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COLLOCATION FLUTTER ANALYSIS STUDY

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W. L. ... 6022

VOLUME IV.

COFA - COMPUTER PROGRAM TO PERFORM FLUTTER
ANALYSIS BY THE COLLOCATION METHOD

APRIL 1969



MISSILE SYSTEMS DIVISION



1969

1970

COFA

COLLOCATION FLUTTER ANALYSIS STUDY

VOLUME IV

COFA - COMPUTER PROGRAM TO
PERFORM FLUTTER ANALYSIS BY THE COLLOCATION METHOD

Prepared by Dynamics & Environments Section Personnel
Hughes Aircraft Company, Missile Systems Division
Contract No. 00019-68-L-0247

APRIL 1969

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ABSTRACT

A collocation solution of the flutter and vibration problems for a multiple component system is presented. The formulation utilizes structural, aerodynamic, and inertial characteristics in the form of matrices of structural and aerodynamic influence coefficients and a mass matrix, respectively, for each component. The use of a rigid-body modal matrix permits a general analysis for a system free in space with up to six rigid-body degrees of freedom.

The computer program provides the flutter or vibration solution for a system composed of as many as 20 flexible components with a maximum total of 49 collocation control points. An option is provided to vary the density as well as the reduced velocity. Another option is provided to yield the modes from a vibration analysis in a punched-card format for use in flutter analysis by modal methods.

SECTION 1

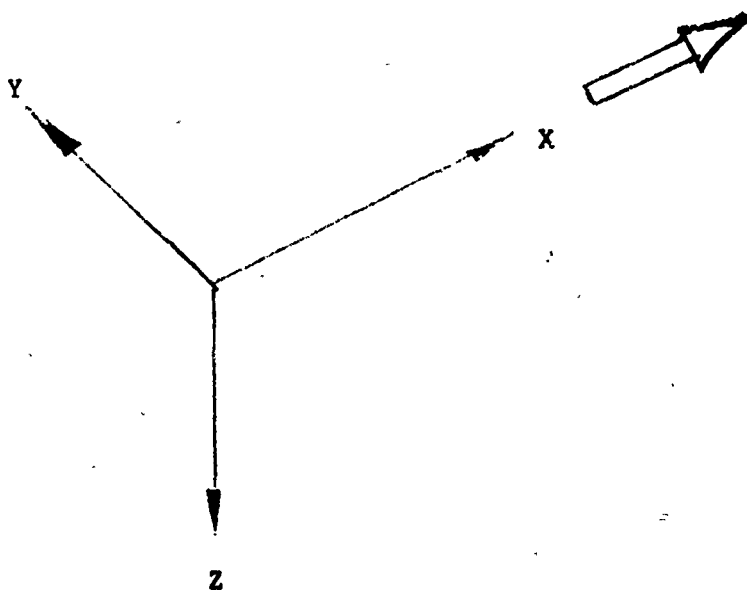
INTRODUCTION

The mathematical formulation of the flutter problem results in a set of integral equations whose closed form solution is impossible to obtain for most practical problems. One of the most useful approximate methods of solving these equations is by direct collocation. A solution by collocation is one in which the equations are satisfied at a finite number of selected points on the structure. These points, known as collocation points, are satisfied simultaneously. The collocation solution results in a matrix formulation which when cast in the canonical form will yield eigenvalues that are directly related to the flutter stability parameters. This manual presents a digital computer program that will perform collocation flutter analyses. The computer program, which is written in Fortran IV, was developed by Rodden, Farkas, and Malcom in Reference 1.

The collocation formulation of the flutter problem has been presented in Reference 2. The equations are presented for analysis of single component systems restrained (cantilevered) in space and for symmetrical systems free in space undergoing either symmetric or antisymmetric flutter. A method of generalizing the matrix equation for free-free flutter to include up to six rigid-body degrees of freedom has been given in Reference 3. The present program extends the formulation of Reference 2 to include an arbitrary combination of rigid-body degrees of freedom (Ref: 3), and to consider more than one flexible component. In addition, an option has been provided to vary the altitude (i. e. density) as well as the reduced velocity. Finally, options have been added to carry out a vibration analysis (which requires no aerodynamic data) and to provide vibration modes in punched-card format for use in a modal flutter or vibration analysis.

SECTION 2

The NASA body axis system with the x , y , and z axes directed forward, starboard, and downward, respectively, is recommended for consistency with the formulation of the static aeroelastic problems in Reference 4. However, the usual flutter convention with the x , y and z axes directed aft, starboard and downward, respectively, may be used instead. In either case, the vertical normal force and deflection are positive downward.



SECTION 3

DERIVATION OF EQUATIONS

The integral equations of aeroelasticity consist of two basic relationships: The first is the relation between the structural deformation, the structural influence function, and the inertial and aerodynamic loadings; the second is the relation between the aerodynamic disturbance (downwash), the aerodynamic influence (kernel) function, and the aerodynamic pressure. A collocation formulation of the deformation integral equation for a vehicle free in space may be written in matrix form by requiring that the integral equation be satisfied at a discrete set of control points. We choose a single type of coordinate, viz., the deflection h , as an adequate measure of both the deformation and the free-stream disturbance, not only for simplicity in the resulting equations but also because deflections have a more general meaning on a cambered vehicle and deflection influence coefficients are more readily obtained from a structural analysis than slope (or twist) influence coefficients. The resulting deformation matrix equation is

$$\{h_1\} - \{h_0\} = K[a] (\{F_i\} + \{F_a\}) \quad (1)$$

where $\{h_1\}$ is the set of components of the absolute deflections of the control points, $\{h_0\}$ is the set of components of the deflections of the control points due to the rigid-body motion of some reference points, $[a]$ is the set of structural influence coefficients (SICs, or flexibility matrix) for the system cantilevered from (or otherwise restrained at) the reference point, $\{F_i\}$ is the set of inertial force components integrated throughout the region adjacent to each control point, $\{F_a\}$ is the set of aerodynamic force components integrated over the vehicle surface adjacent to each control point, and the scalar K has been introduced as a factor to the SICs for convenience in investigating variations in stiffness levels. The inertial forces may be written in terms of a mass matrix $[M]$ and the control point accelerations.

$$\{F_i\} = -(1/386)[M]\{\ddot{h}_1\} \quad (2)$$

where the diagonal elements of the mass matrix are found from integrating the structural mass density throughout the region adjacent to the control points. (N. B., the mass matrix need not be diagonal, and, in general, will not be so if the elements must be derived from a set of weight data previously lumped at a system of control points different from those required in the aeroelastic analysis. The use of a coupled mass matrix permits simulation of given inertial characteristics at a set of control points frequently dictated by more difficult aerodynamic considerations.)

A collocation formulation of the aerodynamic integral equation is more difficult than in the case of the deformation integral equation because of the singularities in the aerodynamic kernel function. The determination of three relationships is necessary to derive a set of aerodynamic influence coefficients (AICs) that relate the control point forces to the deflections. The most basic and difficult is the pressure-downwash relation that is derived from numerical analysis of the aerodynamic integral equation. The simpler relations are the numerical integration of the pressure to obtain the force, and the numerical substantial differentiation of the deflection to obtain the downwash. The effort involved in each step depends on the planform, Mach number regime, and frequency range; a survey of the status of unsteady AICs is given in Ref. 4. For present purposes, it is sufficient to state the definition of the AICs in the oscillatory case. We write the aerodynamic control point forces in terms of the control point deflections as

$$\{F_a\} = (4\pi^2/12)\rho f^2 b_r^2 s [W][C_h]\{h_1\} \quad (3)$$

where $[C_h]$ is the theoretically derived dimensionless (complex) matrix of oscillatory AICs, f is the frequency of the assumed harmonic motion, ρ is the atmospheric density, b_r is the reference semichord, s is the reference span, and $[W]$ is an empirically derived weighting matrix

for modification of the theoretical AICs. A method for obtaining the elements of the weighting matrix has been suggested in Ref. 4.

The sum of the force components may be written now from Eqs. (2) and (3) for the case of harmonic motion.

$$\{F_i\} + \{F_a\} = (4\pi^2 f^2 / 386)([M] + 32.174 \rho b_r^2 s[W][C_h])\{u_1\} \quad (4a)$$

$$= (4\pi^2 f^2 / 386)[\bar{M}]\{h_1\} \quad (4b)$$

We next discuss the manner of inclusion of the rigid-body degrees of freedom in Eq. (1). The matrix $\{h_o\}$ has been defined as the set of components of the deflections of the control points due to the rigid-body motion of the reference point. Each component of the control point deflections h_o is linearly related to the rigid-body translations and rotations, provided the rotations are small. Therefore, we may define a rigid-body modal matrix $|h_R|$ as the transformation

$$\{h_o\} = [h_R] \{a_R\} \quad (5)$$

where $\{a_R\}$ is the set of amplitudes of rigid-body translations and rotations of the reference point. As an example, if we consider symmetrical vertical motion, $[h_R]$ is composed of two columns: the first is a unit column corresponding to the plunging mode, the second consists of the x-coordinate of each control point corresponding to the pitching mode; $|a_R|$ is composed of two elements: the first is the plunging displacement z_o , the second is the pitching angular displacement θ .

Before proceeding in the derivation, we should review the format of the various matrices in the case of a multiple flexible component system. As an example, we consider a symmetrical flutter analysis of an aircraft whose wing, aft fuselage, and tail are flexible, and whose forward fuselage may be assumed to be rigid. We assume that the reference point (cantilever point) can be located in the vehicle such that

its various components are independent. If we choose a point at the intersection of the wing and fuselage, then the wing is independent of the aft fuselage-tail combination, but the tail and aft fuselage must be considered together. The motion of the rigid forward fuselage is determined by the motion of the reference point, and the forward fuselage will not enter into any flexible considerations but only into the free-free boundary conditions. From the foregoing, it is seen that the various matrices will appear in partitioned form. If we denote the wing and aft fuselage-tail system by the subscripts 1 and 2, respectively, then the flexibility matrix appears as

$$[a] = \begin{bmatrix} a_1 & 0 \\ 0 & a_2 \end{bmatrix} \quad (6)$$

the mass matrix as

$$[M] = \begin{bmatrix} M_1 & 0 \\ 0 & M_2 \end{bmatrix} \quad (7)$$

the weighting matrix as

$$[W] = \begin{bmatrix} W_1 & 0 \\ 0 & W_2 \end{bmatrix} \quad (8)$$

the AICs as

$$[C_h] = \left[\begin{array}{c|c} C_{h1} & 0 \\ \hline 0 & C_{h2} \end{array} \right] \quad (9)$$

and the rigid-body modal matrix as

$$[h_R] = \left[\begin{array}{c} h_{R1} \\ \hline h_{R2} \end{array} \right] \quad (10)$$

Two requirements should be emphasized with regard to the AICs. The first concerns the proper inclusion of the reference geometry associated with the nondimensional AICs. The dimensional form of Eq. (9) may be written

$$b_r^2 s [C_h] = \left[\begin{array}{c|c} b_1^2 s_1 C_{h1} & 0 \\ \hline 0 & b_2^2 s_2 C_{h2} \end{array} \right] \quad (11)$$

where b_r and s are the reference semichord and span of the composite system, b_1 and s_1 are the reference geometry for the first component, and b_2 and s_2 are the reference geometry for the second component. The second requirement is that the AICs for each component must be determined for the same "dimensional" reduced velocity V/ω . If the reference reduced velocity is

$$1/k_r = V/b_r \omega \quad (12)$$

then the reduced velocity for the first component must be

$$1/k_1 = (1/k_r)(b_r/b_1) \quad (13)$$

and, for the second component,

$$1/k_2 = (1/k_r)(b_r/b_2) \quad (14)$$

Both of these requirements can be met in formulating the composite AICs by choosing the same reference geometry in determining the AICs for each component.

The rigid-body modal matrix provides the basis for a general statement of the boundary conditions for the free-free flutter of the composite system. The boundary conditions for harmonic motion may be written as

$$[h_R]^T [\bar{M}] \{h_1\} + [\Delta\bar{m}] \{a_R\} = \{0\} \quad (15)$$

where $[\Delta\bar{m}]$ is an incremental generalized mass matrix, including aerodynamic effects, of any rigid component of the system attached to the reference point (e. g., the forward fuselage that was assumed to be rigid in the foregoing example),* and is not considered in the formulation of the flexible component mass and aerodynamic matrices. The form of the matrix $[\Delta\bar{m}]$ may be illustrated by the previous example with the rigid forward fuselage again in symmetrical motion. We may write

$$[\Delta\bar{m}] = [\Delta m] + [\Delta Q] \quad (16)$$

* N. B.: It is assumed that no dynamic coupling exists between the rigid and flexible components. A suitable distinction can always be made between the rigid and flexible components such that this requirement can be met.

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where the generalized rigid component mass matrix of the forward fuselage is

$$[\Delta m] = \begin{bmatrix} M_o & S_o \\ S_o & I_{yo} \end{bmatrix} \quad (17)$$

in which M_o , S_o , and I_{yo} are the mass, static unbalance about the reference point, and pitching moment of inertia about the reference point, respectively, of the forward fuselage, and the generalized aerodynamic forces on the forward fuselage (if not negligible) are found from

$$[\Delta Q] = 32.174 \rho b_o^2 s_o [h_{Ro}]^T [C_{ho}] [h_{Ro}] \quad (18)$$

where $[h_{Ro}]$ is the rigid-body modal matrix, $[C_{ho}]$ is the set of AICs, and b_o and s_o are the reference geometry for the forward fuselage. Again the AICs must be found for the reduced velocity of the composite system.

We are now in a position to eliminate the rigid-body degrees of freedom and to formulate the eigenvalue problem for the flutter of the flexible free-free system. Substituting Eqs. (4b) and (5) into Eq. (1), and adding the structural damping factor $1/(1 + ig)$ to the flexibility matrix to provide the artificial structural damping necessary to sustain the assumed harmonic motion of the flutter system, we obtain

$$\{h_1\} - [h_R] \{a_R\} = (4\pi^2 K_f^2 / 386(1 + ig)) [a] [\overline{M}] \{h_1\} \quad (19)$$

$$\text{or} \quad \lambda(\{h_1\} - [h_R] \{a_R\}) = [a] [\overline{M}] \{h_1\} \quad (20a)$$

$$= [U] \{h_1\} \quad (20b)$$

where λ denotes the eigenvalue

$$\lambda = \lambda_R + i\lambda_I \quad (21a)$$

$$= 386(1 + ig)/4\pi^2 K f^2 \quad (21b)$$

Premultiplying Eq. (20b) by $[h_R]^T [\bar{M}]$, and multiplying Eq. (15) by λ and subtracting, permits solution for the amplitudes of the rigid-body motion

$$\lambda \{a_R\} = - [\bar{m}]^{-1} [h_R]^T [\bar{M}] [U] \{h_1\} \quad (22)$$

where

$$[\bar{m}] = [h_R]^T [\bar{M}] [h_R] + [\Delta \bar{m}] \quad (23)$$

Finally, substituting Eq. (22) into Eq. (20b) yields the generalized matrix equation for free-free flutter

$$\lambda \{h_1\} = ([I] - [h_R] [\bar{m}]^{-1} [h_R]^T [\bar{M}]) [U] \{h_1\} \quad (24)$$

The solution of Eq. (24) for the complex eigenvalues leads to the free-free frequency and the required structural damping. From Eq. (21), we obtain the frequency

$$f = (1/2\pi) \sqrt{386/K\lambda_R} \quad (25)$$

and the required structural damping

$$g = \lambda_I/\lambda_R \quad (26)$$

Since the formulation of the AICs requires the assumption of a reduced velocity $1/k_r$, the velocity follows from that and the frequency obtained in Eq. (25)

$$U = 0.5921 (2\pi f b_r)(1/k_r) \quad (27)$$

Equation (24) is seen to be completely general, being applicable from the cantilever case (in which we let $[h_R]$ vanish) to the case of six rigid body degrees of freedom, and for a vibration analysis for which the aerodynamic terms and required structural damping are deleted. We observe that Eq. (24) is a matrix formulation of the algebraic procedures for free-free vibration analysis described in Ref. 4 (Par. 11.2).

