(1)	(2)	(3)	(4)	(5)	(6)

- (1) NMACH Number of Mach numbers (max 6)
- (2) NFREQ Number of input frequencies (max 10)
- (3) NMODES Number of input modes (max 10)
- (4) NBW Number of chordwise wing boxes (max 10)
- (5) LVPIC Print velocity potential influence coefficients; 0 ~ No, 1 ~ Yes
- (6) LSSVP Print upwashes; 0 ~ No, 1 ~ Yes

4. Mach Numbers (6E12.5 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	FMACH(1)	FMACH(2)	FMACH(3)	FMACH(4)	FMACH(5)	FMACH(6)
Item	(1)	(2)	(3)	(4)	(5)	(6)

- (1) FMACH(i) Mach numbers for which the analysis is to be performed.

5. Frequency (6E12.5 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	FREQ(1)	FREQ(2)	FREQ(3)	FREQ(4)	FREQ(5)	FREQ(6)
Item						

- (1) FREQ Frequencies for which the analysis is to be performed.  
Continue on next card for FREQ(i) > 6

6. Deformation Modes. Repeat the following Cards NMODES Times

(6I12) Format.

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	NTM1(i)	NFI				
Item	(1)	(2)				

- (1) NTM1(i) Number of deformation mode coefficients for the wing, mode i
- (2) NFI Compute generalize forces; 0 ~ No, 1 ~ Yes  
If NFI = 0, the program will compute the VPIC's and stop.

(6E12.5) Format

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	CØ(1)	CØ(2)	CØ(3)	CØ(4)	CØ(5)	CØ(6)
Item	(1)	(2)	(3)	(4)	(5)	(6)

(1) CØ(i) i = 1, NTM deformation polynomial coefficients to be input in the following order: 0,0; 1,0; 0,1; 2,0; 1,1; 0,2; 3,0; where the first integer is the power of x and the second is the power of y. Continue on successive card until all polynomial coefficients are input.

(6E12) Format

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	NTM(i)	NFI				
Item	(1)	(2)				

(1) NTM2(i) Number of deformation mode coefficients for the control surface, mode (i)

(2) NFI Compute generalized forces; 0 ~ No; 1 ~ Yes. If NFI = 0, the program will compute the VPIC's and stop.

(6E12/5) Format

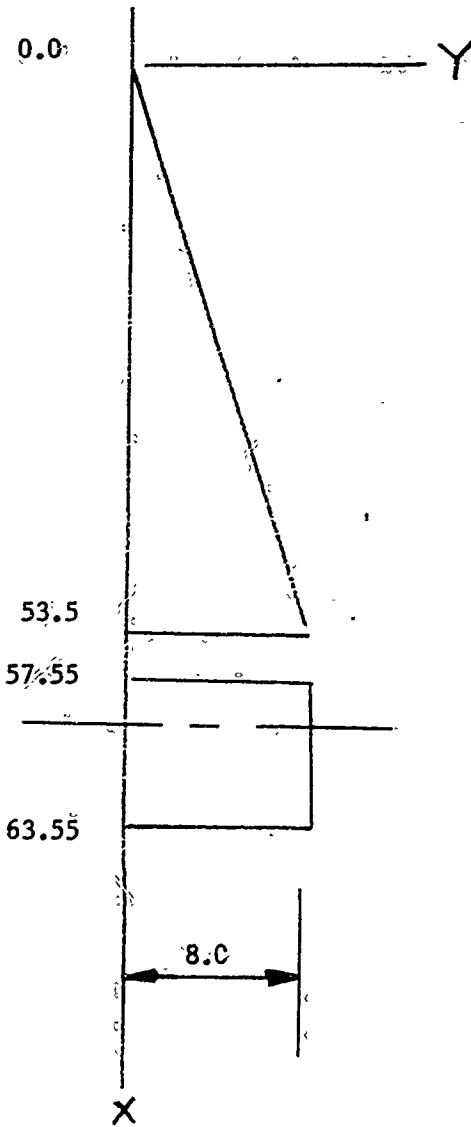
Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	CØ(1)	CØ(2)	CØ(3)	CØ(4)	CØ(5)	CØ(6)
Item	(1)	(2)	(3)	(4)	(5)	(6)

CØ(i) i = 1, NTM deformation polynomial coefficients to be input in the following order: 0,0; 1,0; 0,1; 2,0; 1,1; 0,2; 3,0; etc. where the first integer is the power of "x" and the second is the power of "y". Continue on successive cards until all polynomial coefficients are input.

#### 5.4 SAMPLE PROBLEM

The generalized forces are calculated for the configuration below. The flight parameters and pertinent input data are on the first page of the computer print out.

The coefficients of the deformation modes for the forward surface are shown on the third page of the computer print out, and for the aft surface on the fifth page of the computer print out.



HAC/NAA MISSILE SUPERSONIC AIRLOADS PROGRAM

FLIGHT CONDITIONS AND GEOMETRY.

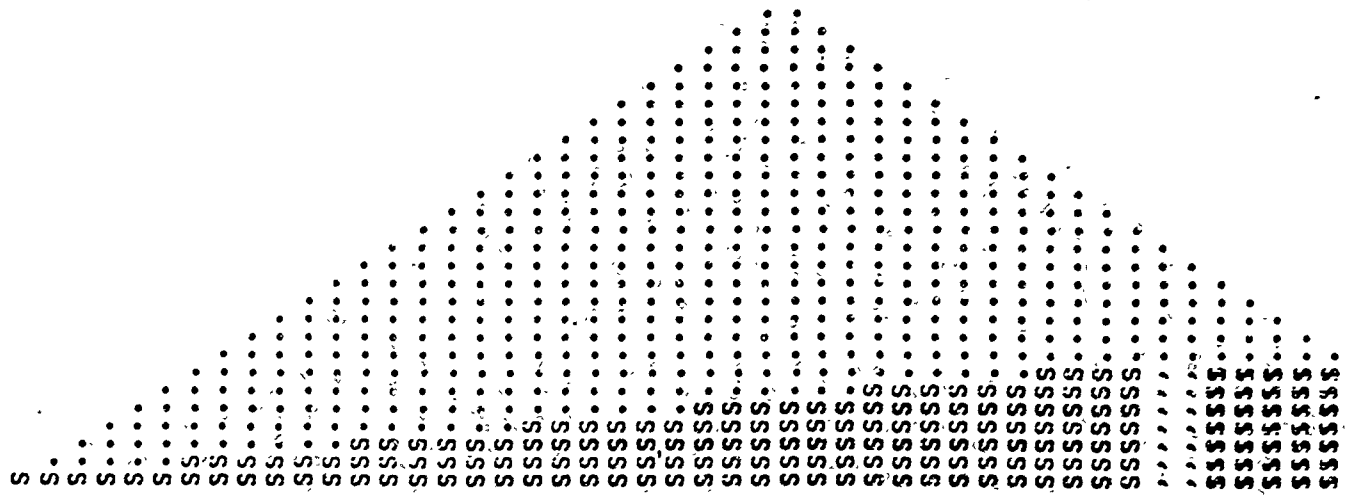
MACH NUMBER = 1.50900      SPEED OF SOUND = 13392.000 L/T      RHO=0.11460000E-06

	WING	TAIL
L.E. STATION (L)	0.	57.550
ROOT CHORD (L)	53.500	6.000
L.E. SPAN (L)	0.	8.000
T.E. SPAN (L)	8.000	8.000
TIP CHORD (L)	0.	6.000
TOTAL AREA (L*L)	428.000	96.000
CHORDWISE BOXES	40	4
SPANWISE BOXES	7	7

TOTAL CHORDWISE BOXES = 47      BOX CHORD = 1.35443E 00 L      BOX SPAN = 1.21144E 00 L

MISSILE SUPERSONIC AIRLOADS PROGRAM (CONT'D)

MAP OF MACH BOX OVERLAY ON  
WING, TAIL, AND DIAPHRAGM  
(S) - WING  
(S) - TAIL  
(.) - WAKE  
(.) - DIAPHRAGM



MISSILE SUPERSONIC AIRLOADS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (CPS) 200.00000 47 BOXES IN CHORD DIRECTION  
 REDUCED FREQUENCY (SEMI CHORD) 1.67339 FREE STREAM MACH NUMBER 1.500

INPUT MODE SHAPE POLYNOMIAL COEFFICIENTS FOR WING  
 REFERENCED TO THE SURFACE LEADING EDGE-CENTERLINE INTERSECTION.

MODE	COEFFS.													
1	-2.7643E-03	-2.3968E-03	1.0698E-01	3.3227E-04	-1.7350E-02	-3.6455E-02	-2.0567E-05	1.0242E-03	-1.5649E-03	2.5596E-02	5.4159E-07	-2.8225E-05	2.0969E-04	-1.7662E-03
	1.4567E-03	-4.8146E-09	2.6893E-07	-3.0507E-06	2.2374E-05	-1.5766E-05	-2.0292E-05							
2	5.9081E-04	1.1346E-02	-1.4269E-01	-1.9870E-03	1.7391E-02	-5.2818E-02	1.2097E-04	-2.0628E-03	3.7740E-02	-1.1759E-01	-2.9744E-06	7.7451E-05	-1.5215E-03	4.6965E-03
	1.1664E-03	2.4952E-08	-8.3941E-07	1.0896E-05	-7.6407E-05	2.3531E-04	-7.3812E-04							
3	1.6687E-02	-1.9542E-02	-1.5043E 00	3.1005E-03	2.2035E-01	1.6944E-01	-1.9229E-04	-9.0043E-03	-2.6816E-02	8.1504E-02	4.8204E-06	1.3340E-04	9.4618E-04	-2.3806E-03
	-7.3799E-03	-4.0844E-08	-5.5376E-07	-1.4601E-05	1.3599E-04	-9.1914E-04	3.1200E-03							
4	1.3375E-01	-9.8015E-03	1.4319E 00	3.0046E-03	-3.8145E-01	6.0607E-01	-2.9098E-04	2.2713E-02	-1.2993E-01	3.2289E-01	9.6282E-06	-8.5727E-04	6.9968E-03	-3.3429E-02
	5.4256E-02	-9.6391E-08	8.2378E-06	-8.4006E-05	3.9512E-04	-1.0736E-04	-2.7726E-03							
5	-2.3479E-04	-5.1973E-03	2.3344E-01	3.7865E-04	-3.3701E-04	-2.7195E-01	-6.4710E-06	-8.1025E-04	1.3782E-02	5.7945E-02	-4.9236E-08	2.7501E-05	-2.6211E-04	-1.5177E-03
	-5.9560E-03	1.3471E-09	-2.6464E-07	2.2137E-06	-1.5090E-08	1.5586E-04	-1.3277E-04							

MISSILE SUPERSONIC AIRLIFTS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (CPS) 200.00000 47 BOXES IN CHORD DIRECTION  
 REDUCED FREQUENCY (SEMI CHORD) 1.67339 FREE STREAM MACH NUMBER 1.500

GENERALIZED FORCES FOR WING

DEFL	LOAD	REAL PART	IMAG PART	ANS VALUE	PHASE ANGLE
1	1	-4.05330E-01	1.41647E-01	4.29367E-01	160.737 DEG
1	2	2.48826E 00	-2.46939E 00	3.50561E 00	-44.762 DEG
1	3	5.69256E 00	2.42253E-01	5.69771E 00	2.437 DEG
1	4	-6.22083E 00	-1.31247E 00	6.66342E 00	-168.465 DEG
1	5	3.05956E-01	-5.45114E-02	3.09994E-01	-8.472 DEG
2	1	5.42497E 00	1.01807E-01	5.42594E 00	1.075 DEG
2	2	-1.13634E 02	5.50276E 01	1.26256E 02	154.161 DEG
2	3	-1.17337E 02	-9.03881E 01	1.48114E 02	-142.392 DEG
2	4	3.85767E 01	7.90880E 01	8.79948E 01	63.998 DEG
2	5	-1.54986E 01	1.65535E 00	1.55868E 01	173.984 DEG
3	1	-3.47591E 00	-4.56201E 00	5.73532E 00	-127.385 DEG
3	2	4.30375E 01	5.02509E 01	6.61678E 01	49.426 DEG
3	3	5.43115E 01	1.55744E 02	1.64942E 02	70.775 DEG
3	4	-8.58316E 01	-6.56561E 01	1.08064E 02	-142.586 DEG
3	5	2.34054E 01	9.49312E 00	2.52574E 01	22.877 DEG
4	1	3.10905E-01	4.44125E 00	1.45212E 00	85.996 DEG
4	2	-6.41152E 01	-8.8872E 00	6.4782E 01	-172.188 DEG
4	3	-4.63360E 01	-1.24207E 02	1.32569E 02	-118.458 DEG
4	4	-3.63002E 01	8.41059E 01	9.16052E 01	113.345 DEG
4	5	-1.47609E 01	-2.25630E 00	1.49323E 01	-171.389 DEG
5	1	-1.45288E-01	-5.12284E-02	1.54055E-01	-168.577 DEG
5	2	-8.22063E 00	7.77921E 00	1.13179E 01	136.580 DEG
5	3	2.71663E 00	1.56198E 00	3.13366E 00	29.898 DEG
5	4	-1.62163E 01	3.83596E 00	1.66638E 01	166.691 DEG
5	5	8.47165E-01	1.39315E 00	1.63051E 00	58.697 DEG



MISSILE SUPERSONIC AIRLOADS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (CPS) 200.00000 47 BOXES IN CHORD DIRECTION  
 REDUCED FREQUENCY (SEMI CHORD) 1.67339 FREE STREAM MACH NUMBER 1.500

INPUT MODE SHAPE POLYNOMIAL COEFFICIENTS FOR TAIL  
 REFERENCED TO THE SURFACE LEADING EDGE-CENTERLINE INTERSECTION

MODE

COEFFS.

1	-2.9509E-01	4.3922E-02	-6.5762E-02	-7.3360E-03	-2.6048E-03	-8.2124E-03	3.9367E-03
	-1.4897E-03	5.5863E-03	-6.6256E-04	-5.0795E-04	3.6026E-04	-2.1683E-04	-4.8161E-04
	1.5973E-04						
2	-5.2445E-03	-1.8889E-02	-1.4280E-03	9.7705E-03	5.1856E-04	-5.6169E-03	-2.6629E-03
	-1.8634E-04	-6.7727E-04	1.2652E-03	2.2149E-04	4.6749E-05	-9.4713E-06	6.8936E-05
	-9.1426E-05						
3	3.6644E-02	-2.5725E-02	-9.3449E-03	5.2614E-03	3.2757E-03	-5.2647E-05	-1.4688E-03
	-2.6833E-04	-7.2607E-04	1.7027E-04	1.3103E-04	-1.3270E-05	5.1347E-05	2.3310E-05
	-1.2438E-05						
4	-9.8849E-02	-6.4342E-03	4.6537E-02	8.2901E-04	1.8417E-02	3.7439E-04	-2.0627E-03
	2.5576E-03	-8.0436E-03	1.7425E-03	2.8345E-04	-1.8412E-04	-9.9538E-05	6.3188E-04
	-3.2428E-04						
5	-5.7341E-01	3.1192E-01	-9.6235E-03	-5.6429E-02	2.0184E-02	-2.2471E-03	1.4691E-02
	-2.9503E-03	-2.7418E-03	8.1679E-04	-1.2591E-03	1.8190E-04	1.6698E-04	1.7044E-04
	-6.1575E-05						