From a series of solutions of Eq. (24) for various reduced velocities, the conventional required damping versus velocity stability curve can be constructed for a specific altitude, and the flutter point is determined as the velocity for which the required damping and actual damping are equal. An alternative approach to the flutter analysis is based on a single representative reduced velocity and a series of solutions of Eq. (24), carried out for various densities. The density at which the required damping and actual damping are equal may be used to find a stiffness-altitude similarity parameter for flutter from which the flutter stability may be determined. However, at present, the validity of this latter approach requires further investigation, particularly the sensitivity of the results to the choice of representative reduced velocity.

The generalized mass corresponding to each free vibration mode is of interest in various modal analyses of flying qualities, stability and control characteristics, or transient response of flexible vehicles. If Eq. (24) is solved for the free vibration modes (by deleting the aerodynamic terms) then the n 'th generalized mass is given by

$$m^{(n)} = \{h_1^{(n)}\}^T [M] \{h_1^{(n)}\} + \{a_R^{(n)}\}^T [\Delta m] \{a_R^{(n)}\} \quad (28)$$

where $\{h_1^{(n)}\}$ is the n'th free vibration mode and the corresponding rigid component mode is found from Eq. (22)

$$\{a_R^{(n)}\} = \frac{4\pi^2 K}{386} f_n^2 [M]^{-1} [h_1]^\top [M] [U] \{h_1^{(n)}\} \quad (29)$$

SECTION 4
REFERENCES

1. W. P. Rodden, E. F. Farkas and H. A. Malcom. "Flutter and Vibration Analysis by a Collocation Method: Analytical Development and Computation Procedure". Aerospace Corporation Report No. TDR-169(3230-11)TN-14, 31 July 1963.
2. W. P. Rodden, "Matrix Approach to Flutter Analysis" Institute of the Aerospace Sciences Fairchild Fund Paper No. FF-23, May 1958; based on North American Aviation, Inc., Report NA-56-1070, 1 May 1956.
3. W. P. Rodden, "On Vibration and Flutter Analysis with Free-Free Boundary Conditions". Journal of the Aerospace Sciences, 28 (1961) 65.
4. W. P. Rodden and J. D. Revell. "The Status of Unsteady Aerodynamic Influence Coefficients". Institute of Aerospace Sciences Fairchild Fund Paper No. FF-33, 23 January 1962; preprinted in Aerospace Corporation Report TDR-930(2230-09) TN-2, 22 November 1961.
5. R. L. Bisplinghoff, H. Ashley, and R. L. Halfman. Aeroelasticity. Reading: Addison-Wesley Publishing Company, Inc., 1955.
6. R. H. Scanlan and Robert Rosenbaum. Introduction to the Study of Aircraft Vibration and Flutter. New York: The MacMillan Company, 1951.

SECTION 5

DESCRIPTION OF PROGRAM INPUT

UNITS

The dimensional data required for each component consist of the mass matrix in pounds, the flexibility matrix in inches per pound, and the reference semichord and semispan in feet. The aerodynamic influence coefficients are dimensionless. In the case of free-free analysis, the rigid-body mass matrix, e. g., in a symmetrical analysis if S_0 and I_{y_0} are given in the foot-pound system, the x-coordinates which correspond to the rigid body pitching mode must be measured in feet, whereas if S_0 and I_{y_0} are given in the inch-pound system, the x-coordinate must be measured in inches. The density is required in slugs per cubic foot.

CLASSES OF DATA AND PROBLEMS

Five classes of data must be provided: mass, aerodynamic influence coefficients (AICs) and their weighting matrices, structural influence coefficients, the rigid-body motion modal matrix, and the rigid component generalized mass characteristics. The cantilever case does not require either the rigid body modal matrix or the generalized masses. (For a vibration analysis, the aerodynamic input is not required.)

Several classifications of problems may be analyzed using the collocation flutter analysis program. They are cantilever flutter analysis — the structure is restrained from plunging motion. Free-free flutter analysis the structure is free to pitch, plunge, and roll. The free-free cases may have rigid components and flexible components. However, when flexible components are coupled together, the structural attachment between component must be statically determinate. When rigid body components are used, any number up to six rigid body modes may be used. Also vibration analyses may be performed when zero aerodynamic forces are used.

PROGRAM RESTRICTIONS AND OPTIONS

1. The maximum number of control points that can be used for all flexible components of any system is 49. A maximum of 49 control points may also be used for the rigid component for the purpose of deriving the generalized aerodynamic force.
2. The maximum number of flexible components is 20.
3. The maximum number of values used in the reference reduced velocity ($1/K_R$) series is 20.
4. The maximum number of values used in a density series is 20.
5. The program provides for varying the densities with each ($1/K_R$) or for using the same densities with all ($1/K_R$)'s.
6. The maximum number of output modes is 25.
7. The maximum number of rigid-body motion modes is 6.
8. It is possible to reserve a partition in the upper left-hand corner of the flexible components AIC matrices for control points whose aerodynamic forces may be neglected or found from an alternate theory to that used for the primary control points. This partition is termed the external stores region since external stores are an example of a source of additional control points requiring such special consideration. The maximum number of control points that can be reserved on each flexible component for external stores is 48.
9. A weighting matrix is an optional input for each flexible component. The order of this matrix must be identical with the order of the AIC matrices for the particular component.
10. Any number of complete sets (decks) of input data may be stacked and run in one machine pass.

DATA DECK SETUP

Loading Order

The data decks are assembled using cards punched from keypunch forms and/or card that are punched-card output from appropriate computer programs. The data items in each deck have the following order,

with the exception that some of the items may be omitted if indicators used in the control cards specify their absence.

1. Title card
2. Data deck general control card
3. K card (flexibility matrix scale factor)
4. Data card for change in matrix iteration tests
5. Control card(s) for external stores and weighting matrices
6. Reference semichord (b_r) and reference reduced velocities ($1/k_r$)'s
7. Reference semichord (b_{r_i}) and reference semispan (S_i) for rigid and flexible components (surfaces)
8. Density series (if same densities are used for all $1/k_r$)'s
9. Generalized mass matrix ($[\Delta m]$) for rigid components
10. Mass matrix ($[M]_i$) for each flexible surface
11. Rigid-body motion modal matrix ($[h_{R_0}]$) for rigid component
12. Rigid-body motion modal matrix ($[h_{R_i}]$) for each flexible surface
13. Flexibility matrix ($[a]_i$)
14. Weighting matrices ($[W]_i$)
15. Aerodynamic input repeated for each $1/k_r$
 - a. Density series cards (if densities vary with each $1/k_r$)
 - b. AIC matrix ($[C_{h_0}]$) for rigid component (if present)
 - c. AIC matrix ($[C_{h_i}]$) for each flexible surface

Input Data Description

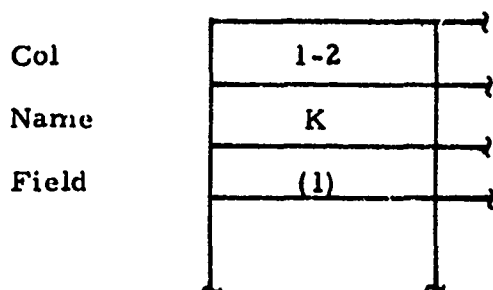
1. The title card may contain any alphanumeric characters desired in Columns 2 through 72.

2. Data deck general control card (FORMAT 18I4):

Col	1-4	5-8	9-12	13-16	17-20	21-24	25-28	29-32	33-36
Name	NSUR	NAERO	NRIGID	NFUS	NDENS	MODES	NDELM	NPUNCH	NCOM
Field	(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)

- NSUR:** Number of flexible components (surfaces), ≤ 20 .
NAERO: Number of reference reduced velocities, ≤ 20 ; NAERO = 0 is used for vibration analyses.
NRIGID: Number of rigid-body motion modes to be input (= number of columns in $([h_R])$); NRIGID = 0 for the cantilever case.
NFUS: NFUS must = 1 if AICs $([C_{ho}]_j)$, $j = 1, NAERO$ are input for the rigid components; NFUS = 0 if $[C_{ho}]$ is not input.
NDENS: If NDENS = 0 the densities are to vary with each $1/k_r$ and are input as part of Item 15; if NDENS > 0 this number of densities must be input as Item 8, and each density value will be used for all $(1/k_r)$'s.
MODES: Number of output modes, ≤ 25 .
NDELM: NDELM = 0 if no rigid component generalized mass matrix $([\Delta m])$ is input; NDELM = 1 if $[\Delta m]$ is input.
NPUNCH: This indicator is used to obtain a printout of the dynamic matrix $([U])$ and to obtain the frequencies and modes in punched-card format; NPUNCH = 0 if no printout of $[U]$ or punched output is desired; NPUNCH = 1 if only punched-card output is desired and NPUNCH = -1 will provide the printout of $[U]$ and the punched output. (The minus sign must be in Column 29 and the 1 (one) in Column 32.)
NCON: This indicator provides for changing five program test numbers used in the matrix iteration subroutine; NCON = 0 if no changes are desired and NCON \neq 0 if any of the tests is to be changed.

3. K card (FORMAT 6E12.8)



Field 1 contains K, the flexibility matrix normalizing constant; if the [a] matrix has not been normalized, enter K = 1.0. The flexibility matrix calculated by the program FLUENC has not been normalized.

4. Data card for changes in matrix iteration tests (FORMAT 3E12.8 and 2I4). Omit this card when NCON = 0. There are three test numbers and two control numbers that define the convergence criteria for the flutter eigenvalue solution. A suggested set of numbers are built into the program; these, however, may be changed by the program user. To alter any number, all five numbers must be reentered.

Col	1-12	13-24	25-36	37-40	41-44	
Name	EPSP	EPDP	AITKEN	NITRSP	NITRDP	
Field	(1)	(2)	(3)	(4)	(5)	

EPSP = 0.5×10^{-6} or input number; test for eigenvector convergence when the iteration procedure is approaching a single root.

EPDP = 0.5×10^{-7} or input number; test for convergence when the iteration procedure is approaching a pair of close roots.

AITKEN = 0.9 or input number; if this test is met, the program uses a procedure (known as Aitken's δ^2 method) to accelerate convergence.

NITRSP = 40; a maximum of 40 single precision arithmetic iterations will be performed for each eigenvalue if its eigenvectors have not converged in a lesser number.

NITRDP = 100; if the eigenvectors for any one eigenvalue have not converged in NITRSP single precision iterations, the program will then use up to a maximum of 100 double arithmetic iterations.

5. Control card(s) for external stores and weighting matrices (FORMAT 18I4); omit this data when NAERO = 0.

Col	1-4	5-8	9-12	13-16	
Name	ISXT ₁	ISW ₁	ISXT ₂	ISW ₂	
Field	1	2	3	4	

Continue on successive cards to ISW_i = ISW_{NSUR}.

ISXT_i = Number of control points reserved for the external stores on surface i.

ISW_i = 0, no weighting matrix is to be input for surface i.
 = 1, weighting matrix is to be input for surface i.

Continue on next card, until i = NSUR.

6. Reference semichord, b_r and reduced velocity ($1/k_r$) series (FORMAT 6E12.8): These reference parameters are used in computing the flutter velocities.

Col	1-12	13-24	25-36	37-48	49-60	61-72
Name	b_r	$(1/k_r)_1$	$(1/k_r)_2$	$(1/k_r)_3$	$(1/k_r)_4$	$(1/k_r)_5$
Field	(1)	(2)	(3)	(4)	(5)	(6)

Continue $(1/k_r)_i$'s on next card(s); $i \leq 20$. The b_r (feet) may be any value; but it is noted that the $(1/k_r)_i$ predetermines the $(1/k_i)$ used when computing the AIC matrices for each surface. The $1/k_i$ for surface i is found from the relationship $(1/k_i) = (1/k_r)(b_r/b_{ri})$ where b_{ri} is the reference semichord for surface i.

7. A reference semichord (b_{r_i}) and semispan (s_i) must be input for the rigid component if NFUS = 1, and for each flexible surface if NAERO > 0.

When NFUS = 1 (FORMAT 6E12.8)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	b_{r0}	s_{r0}	b_{r1}	s_{r1}	b_{r2}	s_{r2}
Field	(1)	(2)	(3)	(4)	(5)	(6)

Where b_{r0} and s_{r0} are the reference semichord and semispan for the rigid component. Continue on next card(s) until $b_{ri} = b_{rNSUR}$ and $s_{ri} = s_{rNSUR}$.

When NFUS = 0 (FORMAT 6E12.8)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	b_{r1}	s_{r1}	b_{r2}	s_{r2}	b_{r3}	s_{r3}
Field	(1)	(2)	(3)	(4)	(5)	(6)

Continue on next card(s) until $b_{ri} = b_{rNSUR}$ and $s_{ri} = s_{rNSUR}$.

8. Density series (FORMAT 6E12. 5): Omit this input if NDENS=0 in Item 2. If NDENS>0 begin in field 1 of this card and NDENS densities, ≤ 20 . Continue on successive card(s).

Column	1-12	13-24	25-36	37-48
Name	ρ_1	ρ_2	ρ_3	ρ_4
Field	1	2	3	4

9. Rigid component generalized mass matrix $[\Delta m]$. The $[\Delta m]$ matrix for the rigid component(s) of the system must be compatible with the flexible surfaces product matrix given by $[h_R]^T [M] [h_R]$, i. e., each element in $[\Delta m]$ is based upon the same rigid-body motion generalized coordinate as the respective element in the product matrix. Input by column beginning each column on a new card. Omit this data when NDELM = 0.

Col	1-12	13-24	25-36		
Name	$\Delta m_{1,1}$	$\Delta m_{2,1}$	$\Delta m_{3,1}$	$\Delta m_{(NRIGID-1),1}$	$\Delta m_{NRIGID,1}$
Field	(1)	(2)	(3)	(NRIGID-1)	(NRIGID)

Continue on successive card(s) until

10. Mass matrix [M]: The mass matrix is partitioned as shown on page A-10, only the nonzero partitions are input; i. e., a separate mass matrix ($[M_i]$) is input for each surface. The sequence for considering the surfaces is the same as that used in Item 5 and 7 if NAERO>0. Repeat the following input for each surface from $i = 1$ to NSUR.

Size Control Cards

Column	1-4	5-8	9-12	
Name	$NSIZE_i$			
Field	(1)	(2)	(3)	

$NSIZE_i =$ the order of $[M]_i$

Often many of the elements in a mass matrix are zero; the following format has been provided so that most of the zero elements will not need to be entered into the program as data.