MISSILE SUPERSONIC AIRHEADS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (CPS) 200.00000 47 BOXES IN CHORD DIRECTION  
 REDUCED FREQUENCY (SEMI CHORD) 1.67339 FREE STREAM MACH NUMBER 1.500

GENERALIZED FORCES FOR TAIL

DEFL.	LOAD	REAL PART	IMAG PART	AWS VALUE	PHASE ANGLE
1	1	-2.38915E 02	1.28104E 02	2.71095E 02	151.000 DEG
1	2	3.49540E 01	8.58631E 01	9.27237E 01	67.854 DEG
1	3	-7.81328E 01	-1.35909E 01	7.93060E 01	-170.132 DEG
1	4	1.81209E 02	-3.54137E 01	1.84637E 02	-11.058 DEG
1	5	-9.35040E 02	9.55015E 01	9.39902E 02	174.168 DEG
2	1	-3.86021E 01	1.54966E 01	3.43021E 01	153.143 DEG
2	2	4.00729E 00	1.35986E 01	1.41767E 01	73.583 DEG
2	3	-1.60314E 01	6.41368E-01	1.60445E 01	177.709 DEG
2	4	3.01063E 01	-6.17353E 00	3.07347E 01	-11.588 DEG
2	5	-1.24952E 02	7.03793E 00	1.25155E 02	176.776 DEG
3	1	-1.43359E 01	7.51749E 00	1.61874E 01	132.328 DEG
3	2	1.61241E 00	7.73430E 00	7.90959E 00	78.224 DEG
3	3	-1.05254E 01	1.96803E 00	1.07064E 01	169.447 DEG
3	4	1.81686E 01	-4.84012E 00	1.88022E 01	-14.917 DEG
3	5	-6.27252E 01	1.56343E 00	6.27447E 01	178.572 DEG
4	1	7.90217E 01	-3.60158E 01	8.68422E 01	-24.582 DEG
4	2	-1.19493E 01	-2.54166E 01	2.80859E 01	-115.180 DEG
4	3	4.69554E 01	5.26476E 00	4.72496E 01	6.397 DEG
4	4	-8.27282E 01	2.59885E 00	8.67142E 01	162.560 DEG
4	5	2.76223E 02	-8.07811E 00	2.76342E 02	-1.675 DEG
5	1	-1.26964E 01	3.06863E 00	1.38620E 01	166.413 DEG
5	2	5.47163E 00	-2.04463E 01	2.11959E 01	-75.018 DEG
5	3	5.91118E 01	-2.80330E 01	6.54221E 01	-25.372 DEG
5	4	-6.53213E 01	2.68424E 01	7.66214E 01	157.661 DEG
5	5	1.87717E 01	3.74297E 01	4.18731E 01	63.365 DEG

MISSILE SUPERSONIC AIRLOADS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (GPM) 200.00000 47 BOXES IN CHORD DIRECTION  
 REDUCED FREQUENCY (SEMI CHORD) 1.67339 FUEL STREAM MACH NUMBER 1.530

GENERALIZED FORCES FOR WING + TAIL

DEFL. LOAD	REAL PART	IMAG PART	ABS VALUE	PHASE ANGLE
1 1	-2.46521E 02	1.20246E 02	2.71917E 02	151.814 DEG
1 2	3.74423E 01	8.34437E 01	9.14018E 01	65.826 DEG
1 3	-7.24402E 01	-1.10486E 01	7.36598E 01	-169.559 DEG
1 4	1.74680E 02	-3.67462E 01	1.78904E 02	-11.880 DEG
1 5	-9.34674E 02	9.54470E 01	9.39535E 02	174.169 DEG
2 1	-2.33771E 01	1.55984E 01	2.96179E 01	148.220 DEG
2 2	-1.09626E 02	6.86261E 01	1.29335E 02	147.953 DEG
2 3	-1.33368E 02	-6.97468E 01	1.60753E 02	-146.462 DEG
2 4	6.86850E 01	7.29145E 01	1.00171E 02	46.711 DEG
2 5	-1.40450E 02	8.69328E 00	1.40719E 02	176.458 DEG
3 1	-1.78118E 01	2.95548E 00	1.80554E 01	178.579 DEG
3 2	4.46499E 01	5.79932E 01	7.31903E 01	52.407 DEG
3 3	4.37861E 01	1.57705E 02	1.63671E 02	74.483 DEG
3 4	-6.76632E 01	-7.04962E 01	9.77140E 01	-133.825 DEG
3 5	-3.93198E 01	1.10566E 01	4.08447E 01	164.294 DEG
4 1	7.93326E 01	-3.15745E 01	8.53851E 01	41.783 DEG
4 2	-7.60644E 01	-3.43043E 01	8.34421E 01	-155.725 DEG
4 3	6.19323E-01	-1.18942E 02	1.18944E 02	-89.782 DEG
4 4	-1.19028E 02	1.10094E 02	1.62137E 02	137.233 DEG
4 5	2.61463E 02	-1.03344E 01	2.61667E 02	-2.263 DEG
5 1	-1.28417E 01	3.01741E 00	3.31914E 01	166.777 DEG
5 2	-2.74901E 00	-1.26669E 01	1.29617E 01	-182.245 DEG
5 3	6.18284E 01	-2.64710E 01	6.72567E 01	-23.178 DEG
5 4	-8.15376E 01	3.06784E 01	8.71180E 01	159.381 DEG
5 5	1.86189E 01	3.88229E 01	4.34989E 01	63.191 DEG

5.5 PROGRAM LISTING

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5      FORTRAN NLSTOU,DECK                                SUP/0210
5      INCLUDE IR:F                                        SUP/0220
CHARLY  DRIV                                             SUP/0230
COMPLEX CZE(0),VPIC,SS,DC,U,PHIW,SPHI,PHI,PHITE,DPHI,FXF  SUP/0240
COMMON/C1/KROX(2000),XF(5),YE(3),AG(3),X1,X2,X3,X4,Y1,Y2,BETA,NBS SUP/0250
COMMON/C2/AS,FMACH,FMACH(6),NFREQ,FREQ(10),NMODE,NSURF,LVPIC,LSSVP SUP/0260
COMMON/C3/CI(10,28,2),NT(10,2),NF(10,2),NTMAX(2),PXY(28),FN(28)  SUP/0270
COMMON/C4/VPIC(1275),SS(2000),DU(28,2),U(10,10,3),PHIW(50),SPHI  SUP/0280
COMMON/C5/MOR(51),NBL(50),KC(50),KL(28),BSL(20),DXE(7),TPI,U     SUP/0290
COMMON/C6/X,Y,DX,DY,EM,EK,FKR,EKR,NP,MP,NB,NBUX,KODE,MODE,NBW,NB1 SUP/0300
COMMON/C7/CZFR0,PHI,PHITE,DPHI,XL,NS,NTM,K,J,QR,QI,UAS,UAN,IFR,TWL SUP/0310
COMMON/C8/R00                                               SUP/0320
1  CALL MAIN                                               SUP/0330
DO 1000 MACI=1,FMACH                                       SUP/0340
FM=FMACH(MACI)                                             SUP/0350
IF (FM.LT.1.1) GO TO 1000                                  SUP/0360
CALL COUL                                                 SUP/0370
TOB = TWL/BETA                                           SUP/0380
CALL POUT(1)                                              SUP/0390
U = AS*FM                                                 SUP/0400
TPI = TPI/U                                              SUP/0410
RFM=DX*(EM/PIA)**2                                       SUP/0420
DO 500 IFR=1,NFR=0                                       SUP/0430
FK=IFR*(IFR)*TPI                                         SUP/0440
FKR = FK*RFM                                             SUP/0450
EKR = FK*X1/2.0                                          SUP/0460
CALL CALI                                               SUP/0470
IF (LVPIC.NE.0) CALL POUT(2)                              SUP/0480
ARG=EK*DX                                                 SUP/0490
FXF=CMPLX(COS(ARG),-SIN(ARG))                          SUP/0500
DO 500 M0DE=1,N10DE                                       SUP/0510
DO 10 J=1,50                                             SUP/0520
10  J0(J,1)=CZE*0                                         SUP/0530
IF (NF(M0DE,1).EQ.1) GO TO 210                          SUP/0540
X=0.5*DX                                                 SUP/0550
NB=1                                                      SUP/0560
IF (LSSVP.NE.0) CALL POUT(3)                              SUP/0570
DO 200 NP=1,N100X                                       SUP/0580
KD = KROX(NP)                                             SUP/0590
NS = 1                                                    SUP/0600
GO TO (70,60,70,60,60,70,70),KD                        SUP/0610
60  NS = 2                                                SUP/0620
70  MH = MOB(NP)                                          SUP/0630
Y=0.0                                                     SUP/0640
DO 100 MP=1,M00X                                       SUP/0650
MP = MP                                                  SUP/0660
KODE=(K00X(NP))                                          SUP/0670
SPHI=CZFR0                                               SUP/0680
IF (MP.GT.1) CALL PHIT                                  SUP/0690
SPHI=SPHI*DY                                             SUP/0700
PHI=CZFR0                                                SUP/0710
GO TO (40,40,40,40,40,20,30),KODE                       SUP/0720
20  SPHI=SPHI-PHIT(MP)                                    SUP/0730
PHI=PHIW(MP)                                             SUP/0740
PHIW(MP)=PHIW(MP)*FXF                                    SUP/0750
GO TO 50                                                 SUP/0760
30  IF (KD.EQ.6) GO TO 40                                SUP/0770
50  SS(NB)=-SPHI/VPIC/DY                                  SUP/0780
GO TO 90                                                 SUP/0790
40  CALL WASH                                             SUP/0800

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IF(KD.LT.6) SS(NB) = SS(NB)-ARLE*TOB*(SS(NB)+SPHI/VPIC/DY) SUP70810
IF(KODE.EQ.6) GO TO 90 SUP70820
PHI=SPHI+SS(NB)*VPIC*DY SUP70830
IF(KODE.EQ.5) PHIW(MP)=PHI*EXF SUP70840
IF(NP.EQ.NBOX-1) PHIW(MP)=PHI SUP70850
IF(NP.EQ.NBOX) PHIT=PHI+(PHI-PHIW(MP))*DXE(5) SUP70860
CALL DQIJ SUP70870
90 IF(LSSVP.NE.0) CALL PJUT(4) SUP70880
NB = NB + 1 SUP70890
KD = KODE SUP70900
100 Y=Y+DY SUP70910
200 X=X+DX SUP70920
210 DO 400 MO=1,NMODE SUP70930
DO 300 NS=1,NSURF SUP70940
Q(MODE,MO,NS)=CZERO SUP70950
NTM=NT(MO,NS) SUP70960
DO 300 N=1,NT SUP70970
300 Q(MODE,MO,NS)=Q(MODE,MO,NS)+C0(MO,N,NS)*DQ(N,NS) SUP70980
Q(MODE,MO,3) = CZERO SUP70990
400 Q(MODE,MO,3)=Q(MODE,MO,1)+Q(MODE,MO,2) SUP71000
500 CONTINUE SUP71010
QF = 2.0*DX*DY*RHO SUP71020
DO 600 NS=1,3 SUP71030
CALL POUT(6) SUP71040
DO 700 J=1,NMODE SUP71050
DO 700 K=1,NMODE SUP71060
QR = QF*REAL(Q(K,J,NS)) SUP71070
QI = QF*AIMAG(Q(K,J,NS)) SUP71080
QAR=SQRT(QI*QI+QR*QR) SUP71090
QAN=0.0 SUP71100
IF(QAR.NE.0.0) QAN=57.29578*AIAN2(QI,QR) SUP71110
700 CALL POUT(7) SUP71120
IF(NSURF.EQ.1) GO TO 900 SUP71130
800 CONTINUE SUP71140
900 CONTINUE SUP71150
1000 CONTINUE SUP71160
GO TO 1 SUP71170
END SUP71180
$ FORTRAN NLST00,DECK SUP71190
$ INCODE I8PF SUP71200
CHAIN MAIN SUP71210
SUBROUTINE MAIN SUP71220
COMMON/C1/K,DX(20*0),XE(5),YE(3),AR(3),X1,X2,X3,X4,Y1,Y2,BETA,NBS SUP71230
COMMON/C2/AS,FMACH,FNACH(6),NFREQ,FREQ(10),NMODE,NSURF,LVPIC,LSSVP SUP71240
COMMON/C3/C0(10,28,2),NT(10,2),NF(10,2),NTMAX(2),PXY(28),FN(28) SUP71250
COMMON/C6/X,Y,DX,DY,FM,EK,EKB,EKR,NP,MP,NB,NBOX,KODE,MODE,NBS,NBT SUP71260
COMMON/C8/RHO SUP71270
READ(5,11) (XF(I),I=1,5) SUP71280
READ(5,11) (YE(I),I=1,3),AS,RHO SUP71290
RHO = RHO/1000.0 SUP71300
READ(5,12) FMACH,NFREQ,NMODE,NBW,LVPIC,LSSVP SUP71310
READ(5,11) (FMACH(I),I=1,NMACH) SUP71320
READ(5,11) (FREQ(I),I=1,NFREQ) SUP71330
NSURF=? SUP71340
IF(XE(4).LT.XE(5)) GO TO 10 SUP71350
NSURF=1 SUP71360
XE(4)=XE(3) SUP71370
XF(5)=XE(3) SUP71380
10 NTMAX(1)=0 SUP71390
NTMAX(2)=0 SUP71400