Control Card(s) for Omitting Zeros (FORMAT 18I4)

Column	1-4	5-8	9-12	13-16	17-20	
Name	LOW_1	$LHIGH_1$	LOW_2	$LHIGH_2$	LOW_3	$LHIGH_i$
Field	(1)	(2)	(3)	(4)	(5)	(2 _i)

LOW_i = The row number in which the first nonzero element appears in Column i .

$LHIGH_i$ = The row number in which the last nonzero element appears in Column i .

If only one nonzero element appears in Column i (i. e., a diagonal mass matrix) the row number in which it appears must be used for both LOW and $LHIGH$.

Mass Matrix Elements (FORMAT 6E12.8)

Col	1-12	13-24	25-36			
Name	$\Delta m_{1, LOW}$	$\Delta m_{1, LOW+1}$	$\Delta m_{1, LOW+2}$		$\Delta m_{1, LHIGH-1}$	$\Delta m_{1, LHIGH}$
Field	(1)	(2)	(3)			

The elements are entered by column; each column begins on a new card. Any zero elements in rows between LOW and $LHIGH$ must be entered or their respective fields left blank. If external stores are present ($ISXT > 0$) all store control points must be entered before the surface control points; i. e., the elements representing the external stores mass must occupy the upper left-hand corner of the mass matrix.

11. Rigid component inodal matrix, $[h_{R_0}]$ (see page. 7). Omit this input when $NFUS = 0$. The number of rows in $[h_{R_0}]$ must be the same as the number of control points considered when computing the $[C_{h_c}]$ matrices; the number of columns must agree with $NRIGID$.

Size Control Card(s) (FORMAT 18I4)

Column	1-4	5-8	
Name	NROWS		
Field	(1)	(2)	

NROWS = The number of rows in $[h_{R_0}]$

Matrix $[h_{R_o}]$ Elements (FORMAT 6E12.8)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	$h_{R_{c1,1}}$	$h_{R_{o2,1}}$	$h_{R_{o3,1}}$	$h_{R_{oNROWS,1}}$
Field	(1)	(2)	(3)	(4)	(5)	(6)

The elements are entered by column, with each column beginning on a new card.

12. Rigid-body modal matrix, $[h_R]$ (see page 7). Omit this input if NRIGID = 0. $[h_R]$ is to be input by partitions $[h_{R_i}]$, each partition is of order (NSIZE x NRIGID) for each surface. The following data is to be repeated for $i = 1, NSUR$.

Size Control Card (FORMAT 18I4)

Column	1-4	5-8	
Name	NSIZE		
Field	(1)	(2)	

NSIZE = Number of control points on each surface

Matrix $[h_{R_i}]$ Elements (FORMAT 6E12.8)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	$h_{R_{1,1}}$	$h_{R_{2,1}}$	$h_{R_{3,1}}$	$h_{R_{NSIZE,1}}$
Field	(1)	(2)	(3)	(4)	(5)	(6)

The elements are entered by column, with each column beginning on a new card.

13. Flexibility matrices, $[a]$ (see page 6). The flexibility matrix is partitioned, only the nonzero partitions $[a_i]$ corresponding to the

flexible surfaces are entered. The matrix may be formed by any of the well-known procedures using elementary beam theory, force or displacement methods. The program FLUENC will generate this matrix using the displacement method. The punched output from FLUENC may be used as direct input into this program. The following data is repeated for $i = 1, NSUR$.

Control Card (FORMAT 18I4):

Column	1-4	5-8	9-12	13-16	
Name	m_i	(BLANK)	IFORM	IROW	
Field	(1)	(2)	(3)	(4)	

m_i = The number of rows in $[a]_i$

IFORM = 0 if the elements are to be input using column binary format.

= 1 if the elements are to be input using FORTRAN (FORMAT 6E12.8) or FLUENC output is to be used directly.

IROW = 0 if the matrix elements are to be entered by column.

= 1 if the matrix elements are to be entered by row.

Matrix $[a]_i$ elements (use format specified above):

For IFORM = 1 and IROW = 1 (FORMAT 6E12.8)

Column	1-12	13-24	25-36	37-48	
Name	$a_{1,1}$	$a_{1,2}$	$a_{1,3}$	$a_{1,4}$	
Field	(1)	(2)	(3)	(4)	

Each row starts on a new card.

For IFORM = 1 and IROW = 0 (FORMAT 6E12.8)

Column	1-12	13-24	25-36	37-48	
Name	$a_{1,1}$	$a_{2,1}$	$a_{3,1}$	$a_{4,1}$	
Field	(1)	(2)	(3)	(4)	

Each column starts on a new card.

If IFORM = 0, then IROW must = 0: The matrix elements are input using column binary format; Column 1 starts in Origin 1. Column 2 starts in location $(1 + m_1)$; Column 3 starts in location $(1 + 2m_1)$; etc. A TRA* card must end each $[a_i]$ deck. (The column binary format should be used only if the data are available as punched-card output from appropriate computer programs.) The only advantage of the C-B format is the minimum card storage space required.

14. Weighting matrix, $[W]$ (see page 6). The weighting matrix is partitioned, only the nonzero partitions $[W]_i$ corresponding to the flexible surface are entered. No provisions have been made for entering a $[W_o]_i$ matrix for the rigid component; any adjustment to $[C_{h_o}]$ must be made before it is input as data. If $ISW_i = 0$ omit this data. Repeat the following data for $i = 1, NSUR$.

For $(ISW)_i = 0$ and $(ISXT)_i > 0$

Control card for external stores elements (FORMAT 1814)

Column	1-4	5-8	9-12	13-16	
Name	$NXST_i$	(BLANK)	NFORM	NROW	
Field	(1)	(2)	(3)	(4)	

*The TRA card has a 7 and 9 punch in Column 1, Column 2 through 72 are blank and Column 73 through 80 will contain the characters used for identification and sequencing in the punched card output deck.

$NXST_i = 0$ if no $[W]_i$ matrix is input for the external stores area (the program will use a unit matrix, I)
 $= n$ the number of control points reserved for stores.
 $NFORM = 1$ if the $[W]_i$ matrix elements will be input using FORTRAN (FORMAT 6E12.8)
 $= 0$ if the elements are to be input using column binary format
 $NROW = 0$ if the $[W]_i$ matrix elements are to be input by column
 $= 1$ if the matrix elements are to be input by row

External stores elements $[W]_i$. Format given on control card above.

For $NFORM = 1$ $NROW = 1$

Column	1-12	13-24	25-36	37-48	
Name	$W_{1,1}$	$W_{1,2}$	$W_{1,3}$	$W_{1,4}$	
Field	(1)	(2)	(3)	(4)	

Each row starts on a new card.

For $NFORM = 1$ $NROW = 0$

Column	1-12	13-24	25-36	37-48	
Name	$W_{1,1}$	$W_{2,1}$	$W_{3,1}$	$W_{4,1}$	
Field	(1)	(2)	(3)	(4)	

Each column starts on a new card.

If NFORM = 0, then must NROW = 0: The matrix elements are input using column binary format; Column 1 starts in Origin 1. Column 2 starts in location $(1 + IXST_1)$; Column 3 starts in location $(1 + 2IXST_1)$; etc. A TRA card must end each $[a_i]$ deck. The column binary format should be used only if the data are available as punched-card output from appropriate computer programs. The only advantage of C-B format is the minimum card storage space required.

Control card for flexible surface weighting matrix $[W]_i$

(FORMAT 18I4) The $[W]_i$ matrix is often sparse, sometimes diagonal and may be of large order, ≤ 49 ; for this reason we provide for partitioning of the matrix and entering only the nonzero partitions.

Column	1-4	5-8	9-12	13-16	
Name	NSIZE _i	NPART	NFORM	NROW	
Field	(1)	(2)	(3)	(4)	

NSIZE = The number of control points used on surface i .

Do not include control points for external stores.

NPART = The number of partitions in the $[W]_{ij}$ surface matrix

NFORM = 1 if the $[W]_i$ will be input using FORTRAN (FORMAT 6E12.8)

= 0 if the elements are to be input using column binary format

NROW = 0 if the $[W]_i$ matrix elements are to be input by column

= 1 if the matrix elements are to be input by row

Repeat the following two data item for each partition $j = 1, \text{NPART}$.

Control card for partition $[W_i]_j$ FORMAT (18I4)

Column	1-4	5-8	9-12	13-16	17-21	
Name	N_j					
Field	(1)	(2)	(3)	(4)	(5)	

N_j = The order of partition j of $[W_i]$

Elements in partition $[W_i]_j$. Format given on the control card for flexible surface weighting matrix.

NFORM = 1 NROW = 1

Column	1-12	13-24	25-36	37-48	
Name	$W_{1,1}$	$W_{1,2}$	$W_{1,3}$	$W_{1,4}$	
Field	(1)	(2)	(3)	(4)	

Each row starts on a new card.

NFORM = 1 NROW = 0

Column	1-12	13-24	25-36	37-48	
Name	$W_{1,2}$	$W_{2,1}$	$W_{3,1}$	$W_{4,1}$	
Field	(1)	(2)	(3)	(4)	

Each column starts on a new card.

If $NFORM = 0$, then must $NROW = 0$: The matrix elements are input using column binary format; Column 1 starts in Origin 1. Column 2 starts in location $(1 + IXST_i)$; Column 3 starts in location $(1 + 2IXST_i)$ etc. A TRA card must end each $[a_i]$ deck. The column binary format should be used only if the data are available as punched-card output from appropriate computer programs. The only advantage of C-B format is the minimum card storage space required.

For $(ISW)_i = 0$ and $(ISXT)_i = 0$

Control card for flexible surface weighting matrix $[W_i]$ (FORMAT 1814). The $[W_i]$ matrix is often sparse, sometimes diagonal and may be of large order, ≈ 49 ; for this reason we provide for partitioning of the matrix and entering only the nonzero partitions. Repeat the following data for $i = 1, NSUR$.

Column	1-4	5-8	9-12	13-16	17-20	
Name	NSIZE _i	NPART	NFORM	NROW		
Field	(1)	(2)	(3)	(4)	(5)	

NSIZE = The number of control points used on surface i

NPART = The number of partitions in the $[W_i]_j$ surface matrix

NFORM = 1 if the $[W_i]$ will be input using FORTRAN (FORMAT 6E12.8)

= 0 if the elements are to be input using column binary format

NROW = 0 if the elements are to be input by column

= 1 if the elements are to be input by row

Repeat the following two data items for each partition $j = 1, NPART$.

Control card for partition $[W_i]_j$ FORMAT (18I4)

Column	1-4	5-8	9-12	13-16	
Name	N_j				
Field	(1)	(2)	(3)	(4)	

N_j = The order of partition j of $[W_i]$

Elements in partition $[W_i]_j$ format given on the control card for flexible surface weighting matrix.

NFORM = 1 NROW = 1

Column	1-12	13-24	25-36	37-48	
Name	$W_{1,1}$	$W_{1,2}$	$W_{1,3}$	$W_{1,4}$	
Field	(1)	(2)	(3)	(4)	

Each row starts on a new card.

NFORM = 1 NROW = 0

Column	1-12	13-24	25-36	37-48	
Name	$W_{1,1}$	$W_{2,1}$	$W_{3,1}$	$W_{4,1}$	
Field	(1)	(2)	(3)	(4)	

Each column starts on a new card.

If NFORM = 0, then must NROW = 0: The matrix elements are input using column binary format; Column 1 starts in Origin 1. Column 2 starts in location $(1 + m_1)$; Column 3 starts in location $(1 + 2m_1)$; etc. A TRA card must end each $[a_i]$ deck. The column binary format should

used only if the data are available as punched-card output from appropriate computer programs. The only advantage of C-B format is the minimum card storage space required.

15. Aerodynamic data: The aerodynamic input consists of NAERO sets of AIC's. Each set of AIC's consists of the AIC's for each surface which have the same reference $1/k_r$ (see Item 6). If NDENS = 0 a density series will precede each set of AIC's. Input the density series (if Item 8 was omitted) and the AIC matrices for each surface with the following input order. Repeat the order for each $(1/k_r)_j$ $j = 1, NAERO$.

Control card for density series (FORMAT 18I4). Omit this input if NDENS > 0.

Column	1-4	5-8	9-12	13-16	
Name	NRHO				
Field	(1)	(2)	(3)	(4)	

NRHO = The number of densities to be entered for $(1/k_r)_j \leq 20$

Density Series (FORMAT 6E12.8)

Column	1-12	13-24	25-36	37-48	
Name	ρ_1	ρ_2	ρ_3	ρ_4	
Field	(1)	(2)	(3)	(4)	

Rigid component AIC matrix $[C_{h_o}]_j$. Omit this input if NFUS = 0. The $[C_{h_o}]_j$ matrix may be sparse; thus, provision has been made to partition the matrix and enter only the nonzero partitions.

Reference $1/k$ for $[C_{h_0}]_j$ (FORMAT 6E12.8)

Column	1-12	13-24	25-36	37-48	
Name	$1/k$				
Field	(1)	(2)	(3)	(4)	

$1/k$ = The reduced velocity used in computing the rigid component $[C_{h_0}]_j$. The AIC's in $[C_{h_0}]_j$ must be computed for a $1/k$ which properly relates them to the j^{th} $1/k_r$.

Control card for $[C_{h_0}]_j$ matrix (FORMAT 18I4)

Column	1-4	5-8	9-12	13-16	
Name	NSIZE	NPART	NFORM	NROW	
Field	(1)	(2)	(3)	(4)	

NSIZE = Number of control points on the rigid component
 NPART = Number of nonzero partitions in $[C_{h_0}]_j$
 = 1 for an unpartitioned matrix
 NFORM = 1 if the $[C_{h_0}]_j$ matrix is to be input using FORTRAN (FORMAT 6E12.8)
 = 0 if the $[C_{h_0}]_j$ matrix is to be input using column binary format
 NROW = 1 if the $[C_{h_0}]_j$ matrix is to be input by row
 = 0 if the $[C_{h_0}]_j$ matrix is to be input by column

Repeat the following data for each partition, $K = 1, \text{NPART}$.

Partition Size Card (FORMAT 18I4)

Column	1-4	5-8	9-12	13-16	
Name	N				
Field	(1)	(2)	(3)	(4)	

N = The order of partition k

Elements in partition K of $[C_{h_0}]_j$. Format is given on the control card for $[C_{h_0}]_j$ matrix. All the elements in the AIC matrices are complex numbers, but the complexity is considered in the program. Thus, each partition may be input as though it is a real matrix of size $N \times 2N$. The real elements form the odd number columns, and the imaginary elements in the even numbered columns.

For NFORM = 1 NROW = 1

Column	1-12	13-24	25-36	37-48	
Name	$a(\text{Re})_{1,1}$	$a(\text{I})_{1,1}$	$a(\text{Re})_{1,2}$	$a(\text{I})_{1,2}$	
Field	(1)	(2)	(3)	(4)	

Each row starts on a new card.

For NFORM = 1 and NROW = 0

Column	1-12	13-24	25-36	37-48	49-60	
Name	$a(\text{Re})_{1,1}$	$a(\text{I})_{1,1}$	$a(\text{Re})_{2,1}$	$a(\text{I})_{2,1}$		
Field	(1)	(2)	(3)	(4)	(5)	

Each column starts on a new card.