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DO 30 MODE=1,4,MODE
DO 30 I=1,N,CURF
DO 20 J=1,2,
20 CO(MODE,J,I)=0.0
RFAD(5,12) TM,NFI
NT(MODE,I)=TM
NTMAX(I)=MAX0(NTMAX(I),NTM)
NF(MODE,I)=NFI
30 REAI(5,11) (CO(MODE,J,I),J=1,NTM)
11 FORMAT(6E12.8)
12 FORMAT(6I12)
RETURN
END
$
FORTRAN NLS100,DECK
$
INCODE IRMF
CCONS
CONS
BLOCK DATA
COMPLEX CZERO,VPIC,SS,DO,Q,PHIW,SPHI,PHI,PHITE,UPHI
COMMON/C3/C0(10,2),NT(10,2),NF(10,2),NTMAX(2),PXY(28),FN(28)
COMMON/C4/VPIC(1275),SS(2000),DO(28,2),Q(10,10,3),PHIW(50),SPHI
COMMON/C5/MUR(50),NBL(50),KC(50),KL(28),BSL(20),DXE(7),IPI,U
COMMON/C7/CZERO,PHI,PHITE,DPHI,XL,NS,NTM,K,J,QR,QI,QAB,QAN,IFR,IWL
COMMON/C8/R00
DATA KC/1,2,4,7,11,16,22,29,37,46,56,67,79,92,106,121,137,154,172,
119,1,211,232,254,277,301,326,352,379,407,436,466,497,529,562,596,
263,1,657,704,742,781,821,862,904,947,991,1036,1082,1129,1177,1226,
3FN/0.,1.,0.,2.,1.,0.,3.,2.,1.,0.,4.,3.,2.,1.,0.,5.,4.,3.,2.,1.,0.,
4 6.,5.,4.,3.,2.,1.,0./,IPI/6.2831853/,CZERO/(0.0,0.0)/
DATA KL/1,1,2,3,1,4,5,6,1,7,8,9,10,1,11,12,13,14,15,1,16,17,18,
1 19,20,21,1/
END
$
FORTRAN NLS100,DECK
$
INCODE IRMF
CCODE
CODE
SUBROUTINE CODE
COMPLEX CZERO,VPIC,SS,DO,Q,PHIW,SPHI,PHI,PHITE,UPHI
COMMON/C1/KI OX(2000),XF(5),YE(3),AR(3),X1,X2,X3,X4,Y1,Y2,BETA,NBS
COMMON/C2/A,AMACH,FMACH(6),NFREQ,FREQ(10),NMODE,NSURF,LVPIC,LSSVPS
COMMON/C3/C0(10,2),NT(10,2),NF(10,2),NTMAX(2),PXY(28),FN(28)
COMMON/C4/VPIC(1275),SS(2000),DO(28,2),Q(10,10,3),PHIW(50),SPHI
COMMON/C5/MUR(50),NBL(50),KC(50),KL(28),BSL(20),DXE(7),IPI,U
COMMON/C6/X,Y,IX,IY,EM,FK,EKB,EKR,MP,MB,NB,NBOX,KUDE,MODE,NBW,NBT
COMMON/C7/CZERO,PHI,PHITE,DPHI,XL,NS,NTM,K,J,QR,QI,QAB,QAN,IFR,IWL
COMMON/C8/R00
BETA = SQRT((FM * FM)-1.0)
X1 = XF(3) - XF(1)
X2 = XF(3) - XF(2)
X3 = XF(4) - XF(1)
X4 = XF(5) - XF(4)
X5 = XF(5) - XF(1)
Y1 = YE(2) - YE(1)
Y2 = YE(3) - YE(1)
IF(X2.GT.X1.OR.X1.GT.X3.OR.X3.GT.X5.OR.X2.LT.0.0) GO TO 50
IF(Y1.GT.Y2.OR.Y1.LT.0.0) GO TO 50
TWI = 0.0
IF(Y2.NE.Y1) TWI = (X1 - X2) / (Y2 - Y1)
AR(1) = (Y2*(X2+X1) - Y1 * (X2+X1))
AR(2) = Y2*X4+2.0
AR(3) = AR(1) + AR(2)
10 DX = X1/(FL*AT(1BW) -0.5)

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IF (50.0 * DX .GT. X5) GO TO 20
15 NBW = NBW-1
GO TO 10
20 DY = DX/BETA
YN1 = Y1/DY
YN2 = Y2/DY
XNL = YN2 - (X1-X2) / DX
XNT = YN2 + X5/DX
XNLE = X3/DX
XNTE = X5/DX
NBOX = XNTE + 0.5
NBS = Y2/DY + 1.0
NBT = X4/DX + 0.5
DXF(1) = 1.0
DXF(2) = 1.0
DXF(3) = 0.5
DXF(4) = AINT(XNLE + 1.5) - XNLE
DXF(5) = XNLE - FLOAT(NBOX-1)
DXF(6) = 0.0
DXE(7) = 0.0
X = 0.5 * DX
NR = 0
DO 40 NP = 1, NBOX
XN = FLOAT(NP) - 0.5
YW = YN2
IF (TWL .GT. 0.0) YW = AMIN1(YW, YN1 + XN / (TW2/BETA))
IF (X .GT. XE(2)) GO TO 24
MB = MIN1(AMAX1(YW, XN + YN1), XNT - XN) + 1
GO TO 28
24 MB = MIN1(AMAX1(XNL + XN, XN + YN1), XNT - XN) + 1
28 MOB(NP) = MB
KODE = 1
IF (NP .EQ. NBW) KODE = 3
IF (NSURF .EQ. 1) GO TO 29
IF (X .GT. X1) KODE = 6
IF (X .GT. X3 ) KODE = 4
IF (X .GT. X3 + DX) KODE = 2
IF (NP .EQ. NBOX) KODE = 5
29 IF (NR + MB .GT. 2000) GO TO 15
NBI(NP) = NR
DO 30 MP = 1, NR
YN = MP - 1
NB = NB + 1
IF (YN .GT. YW) KODE = 7
30 KBOX (NR ) = KODE
40 X = X + DX
RETURN
50 CALL EXIT
RETURN
END

```

```

$ FOPTRAN NLSTOU,DECK
$ INCODE IR:F
C'CAFJ CAFJ

```

```

SUBROUTINE CAFJ

```

```

COMPLEX CZERO,VPIC,SS,DO,Q,PHIW,SPHI,PHI,PHITE,DPHI

```

```

DIMENSION P(5),W(5)

```

```

COMMON/C4/VPIC(1275),SS(2000),DO(28,2),G(10,10,3),PHIW(50),SPHI

```

```

COMMON/C5/MOB(50),NBL(50),KC(50),KL(28),BSL(20),DXE(7),TPI,U

```

```

COMMON/C6/X,Y,DX,DY,EM,EK,EKB,EKR,NP,RP,NB,NBOX,KODE,MODE,NBW,NBT

```

```

COMMON/C7/CZERO,PHI,PHITE,DPHI,XL,NS,NTM,K,J,UR,QI,QAB,QAN,IFR,TWLSUP72420

```

SUP71830  
SUP71840  
SUP71850  
SUP71860  
SUP71870  
SUP71880  
SUP71890  
SUP71900  
SUP71910  
SUP71920  
SUP71930  
SUP71940  
SUP71950  
SUP71960  
SUP71970  
SUP71980  
SUP71990  
SUP72000  
SUP72010  
SUP72020  
SUP72030  
SUP72040  
SUP72050  
SUP72060  
SUP72070  
SUP72080  
SUP72090  
SUP72100  
SUP72110  
SUP72120  
SUP72130  
SUP72140  
SUP72150  
SUP72160  
SUP72170  
SUP72180  
SUP72190  
SUP72200  
SUP72210  
SUP72220  
SUP72230  
SUP72240  
SUP72250  
SUP72260  
SUP72270  
SUP72280  
SUP72290  
SUP72300  
SUP72310  
SUP72320  
SUP72330  
SUP72340  
SUP72350  
SUP72360  
SUP72370  
SUP72380  
SUP75050  
SUP72400  
SUP72410  
SUP72420

```

COMMON/C8/RHO
DATA P/0.95308992,0.76923465,0.5,0.23076535,0.34691008/
1  , W/0.11846344,0.23931434,0.28444444,0.23931434,0.11846344/
PI = TPI/2.0
IF(EKB.GT.0.0) GO TO 10
VPIC = (-1.0,0.0)
GO TO 30
10 VPIC = CZERO
DO 20 I = 1,5
ARG = EKB*P(I)/2.0
F = -(0.5*ARG/E4)**2
ZJ = 1.0
FI = 1.0
AE = 1.0
DO 15 K = 1,20
AE = AE * F/FI**2
FI = FI + 1.0
IF(ABS(AE).LE.1.E-5) GO TO 20
15 ZJ = ZJ + AE
20 VPIC = VPIC - ZJ*W(I)*CMPLX(COS(ARG),-SIN(ARG))
30 DO 80 NP = 2,NBOX
KI = KC(NP)
KZ = KC(NP+1) - 1
DO 40 K = KI,KZ
40 VPIC(K) = CZERO
NU = NP - 1
DO 60 I = 1,5
X = FLOAT(NU) - 0.5 + P(I)
ARG = EKB*X
PHI = W(I)*CMPLX(-COS(ARG),SIN(ARG))*2.0/PI
CALL BSLS(ARG/F4,N)
K = KC(NP)
DO 70 MP = 1,NU
EOX = (FLOAT(MP) - 0.5)/X
C = SQRT(1.0 - EOX**2)
AF = 2.0*ATAN(EOX/(1.0 + C))
S = 2.0*EOX*C
C = 2.0*C*C - 1.0
SO = 0.0
VIN = BSL*AF
F = 1.0
FI = 1.0
DO 50 L = 1,N
VIN = BSL(L+1)*S/FI - VIN
SN = 2.0*S*C - SO
SO = S
S = SN
F = -F
50 FI = FI + 1.0
DPHI = PHI*VIN*F
VPIC(K) = VPIC(K) + DPHI
VPIC(K+1) = VPIC(K+1) - DPHI
IF(MP.EQ.1) VPIC(K) = VPIC(K) + DPHI
70 K = K + 1
80 VPIC(K) = VPIC(K) + PI*BSL*PHI/2.0
RETURN
END

```