For NFORM = 0, NROW must = 0. Use column binary format. Column 1 starts in card Origin 1, Column 2 in location (1 + 2N), Column 3 in location (1 + 4N), etc. A TRA card must end each deck. The column binary format should be used only if the data are available as punched-card output from appropriate computer programs. The only advantage of C-B format is the minimum card storage space required.

Flexible component AIC matrix $[C_h]_i$. The AIC matrices are often sparse; thus, a provision is made partitioning the matrix and entering only the nonzero partitions. The following data is repeated for $i = 1, NSUR$.

For $ISXT_i > 0$.

Control card for external stores partition of the surface i
AIC matrix $[C_h]_{ij}$ (FORMAT 18I4)

Column	1-4	5-8	9-12	13-16	
Name	NXST	(BLANK)	NFORM	NROW	
Field	(1)	(2)	(3)	(4)	

$NXST_i$ = Number of control points reserved for external stores

$NFORM = 1$ if the matrix elements are to be input using

FORTRAN (FORMAT 6E12.8)

= 0 if the matrix elements are to be entered using
column binary format

$NROW = 1$ if the matrix elements are to be entered by row

= 0 if the matrix elements are to be entered by column

Elements for external stores partition of AIC matrix $[C_h]_{ij}$

For $NFORM = 1$ and $NROW = 1$

Column	1-12	13-24	25-36	37-48	
Name	$a(\text{Re})_{1,1}$	$a(\text{I})_{1,1}$	$a(\text{Re})_{1,2}$	$a(\text{I})_{1,2}$	
Field	(1)	(2)	(3)	(4)	

Each row begins on a new card.

For NFORM = 1 and NROW = 0

Column	1-12	13-24	25-36	37-48	
Name	a(Re)i, 1	a(I)1, 1	a(Re)2, 1	a(Re)2, 1	
Field	(1)	(2)	(3)	(4)	

If NFORM = 0 then NROW must = 0 use column binary format. Column 1 starts in card origin 1, Column 2 in Location $(1+2NXT_i)$, Column 3 in Location $(1+4NXST_i)$, etc. A TRA Card must end each deck. The column binary format should be used only if the data are available as punched-card output from appropriate computer programs. The only advantage of C-B format is the minimum card storage space requirements.

Reference $1/k_i$ card for control point AIC matrix $[C_h]_{ij}$

FORMAT (6E12.8)

Column	1-12	13-24	25-36	
Name	1/k			
Field	(1)	(2)	(3)	

$1/k_i$ = The reduced velocity used in computing the flexible component $[C_h]_{ij}$. The AIC's must be computed for a $1/k_i$ which properly relates them to the j th $1/k_r$.

Control card for control point AIC matrix $[C_h]_{ij}$ (FORMAT (1814))

Column	1-4	5-8	9-12	13-16	
Name	NSIZE	NPART	NFORM	NROW	
Field	(1)	(2)	(3)	(4)	

- NSIZE = Order of control point AIC matrix $[C_h]_{ij}$
 NPART = Number of partitions in $[C_h]_{ij}$
 NFORM = 1 matrix elements are to be input using FORTRAN
 (FORMAT 6E12.3)
 = 0 matrix elements are to be input using column binary
 format
 NROW = 1 elements input by row.
 = 0 elements input by column.

Repeat the following data for $j = 2, NPART$. $j = 1$ corresponds to the external stores partition

Control card for partition size of partition j FORMAT (18J4)

Column	1-4	5-8	9-12	
Name	N			
Field	(1)	(2)	(3)	

N = Order of partition j

Elements of control point AIC matrix $[C_H]_{i,j}$ partition j

For NFORM = 1 and NROW = 1 (FORMAT 6E12.8)

Column	1-12	13-24	25-36	37-48	
Name	a(Re)1,1	a(I)1,1	a(Re)1,2	a(I)1,2	
Field	(1)	(2)	(3)	(4)	

Each row starts on a new card

For NFORM = 1 and NROW = 0 (FORMAT 6E12.8)

Column	1-12	13-24	25-36	37-48	
Name	a(Re)1,1	a(I)1,1	a(Re)2,1	a(I)2,1	
Field	(1)	(2)	(3)	(4)	

Each column starts on a new card

For NFORM = 0 then NROW must = 0 use column binary format. Column 1 starts in card origin 1, Column 2 in Location (1 + 2N), Column 3 in Location (1 + 4N), etc. A TRA card must end each deck. The column binary format should be used only if the data are available as punched card output from appropriate computer programs. The only advantage of C-B format is the minimum card storage space requirements

For ISXT_i = 0

Reference 1/k_i card for control point AIC matrix $[C_h]_{ij}$

FORMAT (6E12.8)

Column	1-12	13-24	25-36	
Name	1/k _i			
Field	(1)	(2)	(3)	

1/k_i = The reduced velocity used in computing the flexible component $[C_h]_{ij}$. The AIC's must be computed for a 1/k_i which properly relates them to the jth 1/k_r.

Control card for control point AIC matrix $[C_h]_{ij}$ FORMAT (18I4)

Column	1-4	5-8	9-12	13-16	
Name	NSIZE	NPART	NFORM	NROW	
Field	(1)	(2)	(3)	(4)	

NSIZE = Order of control point AIC matrix $[C_h]_{ij}$
 NPART = Number of partitions in $[C_h]_{ij}$
 NFORM = 1 matrix elements are to be input using FORTRAN (FORMAT 6E12.8)
 = 0 matrix elements are to be input using column binary format.
 NROW = 1 elements input by row
 = 0 elements input by column

Repeat the following data for $j = 1, \text{NPART}$.

Control card for partition size of partition j FORMAT (18I4)

Column	1-4	5-8	9-12	
Name	N			
Field	(1)	(2)	(3)	

$N =$ Order of partition

Elements of control point AIC matrix $[C_h]_{i,j}$ partition j

For $\text{NFORM} = 1$ and $\text{NROW} = 1$ (FORMAT 6E12.8)

Column	1-12	13-24	25-36	37-48	
Name	a(Re)1,1	a(I)1,1	a(Re)1,2	a(I)1,2	
Field	(1)	(2)	(3)	(4)	

Each row starts on a new card

For $\text{NFORM} = 1$ and $\text{NROW} = 0$ (FORMAT 6E12.8)

Column	1-12	13-24	25-36	37-48	
Name	a(Re)1,1	a(I)1,1	a(Re)2,1	a(I)2,1	
Field	(1)	(2)	(3)	(4)	

For $\text{NFORM} = 0$ then NROW must = 0 use column binary format. Column 1 start in card origin 1, Column 2 in Location $(1 + 2N)$, Column 3 in Location $(1 + 4N)$, etc. A TRA card must end each deck. The column binary format should be used only if the data are available as punched card output from appropriate computer programs. The only advantage of C-B format is the minimum card storage requirements.

SECTION 6

DESCRIPTION OF PROGRAM OUTPUT

A. Printed Output

1. All input data.
2. The dynamic matrix or flutter determinant if NPUNCH = -1 is used in the general control card.
3. For the vibration analysis or for each $1/k_r$ in a flutter analysis
 - a. The eigenvalue for each output mode followed by the number of single- and double-precision iterations and the number of Aitken accelerations.
 - b. The normalized eigenvectors (modes) followed by the check eigenvalues and eigenvectors.
 - c. The frequencies (omegas) in cycles per second followed (in a flutter analysis) by the structural damping coefficient and the velocity (knots) associated with each frequency.
 - d. If NPUNCH = ± 1 , the sequencing numbers used for identifying the punched-card output (frequencies and modes); this will conclude the printout for each $1/k_r$ used in a flutter analysis.
4. In a vibration analysis, the generalized mass corresponding to each output (free vibration) mode will follow the above printed output [see Eq. (28), Section I].
5. A number of different statements may be printed which indicate machine or program detected errors in input data (wrong format or incompatibility in the number of rows input for a matrix and the number designated).
6. If the program or the machine fails in the iteration portion of the program, a note will be printed stating the type or cause of failure.

7. If convergence is not obtained in the allowable number of iterations, a note will be printed and the program will continue. (In this case the eigenvalues and eigenvectors should be compared with the check eigenvalues and eigenvectors to determine if the convergence is sufficiently accurate.)
8. The printed output for the example problem is shown on the following pages.

SECTION 7

EXAMPLE PROBLEMS

As example problems, we choose a cantilever flutter analysis and a free-free symmetric flutter analysis of the jet transport wing (and rigid fuselage) treated throughout Ref. 5 and shown in Figure A-1. The wing mass, flexibility and aerodynamic matrices and the fuselage aerodynamic matrix (symmetric case) can be seen in the example problem printed output (pages 41-62) and will not be repeated with the list of input data to follow. The flexibility matrix normalizing factor is $K = 10^{-7}$. The wing weighting matrix is taken as unity ($[I]$) and, in this case, requires no input. The symmetrical rigid component (one-half of the fuselage) generalized mass matrix is given below in the pound-inch system

$$[\Delta m] = \begin{bmatrix} M_o & S_o \\ S_o & I_{y_o} \end{bmatrix} = \begin{bmatrix} 17,400 & 1,370,250 \\ 1,370,250 & 4,457,907,200 \end{bmatrix}$$

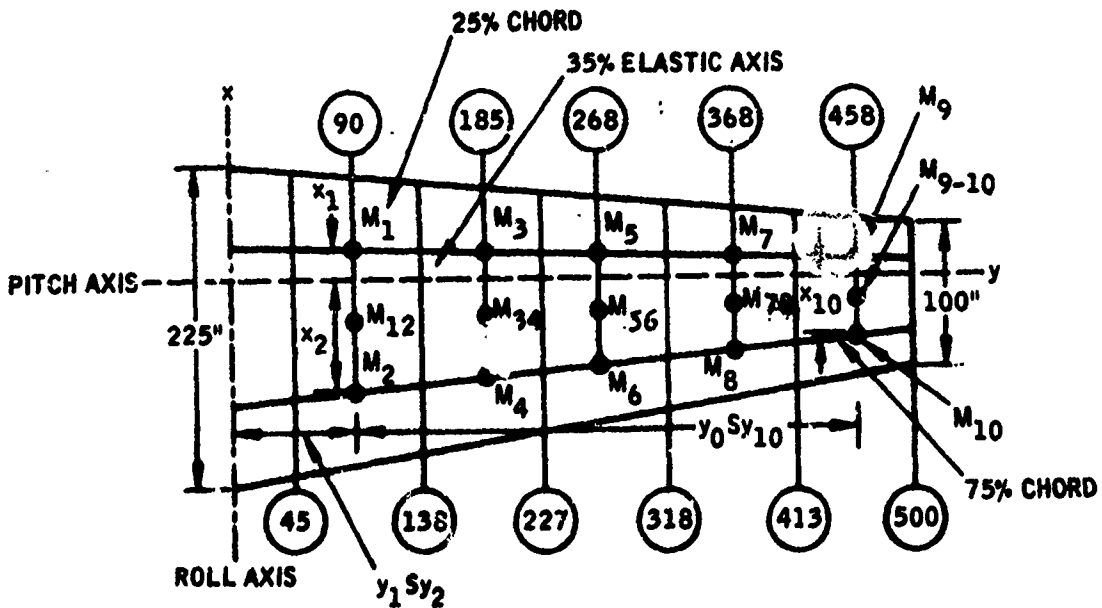


Figure A-1. Jet transport wing geometry.

In the antisymmetric case, the rigid component generalized mass matrix would be $[\Delta m] = [I_{x_0}]$, and in the composite longitudinal-lateral case, the generalized mass matrix would be

$$[\Delta m] = \begin{bmatrix} M_o & S_o & 0 \\ S_o & I_{y_0} & 0 \\ 0 & 0 & I_{x_0} \end{bmatrix}$$

The symmetrical case requires the two rigid-body degrees of freedom of plunging and pitching. The rigid-body modal matrix, therefore, consists of two columns: a unit column, and a column of the x-coordinate of each control point. The rigid-body modal matrix for the wing is

$$[h_R] = [1 \ x] = \begin{bmatrix} 1 & 20.25 \\ 1 & -81.00 \\ 1 & 17.85 \\ 1 & -71.40 \\ 1 & 15.80 \\ 1 & -63.20 \\ 1 & 13.30 \\ 1 & -53.20 \\ 1 & 11.05 \\ 1 & -44.20 \end{bmatrix}$$

The rigid-body modal matrix for the fuselage is

$$[h_{R_0}] = [1 \ x] = \begin{bmatrix} 1 & -373.30 \\ 1 & -248.30 \\ 1 & -123.30 \\ 1 & + 1.70 \\ 1 & +126.70 \end{bmatrix}$$

Note that the above matrix is used in computing the incremental generalized mass which results from the aerodynamic loads on one-half of the fuselage and, therefore, the x-coordinates must be given in the

proper order for the control points used in computing the fuselage AICs. [In this problem the fuselage AICs are hypothetical, but the x-coordinates are given in the order necessary for the slender-body theory AICs.]

The reference geometry for the wing is $b_{rw} = 5.468$ ft and $s_w = 37.917$ ft. The reference geometry for the fuselage is $b_{ro} = 5.468$ ft and $s_o = 18.9585$ ft. [We assume that the wing reference geometry was used to nondimensionalize the fuselage AIC matrix, and, because we require only one-half of the fuselage aerodynamic force, it can be obtained by setting $s_o = (1/2)s_w$.] Both example problems are carried out for the single reduced velocity $1/k_r = 16.67$ with the reference semichord for the system $b_r = 5.468$ ft and with sea-level density $\rho = 0.002378$ slugs/ft³.

The output modes, the flutter frequencies and velocities, and the required structural damping can be seen in the example problem printed output (pages A-55 through A-65).

The input keypunch sheets are given, followed by the computer output.

H I I A I R C R A F T
7094 FORTRAN CODING SHEET

NAME		PHONE	DATE	LOG NO.	PROB. NO.	PROG. NO.	IDENTIFICATION																				
1	JET TRANSPORT	EXAMPLE	PROBLEM	TITLE CARD	CANTILEVER CASE		HM100000																				
2	1	4	0	General Control Card			HM100001																				
3	1	0	0	Fidelity Matrix Normalizing Constant K (FORMAT 2E28)			HM100002																				
4	1	0	-07	ISX1 and ISV1 (Controls for Number of External Steps Control Points and [W]1 = .NSUR) (FORMAT 1E14)			HM100003																				
5	1	0		Reference b _i and Reference 1/r _i (FORMAT 2E12.8)			HM100004																				
6	1	0	16.67	Reference b _i and Reference 1/r _i for Each Strain (FORMAT 2E12.8)			HM100005																				
7	1	0	37.917	Density Series (FORMAT 2E12.8)			HM100006																				
8	1	0		NSIZE for Mass Matrix. [M] (FORMAT 1E4)			HM100007																				
9	1	0		Row Location of First and Last [LOW r, HIGH] Nonzero Element in Each Column of [M]			10HM100008																				
10	1	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25

STEC REV. 2-64

HUGHES AIRCRAFT COMPANY
7094 FORTRAN CODING SHEET

PAGE _____ OF _____

NAME _____ PHONE _____ DATE _____ LOG NO. _____ PROB. NO. _____ PROC. NO. _____

LINE NO.	CHARACTERS	IDENTIFICATION
1	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80	HM 100009
2	[M] Matrix Elements FORMAT (E12.8)	HM 100010
3	15383.6	HM 100011
4	134.9	HM 100012
5	20732.	HM 100013
6	11005.0	HM 100014
7	3113.9	HM 100015
8	139.7	HM 100016
9	2638.8	HM 100017
10	21.0	HM 100018
11	487.5	HM 100019
12	7.3	HM 100020
13	177.9	
14	10	
15	1	
16	0	
17	[M] Matrix Elements	
18	Central Card for Fortuity Matrix. [M] (FORMAT (E14))	
19	[M] Matrix Elements	
20	The matrix elements can be seen in the printed copy. The code card gives the size and specifies the format FORTRAN E12.8.	
21	by column. See Section V, Part B, Item 1 for other formats.	