```

$   FORTRAN NLSTDU,DECK
$   INCOOF IR:F
CBSLS      BSLS

```

```

SUP72430
SUP72440
SUP72450
SUP72460
SUP72470
SUP72480
SUP72490
SUP72500
SUP72510
SUP72520
SUP72530
SUP72540
SUP72550
SUP72560
SUP/2570
SUP72580
SUP72590
SUP72600
SUP72610
SUP72620
SUP72630
SUP72640
SUP72650
SUP72660
SUP72670
SUP72680
SUP72690
SUP72700
SUP72710
SUP72720
SUP72730
SUP72740
SUP72750
SUP72760
SUP72770
SUP72780
SUP72790
SUP72800
SUP72810
SUP72820
SUP72830
SUP72840
SUP/2850
SUP72860
SUP72870
SUP72880
SUP72890
SUP72900
SUP72910
SUP72920
SUP72930
SUP72940
SUP72950
SUP72960
SUP72970
SUP72980
SUP72990
SUP73000
SUP73010
SUP73020

```



```

SUBROUTINE #SLS(ARG,N)
COMMON/C5/HUB(50),NBL(50),KC(50),KL(28),BSL(20),DXE(7),TPI,U
COMMON/C8/RHO
DO 1 I=1,20
1 BSL(I) = 0.0
ASQ = ARG**2
IF(ASQ.LT.0.01) GO TO 50
N = MIN1(17.0,(ARG + 10.0))
F = 2*N + 4
BSL(N+2) = (4.0*F*(F-1.0)/ASQ-(F-1.0)/F)*0.3E-30
PF = 0.0
J = 0
DO 10 I = J,N
M = N - I + 1
F = 2*M + 1
BSL(M) = (4.0*(F-1.0)/ASQ-1.0/F-1.0/(F-2.0))*BSL(M+1)-BSL(M+2)/F
10 PF = PF + 2.0*(F-2.0)*BSL(M+1)
PF = PF + BSL(I)
F = 0.0
IF(ABS(PF).GT.1.0) F = ABS(PF)*1.E-10
N = N + 2
DO 30 I = 1,N
IF(F.GE.ABS(BSL(I))) GO TO 20
BSL(I) = BSL(I)/PF
GO TO 30
20 BSL(I) = 0.0
30 CONTINUE
DO 40 I = 1,N
IF(ABS(BSL(N)).GT.1.0 E-7) RETURN
40 N = N - 1
RETURN
50 BSL(2) = -0.125*ASQ
BSL(1) = 1.0 - 2.0*BSL(2)
N = 2
RETURN
END

```

```

$ FORTRAN NESTOU,DECK
$ INCODE IBMF
CARLE ARLE

```

```

FUNCTION ARLE(TOB)
COMMON/C1/KBOX(200.0),XF(5),YE(3),AR(3),X1,X2,X3,X4,Y1,Y2,BETA,NBS
COMMON/C6/X,Y,DX,DY,EM,EK,EKB,EKR,NP,PP,NB,NBOX,KODE,MODE,NBW,NBT
COMMON/C8/RHO
IF(X-0.5*DX.GE.X1-X2) GO TO 10
YT = (Y-Y1)/DY+0.5-(X/DX-0.5)/TOB
XR = YT*TOB
YB = AMAX1(0.0,AMIN1(1.0,YT-1.0/TOB))
YT = AMIN1(1.0,AMAX1(0.0,YT))
XL = AMAX1(0.0,AMIN1(1.0,XR-TOB))
XR = AMIN1(1.0,AMAX1(0.0,XR))
ARLE = AMAX1(0.5*(YT*(XR+XL)+YB*(XR-XL)),0.0)
IF(MP.EQ.1) ARLE = 2.0*ARLE
RETURN
10 ARLE = AMIN1(1.0,AMAX1(0.0,(Y-Y2)/DY+0.5))
RETURN
END

```

```

$ FORTRAN NESTOU,DECK
$ INCODE IBMF
CPHIB PHIB
SUBROUTINE PHIB

```

SUP73030  
SUP73040  
SUP73050  
SUP73060  
SUP73070  
SUP73080  
SUP73090  
SUP73100  
SUP73110  
SUP73120  
SUP73130  
SUP73140  
SUP73150  
SUP73160  
SUP73170  
SUP73180  
SUP73190  
SUP73200  
SUP73210  
SUP73220  
SUP73230  
SUP73240  
SUP73250  
SUP73260  
SUP73270  
SUP73280  
SUP73290  
SUP73300  
SUP73310  
SUP73320  
SUP73330  
SUP73340  
SUP73350  
SUP73360  
SUP73370  
SUP73380  
SUP73390  
SUP73400  
SUP73410  
SUP73420  
SUP73430  
SUP73440  
SUP73450  
SUP73460  
SUP73470  
SUP73480  
SUP73490  
SUP73500  
SUP73510  
SUP73520  
SUP73530  
SUP73540  
SUP73550  
SUP73560  
SUP73570  
SUP73580  
SUP73590  
SUP73600  
SUP73610  
SUP73620

```

COMPLEX CZERO,VPIC,SS,DO,Q,PHIW,SPHI,PHI,PHITE,DPHI SUP73630
COMMON/C4/VPIC(1275),SS(2000),DO(28,2),Q(10,10,3),PHIW(50),SPHI SUP75050
COMMON/C5/MOB(50),NBL(50),KC(50),KL(28),BSL(28),DXE(7),TPI,U SUP73650
COMMON/C6/X,Y,DX,DY,EM,EK,EKB,EKR,MP,MP,NB,NBOX,KODE,MODE,NBW,NBT SUP73660
COMMON/C7/CZERO,PHI,PHITE,DPHI,XL,NS,NTM,K,J,QR,QI,QAB,QAN,IFR,TWL SUP73670
COMMON/C8/RHO SUP73680
DO 20 I=2, NP SUP73690
NU=NP-I+1 SUP73700
JL=MAX0(1,MP-I+1) SUP73710
JR=MIN0(MOB(NU),MP+I-1) SUP73720
NJ=NBL(NU)+JL SUP73730
DO 20 J=JL, JR SUP73740
K=KC(I)+IABS(MP-J) SUP73750
DPHI=VPIC(K) SUP73760
IF (J.GT.I-MP+1.OR.J.EQ.1) GO TO 10 SUP73770
K=KC(I)+MP+J-2 SUP73780
DPHI=DPHI+VPIC(K) SUP73790
10 SPHI=SPHI+DPHI*SS(NJ) SUP73800
20 NJ=NJ+1 SUP73810
RETURN SUP73820
END SUP73830
$ FORTRAN NLSTOU,DECK SUP73840
$ INCODE IBMF SUP73850
CQC1J DQ1J SUP73860
SUBROUTINE DQ1J SUP73870
COMPLEX CZERO,VPIC,SS,DO,Q,PHIW,SPHI,PHI,PHITE,DPHI SUP73880
COMMON/C1/KI,QX(2000),XE(5),YE(3),AR(3),X1,X2,X3,X4,Y1,Y2,BETA,NBS SUP73890
COMMON/C3/CO(10,28,2),NT(10,2),NF(10,2),NTMAX(2),PXY(28),FN(28) SUP73900
COMMON/C4/VPIC(1275),SS(2000),DO(28,2),Q(10,10,3),PHIW(50),SPHI SUP75050
COMMON/C5/MOB(50),NBL(50),KC(50),KL(28),BSL(28),DXE(7),TPI,U SUP73920
COMMON/C6/X,Y,DX,DY,EM,EK,EKB,EKR,MP,MP,NB,NBOX,KODE,MODE,NBW,NBT SUP73930
COMMON/C7/CZERO,PHI,PHITE,DPHI,XL,NS,NTM,K,J,QR,QI,QAB,QAN,IFR,TWL SUP73940
COMMON/C8/RHO SUP73950
NTM = NTMAX(NS) SUP73960
DPHI=PHI SUP73970
IF(MP.EQ.1) DPHI=0.5*DPHI SUP73980
CON = U*DXE(KODE) SUP73990
DO 20 K=1,NIM SUP74000
KK=K*(K) SUP74010
20 DO(K,NS) = DO(K,NS) + DPHI*CON*CMPLX(PXY(KK)*FN(K),-EK*PXY(K)) SUP74020
IF(KODF.NE.3) GO TO 50 SUP74030
DO 30 K = 1,NTM SUP74040
30 DO(K,1) = DO(K,1) -U*DPHI*PXY(K)/DX SUP74050
ARG = EK*(X3 - X1) SUP74060
DPHI = -DPHI*CMPLX(COS(ARG),-SIN(ARG)) SUP74070
XL = 0.0 SUP74080
CALL QEGE SUP74090
50 IF(KODE.NE.5) RETURN SUP74100
XL = X4 SUP74110
IF(MP.EQ.1)PHITE = 0.5*PHITE SUP74120
DPHI = PHITF SUP74130
CALL QEGE SUP74140
RETURN SUP74150
END SUP74160
$ FORTRAN NLSTOU,DECK SUP74170
$ INCODE IBMF SUP74180
CQEGE QEGE SUP74190
SUBROUTINE QEGE SUP74200
COMPLEX CZERO,VPIC,SS,DO,Q,PHIW,SPHI,PHI,PHITE,DPHI SUP74210
COMMON/C4/VPIC(1275),SS(2000),DO(28,2),Q(10,10,3),PHIW(50),SPHI SUP75050

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```

COMMON/C5/MOR(50),NBL(50),KC(50),KL(28),BSL(20),DXE(7),TP1,U      SUP74230
COMMON/C6/X,Y,DX,DY,EM,EK,EKB,EKR,NP,MP,NB,NBOX,KODE,MODE,NBW,NBT  SUP74240
COMMON/C7/CZERO,PHI,PHITE,DPHI,XL,NS,NTM,K,J,QR,QI,QAB,QAN,IFR,TWL  SUP74250
COMMON/C8/RHO      SUP74260
PX=1.0/DX      SUP74270
IF(XL.EQ.0.0) GO TO 30      SUP74280
YX=Y/XL      SUP74290
K=1      SUP74300
DO 20 N=1,7      SUP74310
PY=PX      SUP74320
DO 10 M=1,N      SUP74330
DQ(K,2) = DQ(K,2) -U*DPHI*PY      SUP74340
IF(K.EQ.NTM) RETURN      SUP74350
K=K+1      SUP74360
10 PY=PY*YX      SUP74370
20 PX=PX*XL      SUP74380
RETURN      SUP74390
30 K=0      SUP74400
DO 40 N=1,7      SUP74410
K=K+N      SUP74420
IF(K.GT.NTM) RETURN      SUP74430
DQ(K,2) = DQ(K,2) -U*DPHI*PX      SUP74440
40 PX=PX*Y      SUP74450
RETURN      SUP74460
END      SUP74470
$   FORTRAN NLST00, D=CK      SUP74480
$   INCODE IBM#      SUP74490
CWASH      WASH      SUP74500
SUBROUTINE WASH      SUP74510
COMMON/CZERO,VPIC,SS,DQ,Q,PHIW,SPHI,PHI,PHITE,DPHI      SUP74520
COMMON/C1/KBOX(2000),XE(5),YE(3),AR(3),X1,X2,X3,X4,Y1,Y2,BETA,NBS      SUP74530
COMMON/C3/CO(10,28,2),NT(10,2),NF(10,2),NTMAX(2),PXY(28),FN(28)      SUP74540
COMMON/C4/VPIC(1275),SS(2000),DQ(28,2),Q(10,10,3),PHIW(50),SPHI      SUP75050
COMMON/C5/MOR(50),NBL(50),KC(50),KL(28),BSL(20),DXE(7),TP1,U      SUP74560
COMMON/C6/X,Y,DX,DY,EM,EK,EKB,EKR,NP,MP,NB,NBOX,KODE,MODE,NBW,NBT      SUP74570
COMMON/C7/CZERO,PHI,PHITE,DPHI,XL,NS,NTM,K,J,QR,QI,QAB,QAN,IFR,TWL      SUP74580
COMMON/C8/RHO      SUP74590
XP = X      SUP74600
IF(NS.EQ.2) XP = X - X3      SUP74610
PXY = 1.0      SUP74620
DO 10 N = 2,28      SUP74630
10 PXY(N) = 0.0      SUP74640
TM = NTMAX(NS)      SUP74650
ID = SQRT(2.0*TM) - 0.5      SUP74660
IF(ID.EQ.0) GO TO 60      SUP74670
K = 1      SUP74680
IF(XP.EQ.0.0) GO TO 40      SUP74690
YX = Y/XP      SUP74700
PX = XP      SUP74710
DO 30 N = 1,10      SUP74720
K = K + 1      SUP74730
PXY(K) = PX      SUP74740
DO 20 M = 1,N      SUP74750
K = K + 1      SUP74760
20 PXY(K) = PXY(K-1)*YX      SUP74770
30 PX = PX*XP      SUP74780
GO TO 60      SUP74790
40 PX = 1.0      SUP74800
DO 50 N = 1,10      SUP74810
PXY(K) = PX      SUP74820

```