HUGHES A. W. TAFT COMPA
7094 FORTSAN CODING SHEET

PAGE _____ OF _____

LINE NO.	NAME	PHONE	DATE	LOG NO.	PROG. NO.	IDENTIFICATION
1						
2						
3						
4						
5						
6						
7						
8						
9						
10						
11						
12						
13						
14						
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25						

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HUGHES AIRCRAFT COMPANY
7094 FORTRAN CODING SHEET

LINE NO.	NAME	PHONE	DATE	LOG NO.	IDENTIFICATION
1	LOW-LEVEL HIGH				HM 2 0 0 0 1 1
2	[[M] Matrix Elements				
3	Number of Rows in Rigid Component Rigid-Body Modal Matrix. [hrd] (FORMAT 1814)				HM 2 0 0 0 2 2
4					
5	[[Eo] Matrix Elements (FORMAT 6E2.8, by Columns)				HM 2 0 0 0 2 3
6	1.0				
7	-2.48.30				HM 2 0 0 0 2 4
8	Number of Rows in Surface Rigid-Body Modal Matrix [hb] (FORMAT 1818)				
9	1.0				HM 2 0 0 0 2 5
10	[[hb] Matrix Elements (FORMAT 6E12.8, by Columns)				
11	1.0				HM 2 0 0 0 2 6
12	1.0				HM 2 0 0 0 2 7
13	-31.0				HM 2 0 0 0 2 8
14	-53.20				HM 2 0 0 0 2 9
15	Control Card for [A]				HM 2 0 0 0 3 0
16	[[A] Matrix Elements				
17	[[K] Rigid Component [Eo] (FORMAT 6E2.8)				
18	16.67				
19					
20					
21					
22					
23					
24					
25					

HUGHES AIRCRAFT COMPANY
 7094 FORTRAN CODING SHEET

PAGE

NAME _____ PHONE _____ DATE _____ LOG NO. _____ PAGE _____

Line	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25
1																									
2																									
3																									
4																									
5																									
6																									
7																									
8																									
9																									
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22																									
23																									
24																									
25																									

Control Card for [Ch] Matrix Input [FORMAT 1314]
 [Ch] Matrix Elements (Column Binary Format)
 The above control card indicates a 5 x 5 (unpartitioned) matrix to be input using column binary format. The matrix can be seen in the printed output and will not be tabulated.
 (Other input formats are explained in Section II, Part B, Item 15.)
 1/4 for Surface [Ch] Matrix
 Control Card for Surface [Ch] Matrix Input
 [Ch] Matrix by Partitions

HIM 2 0 0 0 5 2
 HIM 2 0 0 0 6 4
 HIM 2 0 0 0 6 5

FLEXIBILITY MATRIX

SURFACE 1		SURFACE 2		SURFACE 3		SURFACE 4		SURFACE 5		SURFACE 6	
COLUMN 1	COLUMN 2	COLUMN 3	COLUMN 4	COLUMN 5	COLUMN 6	COLUMN 7	COLUMN 8	COLUMN 9	COLUMN 10	COLUMN 11	COLUMN 12
1	0.0177000E 02	1.1336100E 02	0.1777000E 03	0.0272000E 02	0.1625100E 03	0.1049200E 03	0.1492200E 03	0.3352000E 03	0.3762000E 03	0.5013500E 03	0.11344300E 04
2	0.1336100E 02	0.1777000E 03	0.1777000E 03	0.3249700E 03	0.4825500E 03	0.11344300E 04	0.1699000E 04	0.1816000E 04	0.2292000E 04	0.2429400E 04	0.2624900E 04
3	0.1777000E 03	0.1777000E 03	0.1777000E 03	0.3249700E 03	0.4825500E 03	0.11344300E 04	0.1699000E 04	0.1816000E 04	0.2292000E 04	0.2429400E 04	0.2624900E 04
4	0.0272000E 02	0.3249700E 03	0.3249700E 03	0.0272000E 02	0.1625100E 03	0.1049200E 03	0.1492200E 03	0.3352000E 03	0.3762000E 03	0.5013500E 03	0.11344300E 04
5	0.1625100E 03	0.4825500E 03	0.4825500E 03	0.1625100E 03	0.1049200E 03	0.1492200E 03	0.3352000E 03	0.3762000E 03	0.5013500E 03	0.11344300E 04	0.1699000E 04
6	0.1049200E 03	0.11344300E 04	0.11344300E 04	0.1699000E 04	0.1816000E 04	0.2292000E 04	0.2429400E 04	0.2624900E 04	0.2820400E 04	0.3015900E 04	0.3211400E 04
7	0.2047800E 03	0.3249700E 03	0.3249700E 03	0.0272000E 02	0.1625100E 03	0.1049200E 03	0.1492200E 03	0.3352000E 03	0.3762000E 03	0.5013500E 03	0.11344300E 04
8	0.1563000E 03	0.3502100E 03	0.3502100E 03	0.0272000E 02	0.1625100E 03	0.1049200E 03	0.1492200E 03	0.3352000E 03	0.3762000E 03	0.5013500E 03	0.11344300E 04
9	0.2429400E 03	0.2820400E 03	0.2820400E 03	0.0272000E 02	0.1625100E 03	0.1049200E 03	0.1492200E 03	0.3352000E 03	0.3762000E 03	0.5013500E 03	0.11344300E 04
10	0.2292000E 03	0.2429400E 03	0.2429400E 03	0.0272000E 02	0.1625100E 03	0.1049200E 03	0.1492200E 03	0.3352000E 03	0.3762000E 03	0.5013500E 03	0.11344300E 04
11	0.2624900E 03	0.3015900E 04	0.3015900E 04	0.0272000E 02	0.1625100E 03	0.1049200E 03	0.1492200E 03	0.3352000E 03	0.3762000E 03	0.5013500E 03	0.11344300E 04
12	0.2820400E 03	0.3211400E 04	0.3211400E 04	0.0272000E 02	0.1625100E 03	0.1049200E 03	0.1492200E 03	0.3352000E 03	0.3762000E 03	0.5013500E 03	0.11344300E 04

WEIGHTING MATRIX

SURFACE 1		SURFACE 2		SURFACE 3		SURFACE 4		SURFACE 5		SURFACE 6	
COLUMN 1	COLUMN 2	COLUMN 3	COLUMN 4	COLUMN 5	COLUMN 6	COLUMN 7	COLUMN 8	COLUMN 9	COLUMN 10	COLUMN 11	COLUMN 12
1	0.2047800E 03	0.1563000E 03	0.2429400E 03	0.2820400E 03	0.2624900E 03	0.2292000E 03	0.2047800E 03	0.1563000E 03	0.2429400E 03	0.2820400E 03	0.2624900E 03
2	0.1563000E 03	0.2047800E 03	0.1563000E 03	0.2429400E 03	0.2820400E 03	0.2624900E 03	0.2047800E 03	0.1563000E 03	0.2429400E 03	0.2820400E 03	0.2624900E 03
3	0.2429400E 03	0.1563000E 03	0.2429400E 03	0.2820400E 03	0.2624900E 03	0.2292000E 03	0.2047800E 03	0.1563000E 03	0.2429400E 03	0.2820400E 03	0.2624900E 03
4	0.2820400E 03	0.2429400E 03	0.2820400E 03	0.2624900E 03	0.2292000E 03	0.2047800E 03	0.1563000E 03	0.2429400E 03	0.2820400E 03	0.2624900E 03	0.2292000E 03
5	0.2624900E 03	0.2292000E 03	0.2624900E 03	0.2292000E 03	0.2047800E 03	0.1563000E 03	0.2429400E 03	0.2820400E 03	0.2624900E 03	0.2292000E 03	0.2047800E 03
6	0.2292000E 03	0.2047800E 03	0.2292000E 03	0.2047800E 03	0.1563000E 03	0.2429400E 03	0.2820400E 03	0.2624900E 03	0.2292000E 03	0.2047800E 03	0.1563000E 03
7	0.2047800E 03	0.1563000E 03	0.2047800E 03	0.1563000E 03	0.2429400E 03	0.2820400E 03	0.2624900E 03	0.2292000E 03	0.2047800E 03	0.1563000E 03	0.2429400E 03
8	0.1563000E 03	0.2429400E 03	0.1563000E 03	0.2429400E 03	0.2820400E 03	0.2624900E 03	0.2292000E 03	0.2047800E 03	0.1563000E 03	0.2429400E 03	0.2820400E 03
9	0.2429400E 03	0.1563000E 03	0.2429400E 03	0.2820400E 03	0.2624900E 03	0.2292000E 03	0.2047800E 03	0.1563000E 03	0.2429400E 03	0.2820400E 03	0.2624900E 03
10	0.2820400E 03	0.2429400E 03	0.2820400E 03	0.2624900E 03	0.2292000E 03	0.2047800E 03	0.1563000E 03	0.2429400E 03	0.2820400E 03	0.2624900E 03	0.2292000E 03
11	0.2624900E 03	0.2292000E 03	0.2624900E 03	0.2292000E 03	0.2047800E 03	0.1563000E 03	0.2429400E 03	0.2820400E 03	0.2624900E 03	0.2292000E 03	0.2047800E 03
12	0.2292000E 03	0.2047800E 03	0.2292000E 03	0.2047800E 03	0.1563000E 03	0.2429400E 03	0.2820400E 03	0.2624900E 03	0.2292000E 03	0.2047800E 03	0.1563000E 03

ALGEBRAIC MATRIX 1/K R = 0.100/000E 02
 SURFACE 1, 11 CONTROL POINTS

	COLUMN 1	COLUMN 2	COLUMN 3	COLUMN 4	COLUMN 5	COLUMN 6
1	0.3009700E 03	-0.6000000E 02	-0.0000000E 00	0.3227800E 02	0.	0.
2	0.1011010E 00	0.1651010E 02	0.5733550E 00	-0.8621410E 02	0.	0.
3	0.	0.	0.	0.	0.29334900E 03	-0.5152775E 02
4	0.	0.	0.	0.	0.14211053E 00	0.13934780E 02
5	0.	0.	0.	0.	0.	0.
6	0.	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.	0.
	COLUMN 7	COLUMN 8	COLUMN 9	COLUMN 10	COLUMN 11	COLUMN 12
1	0.	0.	0.	0.	0.	0.
2	0.2972241E 03	0.31240042E 02	0.	0.	0.	0.
3	0.4634856E 00	-0.13934780E 02	0.	0.	0.	0.
4	0.	0.	0.30481990E 03	-0.53868001E 02	-0.38027590E 03	0.51871550E 02
5	0.	0.	0.11084775E 00	0.42087991E 02	0.34154529E 00	-0.12687991E 02
6	0.	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.	0.
	COLUMN 13	COLUMN 14	COLUMN 15	COLUMN 16	COLUMN 17	COLUMN 18
1	0.	0.	0.	0.	0.	0.
2	0.	0.	0.	0.	0.	0.
3	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.
6	0.3248151E 03	-0.5278129E 02	-0.14787	0.3254100E 02	0.	0.
7	0.8021473E 01	0.1074502E 02	0.2520470E 00	-0.11079502E 02	0.	0.
8	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.30321474E 03	-0.43827802E 02
	COLUMN 19	COLUMN 20	COLUMN			
1	0.	0.	0.	0.	0.	0.
2	0.	0.	0.	0.	0.	0.
3	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.
6	0.	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.
10	0.1000000E 00	0.0000000E 00	0.0000000E 00	0.0000000E 00	0.0000000E 00	0.0000000E 00

OUTPUT DATA

FLUTTER ANALYSIS BY A COLLOCATION METHOD USING AERODYNAMIC INFLUENCE COEFFICIENTS

DENSITY = 0.25700000E+02 REDUCED VELOCITY = 0.16670000E+02

RIGID BODY DEGREES OF FREEDOM

MODE	EIGENVALUE	ITERATIONS	S.P.	S.P.	ATKENS	S.P.	U.P.
1	0.28514224E 00	18	0	2	2	0	0
2	0.17153621E 00	18	0	4	0	0	0
3	0.63295350E 07	10	0	4	4	0	0
4	0.24938801E 07	20	0	4	4	0	0

EIGENVECTORS

COLUMN	1	2	3	4	5	6
1	0.41705669E-01	0.39930714E-02	0.5422150E-01	0.27973628E-01	0.11760764E 00	-0.06122170E-01
2	0.33611071E-01	0.62527200E-02	0.01325000E-01	-0.2717133E-02	0.95014571E-01	-0.4760138E-01
3	0.14070067E 00	0.01289006E-02	0.77050650E 00	0.50252559E-01	0.20814691E 00	-0.6973300E-01
4	0.17642782E 00	0.13208503E-01	0.17790778E 00	-0.14884830E-02	0.24426274E 00	-0.50252559E-01
5	0.36193004E 00	0.17490007E-01	0.42532389E 00	0.06469743E-01	0.50779010E 00	-0.44839706E 00
6	0.34535172E 00	0.25592004E-01	0.34030001E 00	0.33068263E-01	0.59176231E 00	-0.17182145E 00
7	0.6771080E 00	0.14759703E-01	0.71753938E 00	0.68203350E-01	0.02465572E 00	-0.01978349E-01
8	0.65908200E 00	0.26087021E-01	0.74431901E 00	0.2992510E-01	0.06821067E 00	-0.1322259E 00
9	0.1000000E 01	0.57693996E-00	0.06504349E 00	0.27935110E-01	0.9370000E 00	0.65739503E-01
10	0.90171925E 00	0.14738217E-01	0.10000000E 01	0.71289627E-10	0.10000000E 01	0.14332015E-09
COLUMN 7						
1	-0.0250170E-01	-0.1184500E 00				
2	-0.1442210E 00	-0.0730790E-01				
3	-0.1972000E 00	-0.1172000E 00				
4	-0.1879000E 01	-0.1670200E 00				
5	-0.4091000E 00	-0.1730000E 00				
6	-0.4903000E 10	-0.2000000E 00				
7	-0.1312600E-01	-0.0000000E-01				
8	0.0540000E-01	0.0000000E 01				
9	0.0000000E 01	0.0000000E 01				
10	0.0000000E 01	0.0000000E 01				

CHECK EIGENVALUES AND EIGENVECTORS

MODE	FREQ (CPS)	DAMPING	VELOCITY (KNOTS)
1	0.18517534E 01	-0.86317019E 00	0.62794529E 03
2	0.28363506E 01	-0.23510478E -01	0.96183365E 03
3	0.59303258E 01	0.16747073E 00	0.13328069E 04
4	0.69164967E 01	-0.61758942E 00	0.23454407E 04

MODE	FREQ (CPS)	DAMPING	VELOCITY (KNOTS)
1	0.41765565E -01	0.57421844E -01	0.11260817E 00
2	0.33611786E -01	0.67227245E -02	0.95835350E -01
3	0.14070066E 00	0.81283441E -02	0.26811789E 00
4	0.12626694E 00	0.13288569E -01	0.24426423E 00
5	0.36103078E 00	0.17496533E -01	6.58779208E 00
6	0.34635159E 00	0.25592861E -01	0.59176783E 00
7	0.6771181E 00	0.14759617E -01	0.82485651E 00
8	0.65968186E 00	0.27876910E -01	0.86821284E 00
9	0.1000000E 01	0.10363474E -08	0.93069882E 00
10	0.00173218E 00	0.14730288E -01	0.10000000E 01

MODE	FREQ (CPS)	DAMPING	VELOCITY (KNOTS)
1	0.85493178E -01	-0.11845119E 00	0.48020418E -09
2	0.19421509E 00	-0.9738746E -01	0.10000000E 01
3	0.15970453E 00	-0.17268E 00	0.10000000E 01
4	0.18188963E 00	-0.176879E 00	0.10000000E 01
5	0.46007509E 00	-0.1309738E 00	0.10000000E 01
6	0.45833512E 00	-0.20537629E 00	0.10000000E 01
7	0.18102238E -01	-0.66989833E -01	0.10000000E 01
8	0.97884560E -02	-0.12320435E 00	0.10000000E 01
9	0.10000000E 01	0.81152384E -09	0.10000000E 01
10	0.95823533E 00	-0.11462694E -01	0.10000000E 01

JET TRANSPORT EXAMPLE PROBLEM - SYMMETRIC CASE
 FLUTTER ANALYSIS BY A COLLOCATION METHOD USING AERODYNAMIC INFLUENCE COEFFICIENTS

PM651699

NSUR = 1 MAFRO = 1 MRIGID = 2 NFUS = 1 MPENS = 1 MODES OUT = 4 NDELM = 1 NPUNCH = 0
 R RIGID COMPONENT = 0.5468000E 01 S RIGID COMPONENT = 0.18958500E 02

H (REF) = 0.5468000E 01 K = 0.10000000E-06

SURFACE 1 SURFACE 8 SURFACE S
 0.5468000E 01 0.5468000E 01 0.3791700E 02
 0.5468000E 01 0.5468000E 01 0

RIGID COMPONENT MASS MATRIX

COLUMN 1 COLUMN 2 COLUMN 3
 0.1740000E 05 0.1770000E 07
 0.3370200E 07 0.4570072E 10

MASS MATRIX

	SURFACE 1		SURFACE 8		SURFACE S	
	COLUMN 1	COLUMN 2	COLUMN 3	COLUMN 4	COLUMN 5	COLUMN 6
1	0.5383600E 04	-0.1490000E 03	0.	0.	0.	0.
2	-0.1349000E 03	0.9222000E 03	0.	0.	0.	0.
3	0.	0.	0.7073000E 05	-0.11005000E 05	0.	0.
4	0.	0.	-0.11005000E 05	0.11478000E 05	0.	0.
5	0.	0.	0.	0.	0.31109000E 04	0.130
6	0.	0.	0.	0.	0.13970000E 03	0.00
7	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.	0.

CONTROL POINTS

	SURFACE 1		SURFACE 8		SURFACE S	
	COLUMN 7	COLUMN 8	COLUMN 9	COLUMN 10	COLUMN 11	COLUMN 12
1	0.	0.	0.	0.	0.	0.
2	0.	0.	0.	0.	0.	0.
3	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.
6	0.	0.	0.	0.	0.	0.
7	0.2638800E 04	-0.2100000E 02	0.	0.	0.	0.
8	-0.2100000E 02	0.8033000E 03	0.	0.	0.73060000E 01	0.
9	0.	0.	0.4875000E 03	0.	0.17790000E 03	0.
10	0.	0.	0.73060000E 01	0.	0.17790000E 03	0.

RIGID COMPONENT MODES

	SURFACE 1		SURFACE 8		SURFACE S	
	COLUMN 1	COLUMN 2	COLUMN 3	COLUMN 4	COLUMN 5	COLUMN 6
1	0.1000000E 01	-0.3733000E 03	0.	0.	0.	0.
2	0.1000000E 01	-0.2583000E 03	0.	0.	0.	0.
3	0.1000000E 01	0.1300000E 03	0.	0.	0.	0.
4	0.1000000E 01	0.4700000E 03	0.	0.	0.	0.
5	0.1000000E 01	0.1267000E 01	0.	0.	0.	0.

RIGID BODY MODAL MATRIX
SURFACE 1, 10 CONTROL POINTS

	COLUMN 1	COLUMN 2	COLUMN 3	COLUMN 4	COLUMN 5	COLUMN 6
1	0.1360000E 01	1.2029000E 02				
2	0.1360000E 01	-0.8500000E 02				
3	0.1000000E 01	0.1785000E 02				
4	0.1000000E 01	-0.7184000E 02				
5	0.1000000E 01	0.1280000E 02				
6	0.1000000E 01	-0.6320000E 02				
7	0.1000000E 01	0.1336000E 02				
8	0.1000000E 01	-0.5220000E 02				
9	0.1000000E 01	0.1105000E 02				
10	0.1000000E 01	-0.4420000E 02				

FLEXIBILITY MATRIX
SURFACE 1, 10 CONTROL POINTS

	COLUMN 1	COLUMN 2	COLUMN 3	COLUMN 4	COLUMN 5	COLUMN 6
1	0.8717200E 02	0.1336000E 02	0.1277000E 03	0.6272000E 02	0.1625100E 03	0.10492200E 03
2	0.1336100E 02	0.3086100E 03	0.6272000E 02	0.5229700E 03	0.10492200E 03	0.33529000E 03
3	0.1277900E 03	0.6272100E 02	0.2772000E 03	0.1577600E 03	0.4825500E 03	0.37628000E 03
4	0.6272000E 02	0.5229700E 03	0.1577600E 03	0.6374900E 03	0.3762800E 03	0.80136000E 03
5	0.1625100E 03	0.1049200E 03	0.4825500E 03	0.3762800E 03	0.1275800E 04	0.11344300E 04
6	0.1049200E 03	0.3352900E 03	0.3762800E 03	0.8013600E 03	0.11344300E 04	0.16999000E 04
7	0.3352900E 03	0.1049200E 03	0.3762800E 03	0.6433800E 03	0.1935000E 04	0.18160000E 04
8	0.2047000E 03	0.1561000E 03	0.6433800E 03	0.1001210E 04	0.1816000E 04	0.22920000E 04
9	0.1561000E 03	0.3502100E 03	0.6433800E 03	0.8637800E 03	0.2528300E 04	0.24294000E 04
10	0.2047000E 03	0.3502100E 03	0.8637800E 03	0.1181060E 04	0.2429400E 04	0.28249000E 04

COLUMN 7

	COLUMN 7	COLUMN 8	COLUMN 9	COLUMN 10
1	0.2047000E 03	0.1561000E 03	0.2429400E 03	0.2047000E 03
2	0.1561000E 03	0.3502100E 03	0.2047000E 03	0.3578500E 03
3	0.2429400E 03	0.2047000E 03	0.9581000E 03	0.88378000E 03
4	0.2047000E 03	0.1561000E 03	0.88378000E 03	0.11810600E 04
5	0.1935000E 04	0.1816000E 04	0.2528300E 04	0.24294000E 04
6	0.1816000E 04	0.2292000E 04	0.2429400E 04	0.28249000E 04
7	0.3602000E 04	0.3502100E 04	0.5267500E 04	0.51171000E 04
8	0.3502100E 04	0.4292000E 04	0.51171000E 04	0.57187000E 04
9	0.5267500E 04	0.51171000E 04	0.8484000E 04	0.82340000E 04
10	0.51171000E 04	0.57187000E 04	0.82340000E 04	0.92340000E 04

WEIGHTING MATRIX
SURFACE 1, NO WEIGHTING MATRIX

	COLUMN 1	COLUMN 2	COLUMN 3	COLUMN 4	COLUMN 5	COLUMN 6
1						
2						
3						
4						
5						
6						
7						
8						
9						
10						

RIGID COMPONENT AERO MATRIX S. CONTROL POINTS

	COLUMN 1	COLUMN 2	COLUMN 3	COLUMN 4	COLUMN 5	COLUMN 6
1	-0.1988336E 01	0.1022447E 01	-0.5178207E 01	0.99733821E 01	0.17128096E 01	-0.24681993E 01
2	0.20347044E 01	-0.50574088E 01	-3.89710978E 01	0.67589525E 00	0.25888789E 01	0.32829872E 01
3	0.	0.	0.25888789E 01	-0.32829872E 01	-0.89710928E 01	-0.67589525E 00
4	0.	0.	0.	0.	0.18608618E 01	-0.23997268E 01
5	0.	0.	0.	0.	0.19459838E 00	0.73566824E 00

	COLUMN 7	COLUMN 8	COLUMN 9	COLUMN 10
1	0.	0.	0.	0.
2	0.	0.	0.	0.
3	0.20347044E 01	0.30575088E 01	0.	0.17538263E 01
4	-0.5988403E 01	-0.47440609E 00	0.17700520E 01	0.81588698E 00
5	0.4545274E 00	-0.31680244E 01	-0.59732837E 01	0.81588698E 00

AERODYNAMIC MATRIX 1-K R = 0.1667000E 02

	COLUMN 1	COLUMN 2	COLUMN 3	COLUMN 4	COLUMN 5	COLUMN 6
1	0.3009970E 03	-0.6099267E 02	-0.4057001E 03	0.3227829E 02	0.	0.
2	0.1931181E 00	0.1623119E 02	0.5713544E 00	-0.1671411E 02	0.	0.
3	0.	0.	0.	0.	0.2933498E 03	-0.5615277E 02
4	0.	0.	0.	0.	0.1421153E 00	0.13930788E 02
5	0.	0.	0.	0.	0.	0.
6	0.	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.	0.
	COLUMN 7	COLUMN 8	COLUMN 9	COLUMN 10	COLUMN 11	COLUMN 12
1	0.	0.	0.	0.	0.	0.
2	0.	0.	0.	0.	0.	0.
3	-0.272824E 03	0.3124032E 02	0.	0.	0.	0.
4	0.4263405E 00	-0.1395774E 02	0.	0.	0.	0.
5	0.	0.	0.3058399E 03	-0.5068806E 02	-0.30027594E 03	0.31671554E 02
6	0.	0.	0.1338477E 00	0.1268799E 02	0.34154329E 00	-0.1268799E 02
7	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.	0.
	COLUMN 13	COLUMN 14	COLUMN 15	COLUMN 16	COLUMN 17	COLUMN 18
1	0.	0.	0.	0.	0.	0.
2	0.	0.	0.	0.	0.	0.
3	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.
6	0.	0.	0.	0.	0.	0.
7	0.3248325E 03	-0.5227814E 02	-0.2276746E 03	0.32541166E 02	0.	0.
8	0.8421623E-01	0.1197956E 02	0.2526407E 00	-0.1337956E 02	0.30321474E 03	-0.4362788E 02
9	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.52326897E-01	0.6430026E 01
	COLUMN 19	COLUMN 20	COLUMN 21	COLUMN 22	COLUMN 23	COLUMN 24
1	0.	0.	0.	0.	0.	0.
2	0.	0.	0.	0.	0.	0.
3	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.
6	0.	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.
9	-0.1052102E 03	0.2851713E 02	0.	0.	0.	0.
10	0.1997164E 00	-0.0030024E 01	0.	0.	0.	0.

OUTPUT DATA

FLUTTER ANALYSIS BY A COLLOCATION METHOD, USING AERODYNAMIC INFLUENCE COEFFICIENTS

DENSITY = 0.2378000E-02 REDUCED VELOCITY = 0.16670000E-02

RIGHT BODY DEGREES OF FREESON

ITERATIONS S.P. U.P. AITKENS S.P. U.P.

EIGENVALUE

MODE	ITERATIONS	S.P.	U.P.	AITKENS S.P.	U.P.
1	13	0	3	0	0
2	15	0	4	0	0
3	13	0	6	0	0
4	18	0	4	0	0

EIGENVECTORS

COLUMN	1	2	3	4	5	6
1	-0.2267220E 00	0.9788124E-01	-0.3098063E 00	-0.1024993E 00	-0.1156634E 00	0.1052824E-02
2	-0.2432261E 00	0.9623145E-01	-0.3175799E 00	-0.1372330E 00	-0.1428234E 00	0.4208415E-03
3	-0.1889654E 00	0.9012853E-01	0.3683428E-02	-0.7233892E-01	0.3934475E-01	-0.3721788E-01
4	-0.1314023E 00	0.9091440E-01	0.3869129E-02	-0.1285663E 00	0.6288741E-02	-0.4150640E-01
5	0.1039073E 00	0.8266946E-01	0.2738499E 00	-0.1587238E-01	0.3896276E 00	-0.1403765E 00
6	0.1389319E 00	0.9180556E-01	0.2771121E 00	-0.7091994E-01	0.3813744E 00	-0.1581460E 02
7	0.5735265E 00	0.5146260E-01	0.6386342E 00	0.2094076E-01	0.7214868E 00	-0.9310759E-01
8	0.5457153E 00	0.6242830E-01	0.6474863E 00	-0.2646831E-01	0.7514715E 00	-0.1374385E 00
9	0.1400030E 01	0.3925881E-00	0.9869487E 00	0.36698160E-01	0.9438403E 00	0.6712134E-01
10	0.9716649E 00	0.1928632E-01	0.1000000E 01	0.10248185E-09	0.1000000E 01	0.73126528E-09

COLUMN

COLUMN	7	8
1	0.5951750E-01	-0.2865716E-01
2	0.3740337E-01	-0.3745680E-02
3	-0.6179831E-01	-0.4192661E-01
4	-0.7226718E-01	-0.5864427E-01
5	-0.5383095E 00	-0.1374365E 00
6	-0.5181013E 00	-0.1636344E 00
7	-0.1207990E 00	-0.6996788E-01
8	-0.8707179E-01	-0.1380777E 00
9	0.1000000E 01	0.1000000E 01
10	0.9430371E 00	-0.9070476E-02

CHECK EIGENVALUES AND EIGENVECTORS

	0.2291607E 06	-0.1592555E 06	0.1301411E 05	-0.1569169E 06	0.4890500E 07	0.1360439E 07												
	0.1994759E 07	-0.1231507E 07																
	COLUMN 1	COLUMN 2	COLUMN 3	COLUMN 4	COLUMN 5	COLUMN 6												
1	-0.2247210E 06	0.9780124E-01	-0.1093607E 00	-0.1024992E 00	-0.1156632E 00	0.1087939E-02												
2	-0.2437201E 00	0.9623146E-01	-0.1125298E 00	-0.1372329E 00	-0.1420232E 00	0.4280173E-03												
3	-0.1089654E 00	0.9012456E-01	0.3683497E-02	-0.7243889E-01	0.3934489E-01	-0.3721773E-01												
4	-0.1314021E 00	0.9591447E-01	0.3869231E-02	-0.1286630E 00	0.6260245E-02	-0.4350637E-01												
5	-0.1639735E 00	0.9466946E-01	0.2738499E 00	-0.1587235E-01	0.3696277E 00	-0.1403485E 00												
6	-0.1089196E 00	0.9380552E-01	0.2771122E 00	-0.1051997E-01	0.3813746E 00	-0.1581466E 00												
7	-0.5735265E 00	0.5146266E-01	0.6390143E 00	0.2094076E-01	0.7214869E 00	0.9310964E-01												
8	-0.5457134E 00	0.6424832E-01	0.6447480E 00	-0.2646030E-01	0.7514716E 00	-0.1374736E 00												
9	0.1060010E 01	0.1825682E-04	0.6694071E 00	0.3669810E-01	0.9430840E 00	0.0712124E-01												
10	0.2910638E 00	0.1122002E-01	0.1000000E 01	0.1926815E-10	0.1000000E 01	0.1159552E-08												
	COLUMN 7	COLUMN 8																
1	0.5251719E-01	-0.2863931E-01																
2	0.3750271E-01	-0.3145196E-02																
3	-0.6129824E-01	-0.8192367E-01																
4	-0.7267375E-01	-0.5864522E-01																
5	-0.5363085E 00	-0.1174523E 00																
6	-0.5163036E 00	-0.1630335E 00																
7	-0.1207081E 00	-0.6962363E-01																
8	-0.8736019E-01	-0.1180159E 00																
9	0.1000000E 01	0.1000000E 01																
10	0.9430927E 00	-0.8078056E-02																