```

K = K + N + 1
50 PX = PX*Y
60 NTH = NT(MODE,NS)
Z = CO(MODE,1,NS)
DZ = 0.0
IF(NTH.EQ.1) GO TO 80
DO 70 K = 2,NTH
7 = Z + PXY(K)*CO(MODE,K,NS)
KK = KL(K)
70 DZ = DZ + PXY(KK)*CO(MODE,K,NS)*FN(K)
80 SS(NB) = U*CMPI X(DZ,EK*Z)
RETURN
END
S FORTRAN NLSTOU,DECK
CPOUT POUT
SUBROUTINE POUT(IND)
COMPLEX CZERO,VPIC,SS,DU,Q,PHIW,SPHI,PHI,PHITE,DPHI
DIMENSION CARDS (25,50)
DIMENSION SW(5,6),SURF(2,3),COD(7),C(50)
COMMON/C1/KPOX(2000),XE(5),YE(3),AR(3),X1,X2,X3,X4,Y1,Y2,BETA,NBS
COMMON/C2/AS,NMACH,FMACH(6),NFREQ,FREQ(10),NMODE,NSURF,LVPIC,LSSVPS
COMMON/C3/CO(10,28,2),N1(10,2),NF(10,2),NTHAX(2),PXY(28),FN(28)
COMMON/C4/VPIC(1275),SS(2000),DU(28,2),Q(10,10,3),PHIW(50),SPHI
COMMON/C5/MOB(50),NRL(50),KC(50),KL(28),BSL(20),DXE(7),TPI,U
COMMON/C6/X,Y,DX,DY,EM,EK,EKB,EKR,MP,MP,NB,NBOX,KODE,MODE,NBW,NBT
COMMON/C7/CZERO,PHI,PHITE,DPHI,XL,NS,NTH,K,J,QR,Q1,QAB,QAN,IFR,TWLS
COMMON/C8/RFO
DATA (SW(1,I),I=1,6)/26HMAP OF MACH BOX OVERLAY ON,
1 26HWING, TAIL, AND DIAPHRAGM ,
2 26H (S) - WING ,
3 26H (S) - TAIL ,
4 26H (.) - WAKE ,
5 26H (.) - DIAPHRAGM /
DATA (SURF(1,I),I=1,3)/8HWING ,8HTAIL ,11HWING + 7TAIL /
DATA COD/1HS,1HS,1HS,1HS,1HS,1H,1H./
GO TO (10,20,30,40,50,60,70),IND
10 WRITE(6,11)FM,AS,RHO,XE(1),XE(4),X1,X4,Y1,Y2,Y2,Y2,X2,X4,AR(1),
1 AR(2),NBW,NBT,NBS,NBS
11 FORMAT(1H1////////30X,43HMAC/NA: MISSILE SUPERSONIC AIRLOADS PROGRAMS
1 //37X,30HFLIGHT CONDITIONS AND GEOMETRY/1H0//15X, 13HMACH NUMBERS
2 =,F8.5,4X,16HSPEED OF SOUND =F10.3,4H L/T,4X,4HRHO=,E14.8//1H0/
X54X,4HWING,18X,
3 4HTAIL//22X,16HL.F. STATION (L),2F22.3//22X,16HROOT CHORD (L),
4 2F22.3// 22X,16HL.F. SPAN (L),2F22.3//22X,16HT.E. SPAN (L),
5 2F22.3// 22X,16HTIP CHORD (L),2F22.3//22X,16HTOTAL AREA (L*L),
6 2F22.3// 22X,16HCHORDWISE BOXES ,I19,I22//22X,
/16HSPANWISE BOXES ,I19,I22)
WRITE(6,12)NBOX,DX,DY
12 FORMAT(1H0//,11X,23HTOTAL CHORDWISE BOXES =,13, 5X,11HBOX CHORD =,
1 1P1E12.5,2H L, 5X,10HBOX SPAN =,1P1E12.5,2H L/ )
WRITE(6,91)
NB = 1
DO 17 NP = 1,NB*X
MB = MOB(NP)
IF(MB.GT.50) GO TO 800
DO 13 MP = 1,MB
K = KBOX(NB)
C(MP) = COD(K)
13 NB = NB + 1
IF(NP.GT.6) GO TO 15

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```

WRITE(6,14)(SH(I,MP),I=1,5),(C(MP),MP=1,MB)
14 FORMAT(10X,5A6,50A1)
GO TO 17
15 WRITE(6,16) (C(MP),MP=1,MB)
16 FORMAT(40X,50A1)
17 CONTINUE
GO TO 1000
800 WRITE(6,801)
801 FORMAT(9X,52HWHEN MOB EXCEEDS 50 THE MAP PRINTING IS DISCONTINUED
1 /1H0,48H CALCULATIONS PROCEED IN NORMAL MANNER )
GO TO 1000
20 WRITE(6,51)FREQ(IFR),NBOX,EKR ,EM
WRITE(6,21)EM,EKB
21 FORMAT(1H ,28X,48HPLANAR VELOCITY POTENTIAL INFLUENCE COEFFICIENTS
1 /1H0,30X,10HACH NO. =,F8.5,10X, 6HKBAR =,F9.5/1H0,13X,1H1,5X,1HJS
2 10X,5HNUBAR,5X,5HMUBAR,11X,14HREAL VPIC(I,J),8X,14HIMAG VPIC(I,J)
3 /1H )
K = 0
DO 22 I = 1,NBOX
DO 22 J = 1,I
BARNU = I - 1
BARMU = J - 1
K=K+1
22 WRITE(6,23) I,J,BARNU,BARMU,VPIC(K)
23 FORMAT(9X,216,4X,2F10.1,2X,1P2E22.5)
GO TO 1000
30 WRITE(6,51) FREQ(IFR),NBOX,EKR ,EM
WRITE(6,31)MODE
31 FORMAT(1H ,21X, 59HUPPER VELOCITY POTENTIALS AND SOURCE STRENGTHS
1 FOR MODE NO.13/1H0,9X,1HN,6X,1HM,5X,2HNB,7X,10HR PHI(N,M),7X,10HI
2 PHI(N,M)10X,9HR SS(N,M),8X,9HI SS(N,M)/1H )
GO TO 1000
40 WRITE(6,41)MP,MB,AB,PHI,SS(NB)
41 FORMAT(4X,317,122E17.5,3X,1P2E17.5)
GO TO 1000
60 IF(NS.EQ.3) GO TO 100
50 WRITE(6,51)FREQ(IFR),NBOX,EKR ,EM
51 FORMAT(1H1,33X,44HMISSILE SUPERSONIC AIRLOADS PROGRAM (CONT=D)//
X1H0
1 8X,27HOSCILLATORY FREQUENCY (CPS),F12.5,14X,12,25H BOXES IN CHORD
2 DIRECTION /1H0,8X,30HREDUCED FREQUENCY (SEMI CHORD),F9.5,14X,
3 23HFREE STREAM MACH NUMBER,F9.3,/1H )
WRITE(6,101) SURF(1,NS)
101 FORMAT(28X,45HINPUT MODE SHAPE POLYNOMIAL COEFFICIENTS FOR ,A6/
1 22X,62HREFERENCED TO THE SURFACE LEADING EDGE-CENTERLINE INTERSECS
2 TION //2X,4HMODE,20X, 7HCoeffs.)
DO 102 I=1,NMODE
NTM=NI(I,NS)
102 WRITE(6,103) I,(CO(I,J,NS),J=1,NTM)
103 FORMAT(1H0,14,4X,1P7E13.4/(9X,1P7E13.4))
100 WRITE(6,51)FREQ(IFR),NBOX,EKR ,EM
WRITE(6,61)(SURF(I,NS),I=1,2)
61 FORMAT(1H ,35X,23HGENERALIZED FORCES FOR ,2A6/1H0,6X,4HDEF L,3X,
1 4HLOAD,10X,9HREAL PART,10X,9HIMAG PART,10X,9HABS VALUE,10X,
2 11HPHASE ANGLE //)
GO TO 1000
70 WRITE(6,71)J,K,QR,QI,QAB,QAN
IF (NSURF.EQ. 1) GO TO 632
IF (NS.NE.3) GO TO 1000
632 KKK=2*NMODE

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SUP75430
SUP75440
SUP75450
SUP75460
SUP75470
SUP75480
SUP75485
SUP75490
SUP75500
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SUP75700
SUP75710
SUP75720
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SUP75900
SUP75910
SUP75920
SUP75930
SUP75940
SUP75950
SUP75960
SUP75970
SUP75980

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NNN=2*K	*****
NNNN=NNN-1	*****
CARDS(J,NNNN)=QP	*****
CARDS(J,NNN)=QI	*****
IF (J.NE.NMODE) GO TO 1000	*****
IF (K.NE.NMODE) GO TO 1000	*****
PUNCH 6969, ((CARDS(II,JJ),JJ=1,KKK), II=1,NMODE)	*****
6969 FORMAT(6E12.5)	*****
71 FORMAT(1H0,19,17,2X,1P3E19.5,0PF16.3,4H DEB)	SUP75990
91 FORMAT(1H1,30X,44HMISSILE SUPERSONIC AIRLOADS PROGRAM (CONT-D)//)	SUP76000
1000 RETURN	SUP76010

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