MODE	FREQY (GCS)	DAMPING	VELOCITY (KNOTS)
1	0.2084798E 01	-0.6944371E 00	0.7081911E 03
2	0.2749231E 01	-0.1205697E-01	0.9294703E 03
3	0.4471368E 01	0.2781806E 00	0.1516268E 04
4	0.69985134E 01	-0.6369962E 00	0.2373255E 04

SECTION 8
PROGRAM LISTING

```

$ OPTION FORTRAN
$ FORTRAN LSTOU,DECK
C MAIN FLUTTER OVERLAY
C JAN 13,1967
COMM, J IT(218)
C CHANGE BCD TAPES TO BINARY TAPES
10 CALL LLINK (4HPAR/TT)
CALL PART1
CALL LLINK (4HPAR/TT)

CALL PART2
GO TO 10
END

$ FORTRAN LSTOU,DECK
C MPRINT
SURROUTINE MPRINT (A,M,N,MD,NTAPE)
DIMENSION A(1), IT(6), C(6)
EQUIVALENCE (IT,C)
2 FORMAT (1H , 4X, 6( 6X, 7HCOLUMN 114 ) /// )
3 FORMAT (1H 114, X, (6E 17.8) )
N1=N
N2=6
N3=6
N4=1
4 IF (N3-N1) 6,6,5
5 N2=N1-N3+6
N3=N1
6 K=0
DO 7 I= N4,N1
K=K+1
IT(K)=I
7 WRITE (NTAPE,2) (IT(I),I=1,N2)
DO 9 J=1,M
K=0
L=MD*(N4-1)+1
DO 8 J=N4,N3
K=K+1
C(K)=A(L)
L=L+MD
8 WRITE (NTAPE,3) L,(C(K),K=1,N2)
IF (N3-N1) 10,11,11
10 N3=N3+6
N4=N4+6
GO TO 4
11 RETURN
END

$ FORTRAN LSTOU,DECK
C MPUNCH
SURROUTINE MPUNCH(A,M,N,IOUT,ITRA,IORG,BCDZ,MAXM,NTAPE,NCARDS)
DIMENSION A(1)
RETURN
END

$ LINK PART1
$ FORTRAN LSTOU,DECK
C PART1
SURROUTINE PART1
NSUR=TOTAL NUMBER OF SURFACES ALLOWED.
NDENS=TOTAL NUMBER OF DENSITIES ALLOWED.
NRIGID=TOTAL NUMBER OF RIGID BODIES ALLOWED
NSIZE=TOTAL NUMBER CONTROL POINTS ON ANY ONE SURFACE ALLOWED
NMODES=TOTAL NUMBER MODES INPUT ON ANY ONE SURFACE.

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HM14007
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005
006

DIMENSION	ISXST(20), ISW(20), BR(21), S(21), RHO(20), UM(6,6),	01
1	DU(6,12), DMBAR(6,12), HARMRP(6,12), LOW(50), LHIGH(20)	013
2	, IT(218), VELCT(20), NSIZES(20),	01
3	A(50,100), F(50,100), U(50,100), HR(50,6), HRT(6,100),	016
4	HT(6,100), G(6,100)	017

C THE FOLLOWING STATEMENT(S) HAVE BEEN MANUFACTURED BY THE TRANSLATOR TO
 COMPENSATE FOR THE FACT THAT EQUIVALENCE DOES NOT REORDER COMMON---

COMMON IT
 EQUIVALENCE

1	(IT(1), ISXST), (IT(21), ISW), (IT(41), RHO),	025
2	(IT(61), NTAPE1), (IT(62), NTAPE2), (IT(63), NTAPE3),	02
3	(IT(64), NTAPE4), (IT(65), NTAPE5), (IT(66), NTAPE6),	028
4	(IT(67), NTAPE7), (IT(68), NTAPE8), (IT(69), NTAPE9),	02
5	(IT(70), NSUR), (IT(71), NRIGID), (IT(72), BREF),	03
6	(IT(73), NAERO), (IT(74), NFUS), (IT(75), NDENS),	033
7	(IT(76), MODES), (IT(77), NPOINT), (IT(78), NPUNCH),	032
8	(IT(79), MAXR), (IT(80), MAXQ), (IT(81), MAXS),	03
9	(IT(82), NC), (IT(83), NSURFS), (IT(84), NP2),	034
10	(IT(85), BR), (IT(106), S), (IT(127), VELCTY),	035
11	(IT(147), NTAPEU), (IT(148), NRHO), (IT(149), NITRSP),	03
12	(IT(150), NITRDP), (IT(151), FPSP), (IT(152), FPPD),	03
13	(IT(153), PICON), (IT(154), NVEL), (IT(155), NCARDS),	038
14	(IT(156), AITKEN), (IT(157), NGO), (F,0), (F(601,1), HT)	039
15	(U,LOW), (U(51,1), LHIGH), (IT(158), FK), (IT(159), SQR	04
16	(IT(160), NSIZES), (IT(180), UM), (DMBAR, HARMRR)	041
17	(IT(216), NDELH), (IT(217), AITKED), (IT(218), KPART)	043

1	FORMAT (1814)	043
2	FORMAT (6E12.8)	044
3	FORMAT (1H 16X, 41H FLUTTER ANALYSIS BY A COLLOCATION METHOD	044
4	42H USING AERODYNAMIC INFLUENCE COEFFICIENTS // 10H NSUR =	046
5	112, 10H NAERO = 114, 11H NRIGID = 112, 9H NFUS =	047
6	112, 10H NDENS = 114, 14H MODES OUT = 112	04
7	, 9H NDELM = 112, 10H NPUNCH = 112)	049
8	FORMAT (1H0.22X, 11H B (REF) = 1E20.8, 5X, 4HK = 1E20.8 // 1HU 25X,	050
9	7HSURFACE 18X, 1HR 19X, 1HS 10X, 20HEXTERNAL STORES SIZE //)	051
10	FORMAT (1H0 10X, 21H B RIGID COMPONENT = 1E18.8, 5Y, 8H S RIGID	054
11	13H COMPONENT = 1E18.8)	053
12	FORMAT (1H 1129, 2(5X, 1E20.8), 1112)	057
13	FORMAT (1H1 48X, 12H MASS MATRIX)	051
14	FORMAT (41H0 NUMBER OF CONTROL POINTS THIS MATRIX, (114,	056
15	1 48H) AND TOTAL NUMBER OF CONTROL POINTS EXPECTED, (114,	057
16	2 57H) DO NOT AGREE. PROGRAM CONTINUED....)	051
17	FORMAT (1H) 42X, 24H RIGID BODY MODAL MATRIX)	059
18	FORMAT (1H 58X, 8HSURFACE 112, 1H, 116, 15H CONTROL POINTS)	060
19	FORMAT (1H) 41X, 20H FLEXIBILITY MATRIX)	06
20	FORMAT (1H) 46X, 18H WEIGHTING MATRIX)	06
21	FORMAT (1H) 20X, 20H RIGID COMPONENT AERO MATRIX, 119, 8H CONTROL	063
22	1 7H POINTS)	064
23	FORMAT (1H) 31X, 20H AERODYNAMIC MATRIX 8X, 10H 1./K R =	06
24	1 1E20.8)	066
25	FORMAT (1H0 40X, 23H RIGID COMPONENT MODES, 1110,	067
26	1 17H CONTROL POINTS.)	06
27	FORMAT (1H0 50X, 24H RIGID COMPONENT MASS MATRIX)	06
28	FORMAT (47H) ERROR IN INVERSE ROUTINE. PROGRAM TERMINATED)	070
29	FORMAT (1H 58X, 8HSURFACE 112, 1H, 6X, 13H NO WEIGHTING	071
30	1 7H MATRIX)	071
31	FORMAT (3E12.8, 214)	073
32	FORMAT (4H0FPSP = 1E16.8, 1X, 8H EPDP = 1E16.8, 1X,	074
33	1 10H AITKEN = 1E16.8, 1X, 10H NITRSP = 114, 1X,	071
34	2 10H NITRDP = 114)	071
35	FORMAT (1H0 40X, 20H GENERALIZED MASSES // // (1H 30X,	077
36	1 5H MASS 114, 5H = 1E16.8))	071

25	FORMAT	(1H0 30X, 23H RIGID COMPONENT MODES	///)	079
26	FORMAT	(214, 62X, 1A6, 114)		080
27	FORMAT	(1H0 33X, 23H PUNCHED CARDS NUMBERS	1A6, 114, 6H THRU	081
		1A6, 114)		082
28	FORMAT	(1H0 20X, 3H K= 1E16.R)		083
		DATA Q000CT/02020.50440005/		
		RCDZ =Q000CT		085

```

S      OPTION FORTRAN
S      FORTRAN LISTING DECK
C MAIN  FLUTTER OVERLAY
C      JAN 15, 1967
C      COMMON IT(218)
C      CHANGE BCD TAPES TO BINARY TAPES
10 CALL LLINK (6HPAR1TT)
      CALL PART1
      CALL LLINK (6HPAR2TT)

```

```

$      OPTION FORTRAN
$      FORTRAN LSTOU,DECK
C MAIN      FLUTTER OVERLAY
C           JAN 13,1967
COMMON IT(218)
C CHANGE BCD TAPES TO BINARY TAPES
10 CALL LLINK (6HPAR1TT)
CALL PART1
CALL LLINK (6HPAR2TT)

CALL PART2
GO TO 10
END

$      FORTRAN LSTOU,DECK
C MPRINT
SURROUTINE MPRINT (A,M,N,MD,NTAPE)
DIMENSION A(1), IT(6), C(6)
EQUIVALENCE (IT,C)
2 FORMAT (1H , 4X, 6( 6X, 7HCOLUMN 114 ) /// )
3 FORMAT (1H 114, X, (6E 17.8) )
N1=N
N2=6
N3=6
N4=1
4 IF (N3-N1) 6,6,5
5 N2=N1-N3+6
N3=N1
6 K=0
DO 7 I= N4,N3
K=K+1
7 IT(K)=I
WRITE (NTAPE,2) (IT(I),I=1,N2)
DO 9 I=1,M
K=0
I=MD*(N4-1)+I
DO 8 J=N4,N3
K=K+1
C(K)=A(I)
I=L+MD
8 WRITE (NTAPE,3) I,(C(K),K=1,N2)
IF (N3-N1) 10,11,11
10 N3=N3+6
N4=N4+6
GOTO 4
11 RETURN
END

$      FORTRAN LSTOU,DECK
C MPUNCH
SURROUTINE MPUNCH(A,M,N,IOUT,ITRA,IORG,BCDZ,MAXM,NTAPE,NCARDS)
DIMENSION A(1)
RETURN
END

$      LINK PAR1TT
$      FORTRAN LSTOU,DECK
C PART1
SURROUTINE PART1
C NSUR=TOTAL NUMBER OF SURFACES ALLOWED.
C NDENS=TOTAL NUMBER OF DENSITIES ALLOWED.
C NRIGID=TOTAL NUMBER OF RIGID BODIES ALLOWED
C NSTZF=TOTAL NUMBER CONTROL POINTS ON ANY ONE SURFACE ALLOWED
C NMODES=TOTAL NUMBER MODES INPUT ON ANY ONE SURFACE.

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HM14007
HM140078
HM140079
HM14008
HM14008
HM140084
HM14008
HM14008
HM140087
HM140088
HM14008
HM14009
HM140091
HM14009
HM14009
HM140094
HM14009
HM140097
HM140098
HM14009
HM14010
HM140101
HM140102
HM140104
HM140105
HM140106
HM140107
HM140108
HM140109

0010
0020
0030
0040

0010
0020
0030
0040
0050
0060

DIMENSION	ISXST(20), ISW(20), HR(21), S(21), RHO(20), DM(6,6),	0120
1	DO(6,12), DMBAR(6,12), BARMRR(6,12), LOW(50), LHIGH(50)	0130
2	, IT(218), VELCTY(20), NSIZES(20),	0140
3	A(50,100), F(50,100), U(50,100), HR(50,6), IRT(6,100),	0150
4	HT(6,100), G(6,100)	0160
C	THE FOLLOWING STATEMENT(S) HAVE BEEN MANUFACTURED BY THE TRANSLATOR TO	0170
C	COMPENSATE FOR THE FACT THAT EQUIVALENCE DOES NOT REORDER COMMON---	0180
	COMMON IF	0190
	EQUIVALENCE (IT(1),ISXST), (IT(21),ISW), (IT(41),RHO)	0250
1	, (IT(61),NTAPE1), (IT(62),NTAPE2), (IT(63),NTAPE3),	0260
2	(IT(64),NTAPE4), (IT(65),NTAPE5), (IT(66),NTAPE6),	0270
3	(IT(67),NTAPE7), (IT(68),NTAPE8), (IT(69),NTAPE9),	0280
4	(IT(70),NSUR), (IT(71),NRIGID), (IT(72),HREF),	0290
5	(IT(73),NAERO), (IT(74),NFUS), (IT(75),NDENS),	0300
6	(IT(76),MODES), (IT(77),NPOINT), (IT(78),NPUNCH),	0310
7	(IT(79),MAXR), (IT(80),MAXU), (IT(81),MAXS),	0320
8	(IT(82),NC), (IT(83),NSURFS), (IT(84),N02),	0330
9	(IT(85),HR), (IT(106),S), (IT(127),VELCTY)	0340
	EQUIVALENCE (IT(147),NTAPE0), (IT(148),NRHO), (IT(149),NITRSP),	0350
1	(IT(150),NITRDP), (IT(151),EPSP), (IT(152),EPDP),	0360
2	(IT(153),PICON), (IT(154),NVEL), (IT(155),NCARDS),	0370
3	(IT(156),AITKEN), (IT(157),NGO), (F,G), (F(601,1),HT)	0380
4,	(U,LOW), (U(51,1),LHIGH), (IT(158),FK), (IT(159),SQR	0390
5CON)	, (IT(160),NSIZES), (IT(180),DM), (DMBAR,BARMRR)	0400
6	, (IT(216),NDELM), (IT(217),AITKED), (IT(218),KPART)	0410
1	FORMAT (18I4)	0430
2	FORMAT (6E12.8)	0440
3	FORMAT (1H 16X, 41H FLUTTER ANALYSIS BY A COLLOCATION METHOD	0450
1	42H USING AERODYNAMIC INFLUENCE COEFFICIENTS ///10H NSUR =	0460
2	112, 10H NAERO = 114, 11H NRIGID = 112, 9H NFUS =	0470
3	112, 10H NDENS = 114, 14H MODES OUT = 112	0480
4	, 9H NDELM = 112, 10H NPUNCH = 112)	0490
4	FORMAT (1H0 22X, 11H B (REF) = 1E20.8, 5X, 4HK = 1E20.8 /1H0 25X,	0500
1	7HSURFACE 18X, 1HB 19X, 1HS 10X, 20HEXTERNAL STORES SIZE ///	0510
5	FORMAT (1H0 10X, 21H B RIGID COMPONENT = 1E18.8, 5V, 8H S RIGID	0520
1	13H COMPONENT = 1E18.8)	0530
6	FORMAT (1H 1E20, 2(5X, 1E20.8), 1112)	0540
10	FORMAT (1H1 48X, 12H MASS MATRIX)	0550
11	FORMAT (41H0 NUMBER OF CONTROL POINTS THIS MATRIX, (114,	0560
1	48H) AND TOTAL NUMBER OF CONTROL POINTS EXPECTED, (114,	0570
2	37H) DO NOT AGREE, PROGRAM CONTINUED....)	0580
12	FORMAT (1H1 42X, 24H RIGID BODY MODAL MATRIX)	0590
13	FORMAT (1H 38X, 8HSURFACE 112, 1H, 116, 15H CONTROL POINTS)	0600
14	FORMAT (1H1 43X, 20H FLEXIBILITY MATRIX)	0610
15	FORMAT (1H1 46X, 18H WEIGHTING MATRIX)	0620
16	FORMAT (1H1 29X, 29H RIGID COMPONENT AERO MATRIX, 119, 8H CONTROL	0630
1	7H POINTS)	0640
17	FORMAT (1H1 34X, 20H AERODYNAMIC MATRIX 8X, 10H 1./K R =	0650
1	1E20.8)	0660
18	FORMAT (1H0 50X, 23H RIGID COMPONENT MODES, 1110,	0670
1	17H CONTROL POINTS.)	0680
19	FORMAT (1H0 50X, 29H RIGID COMPONENT MASS MATRIX)	0690
20	FORMAT (47H) ERROR IN INVERSE ROUTINE, PROGRAM TERMINATED)	0700
21	FORMAT (1H 38X, 8HSURFACE 112, 1H, 6X, 13H NO WEIGHTING	0710
1	7H MATRIX)	0720
22	FORMAT (3E12.8, 214)	0730
23	FORMAT (8H0 EPSP = 1E16.8, 1X, 8H EPDP = 1E16.8, 1X,	0740
1	10H AITKEN = 1E16.8, 1X, 10H NITRSP = 114, 1X,	0750
2	10H NITRDP = 114)	0760
24	FORMAT (1H0 40X, 20H GENERALIZED MASSES //// (10 30X,	0770
1	5H MASS 114, 3H = 1E16.8))	0780

25	FORMAT	(140 3IX, 23H RIGID COMPONENT MODES ///)	0790
26	FORMAT	(214, 62X, 1A6, 114)	0800
27	FORMAT	(140 3IX, 23H PUNCHED CARDS NUMBERS 1A6, 114, 6H THRU 1 1A6, 114)	0810
28	FORMAT	(140 20X, 3H K= 1E16.8)	0820
		DATA Q000CT/0202030440005/	0830
		RCDZ =Q000CT	0850
C		NTAPE0 = PUNCH OUTPUT TAPE	0860
C		NTAPE2 = INPUT TAPE	0880
C		NTAPE3 = OUTPUT PRINT TAPE	0890
C		NTAPE4 = /	0900
C		NTAPE5 = / ARE UTILITY TAPES	0910
C		NTAPE6 = /	0920
C		NTAPE7 = /	0930
C		NTAPE8 = /	0940
C		NTAPE9 = /	0950
	IF	(NGO-98765) 90,97,99	0960
97	IF	(NAFRO) 98,320,98	0970
98	NAERO = NAERO-1		0980
	IF	(NAFRO) 99,99,170	0990
99	NTAPE0 = 8		1000
	NTAPE2 = 5		
	NTAPE3 = 6		
	NTAPE4 = 9		1030
	NTAPE5 = 3		1040
	NTAPE6 = 4		1050
	NTAPE7 = 11		
	NTAPE8 = 1		
	NTAPE9 = 10		1080
	MAXR = 50		1090
	MAXQ = 6		1100
	NCON = 0		
	MAXS = 50		1110
991	REWIND	NTAPE4	1120
	REWIND	NTAPE5	1130
	REWIND	NTAPE6	1140
	REWIND	NTAPE9	1150
	SORCON =	SQRT(386.0) / (2.0*3.14159)	1160
	EPSP =	.5E-06	1170
	FPDP =	.5E-07	1180
	AITKEN =	.9	1190
	AITKED =	.9	1200
	PICON =	.5921*2.0*3.14159	1210
	NCARDS =	0	1220
	NVFI =	0	1230
	NC =	1	1240
	NITRSP =	40	1250
	NITRDP =	100	1260
	RHO(1) =	0.0	1270
C.....			
C	READ	IN TITLE, CONTROLS AND CONSTANTS AND PRINT.	1280
	100	CALL RDIN (NTAPE2,NTAPE3,1)	1290
		READ (NTAPE2,1)NSUR, NAERO, NRIGID, NFUS, NDENS, MODES	1300
		INDFIM, NPUNCH, NCON	1310
		READ (NTAPE2,2)FK	1320
		WRITE (NTAPE3,3)NSUR,NAERO, NRIGID,NFUS, NDENS,MODES	1330
	1	, INDFIM, NPUNCH	1340
		NR2=NRIGID*NC	1350
		NSURFS=NSUR+NFUS	1360
		IF (NCON) 102,104,102	1370
	102	READ (NTAPE2,22)EPSP,FPDP,AITKEN, NITRSP,NITRDP	1380
			1390

```

READ (NTAPE2,2)AITKEN 1400
WRITE (NTAPE3,23)EPSP, EPDP, AITKEN, NITRSP, NITROP 1410
104 IF ( NAERO ) 105,103,105 1420
103 WRITE (NTAPE3,28)FK 1430
GOTO 111 1440
105 READ (NTAPE2,1)(ISXST(I), ISW(I), I=1, NSUR) 1450
READ (NTAPE2,2)RREF, (VELCTY(I), I=1, NAERO) 1460
NC=2 1470
NR2= NRIGID *NC 1480
READ (NTAPE2,2)(BR(I), S(I), I=1, NSURFS) 1490
IF ( NDFNS ) 106,107,106 1500
106 READ (NTAPE2,2)(RHO(I), I=1, NDFNS) 1510
107 IF ( NFUS ) 108,109,108 1520
108 WRITE (NTAPE3,5)BR(I), S(I) 1530
109 WRITE (NTAPE3,4)RREF ,FK 1540
DO 110 I=1, NSUR 1550
J=I+NFUS 1560
110 WRITE (NTAPE3,6) I, BR(J), S(J) ,ISXST(I) 1570
***** 1580
C READ IN FUSE OF MASS CHARACTERISTICS 1590
111 IF ( NRIGID ) 112,117,112 1600
112 IF ( NDFLM ) 115,113,115 1610
113 DO 114 I=1, NRIGID 1620
DO 114 J=1, NRIGID 1630
114 DM(I, J)=0.0 1640
GOTO 117 1650
115 DO 116 I=1, NRIGID 1660
116 READ (NTAPE2,2)(DM(J, I), J=1, NRIGID) 1670
WRITE (NTAPE3,19) 1680
CALL MPRINT (DM, NRIGID, NRIGID, MAXQ, NTAPE3) 1690
***** 1700
C READ MASS MATRIX FOR EACH SURFACE, STORE SYSTEM MASS MATRIX ON NTAPE4 1710
117 K1=0 1720
WRITE (NTAPE3,10) 1730
DO 120 I=1, NSUR 1740
READ (NTAPE2,1)NSIZE 1750
READ (NTAPE2,1)(LOW(J), LHIGH(J), J=1, NSIZE) 1760
DO 119 J=1, NSIZE 1770
DO 118 K=1, NSIZE 1780
118 A(K, J)=0.0 1790
N1=LOW(J) 1800
N2=LHIGH(J) 1810
119 READ (NTAPE2,2)(A(N, J), N=N1, N2) 1820
WRITE (NTAPE4)NSIZE, NSIZE, ((A(N, J), N=1, NSIZE), J=1, NSIZE) 1830
WRITE (NTAPE3,11)I, NSIZE 1850
CALL MPRINT (A, NSIZE, NSIZE, MAXR, NTAPE4) 1860
NSIZES(I)=NSIZE 1870
120 K1=K1+NSIZE 1880
***** 1890
NPOINT = TOTAL NUMBER OF CONTROL POINTS ON ALL SURFACES. 1900
NPOINT=K1 1910
C READ IN RIGID BODY MODAL MATRIX FOR EACH SYSTEM. 1920
IF ( NFUS ) 121,123,121 1930
121 READ (NTAPE2,1)NSIZE 1940
DO 122 J=1, NRIGID 1950
122 READ (NTAPE2,2)(HR(I, J), I=1, NSIZE) 1960
WRITE (NTAPE3,18)NSIZE 1970
CALL MPRINT (HR, NSIZE, NRIGID, MAXS, NTAPE3) 1980
WRITE (NTAPE4)NSIZE, NRIGID, ((HR(I, J), I=1, NSIZE), J=1, NRIGID) 1990
123 IF ( NRIGID ) 124,128,124 2010
124 K1=1 2020

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WRITE (NTAPE3,12)
DO 126 ISUR=1,NSUR
  READ (NTAPE2,1)NSIZE
  K2=K1+NSIZE-1
  DO 125 J=1,NRIGID
125  READ (NTAPE2,2)(HR(I,J),I=K1,K2)
    WRITE (NTAPE3,13)ISUR,NSIZE
    CALL MPRINT (HR(K1,1),NSIZE,NRIGID,MAXS,NTAPE3)
126  K1=K1+NSIZE
  WRITE (NTAPE5)NPOINT, NRIGID, ((HR(N,J),N=1,NPOINT),I=1,
  1 NRIGID )
  IF ( K1-NPOINT-1) 127,128,127
127 WRITE (NTAPE3,11)K1, NPOINT
*****
READ IN FLXIBILITY MATRIX FOR EACH SURFACE, STORE ON NTAPES
128 K1=0
  WRITE (NTAPE3,14)
  DO 153 I=1,NSUR
  READ (NTAPE2,1)NSIZE, J, IFORM, IROWS
  CALL MREAD (A,NSIZE,NSIZE,IFORM,IROWS,0,1,F,MAXR,NTAPE2,NTAPE3)
  WRITE (NTAPE3,15)I,NSIZE
  CALL MPRINT (A,NSIZE,NSIZE,MAXR,NTAPE3)
  WRITE (NTAPE5)NSIZE, NSIZE, ((A(J,K),J=1,NSIZE),K=1,NSIZE)
153 K1=K1+NSIZE
  IF ( K1-NPOINT ) 158,164,158
158 WRITE (NTAPE3,11)K1, NPOINT
164 IF ( NAERO ) 166,165,166
165 NRHO=1
  DO 500 I=1,NRIGID
  DO 500 J=1,NRIGID
500 DQ(I,J)=0.0
  WRITE (NTAPE5)((DM(I,J),I=1,NRIGID),J=1,NRIGID)
  NC)=NC
  GOTO 215
C*****
C READ IN WEIGHTING MATRIX FOR EACH SURFACE.....STORE ON NTAPE6,
166 WRITE (NTAPE3,15)
  DO 178 I=1,NSUR
  IF ( ISW(I) ) 167,177,167
167 N1=ISYST(I)
  IF ( N1 ) 168,172,168
168 DO 170 J=1,N1
  DO 169 L=1,MAXR
  A(J,L)=0.0
169 A(L,J)=0.0
170 A(J,J)=1.0
  READ (NTAPE2,1)NXST, J, IFORM, IROW
  IF ( NXST ) 171,172,171
171 CALL MREAD (A,NXST,NXST,IFORM,IROW,0,1,F,MAXR,NTAPE2,NTAPE3)
172 K=N1+1
  READ (NTAPE2,1)NSIZE, NPART, IFORM, IROW
  IF ( IFORM ) 174,173,174
173 CALL MREAD (A(K,K),NSIZE,NSIZE,0,0,0,1,F,MAXR,NTAPE2,NTAPE3)
  K=K+NSIZE
  GOTO 176
174 DO 175 J=1,NPART
  READ (NTAPE2,1)NSIZE
  N=K+NC
  DO 1741 L=K,N
  DO 1741 M=1,K
1741 A(M,L)=0.0

```

	CALL MREAD (A(K,K),NSIZE,NSIZE,1,IROW,0,0,F,MAXR,NTAPE2,NTAPE3)	2670
175	K=K+NSIZE	2680
176	K=K-1	2690
.....		
	WRITE (NTAPE3,1)I, K	2710
	CALL MPRINT (A,K,K,MAXR,NTAPE3)	2720
	WRITE (NTAPE6)K, K, ((A(J,L),J=1,K),L=1,K)	2730
	GOTO 178	2740
177	WRITE (NTAPE3,2)I	2750
178	CONTINUE	2760
179	REWIND NTAPE6	2770
	REWIND NTAPE7	2780
	NCX=NC	2790
	NVFL = NVEL+1	2800
.....		
	IF SERIES OF DENSITIES FOR EACH V/R OMEGA, READ IN THAT SERIES.	2810
	IF (NDFNS) 180,181,180	2820
180	NRHO=NDENS	2830
	GOTO 182	2840
181	READ (NTAPE2,1)NRHO	2850
	READ (NTAPE2,2)(RHO(I),I=1,NRHO)	2860
.....		
	READ IN COMPLEX AERODYNAMIC MATRIX FOR EACH SURFACE	2870
182	DO 210 I=1,NSURFS	2880
	K=1	2890
	K2=1	2900
	IF (NFUS) 183,184,183	2910
183	IF (I-1) 184,188,184	2920
184	L=I-NFUS	2930
	IF (ISXST(L)) 185,188,185	2940
185	K=ISXST(L)+1	2950
	K2 = K+ISXST(L)	2960
	DO 186 J=1,K	2970
	DO 186 L=1,K2	2980
186	A(J,L)=0.0	2990
	READ (NTAPE2,1)NXST, J, IFORM, IROW	3000
	IF (NXST) 187,188,187	3010
187	N= NXST *NC	3020
	CALL MREAD (A,NXST,N,IFORM,IROW,0,1,U,MAXR,NTAPE2,NTAPE3)	3030
188	READ (NTAPE2,2)VFLC	3040
	READ (NTAPE2,1)NSIZE, NPART, IFORM, IROW	3050
	IF (IFORM) 190,189,190	3060
189	N= NSIZE *NC	3070
	CALL MREAD (A(K,K2),NSIZE,N,IFORM,IROW,0,1,U,MAXR,NTAPE2,NTAPE3)	3080
	NSIZEF=NSIZE+K-1	3090
	GOTO 193	3100
190	DO 192 J=1,NPART	3110
	READ (NTAPE2,1)NSIZE	3120
	N=K2+NC	3130
	DO 191 M=K2,N	3140
	DO 191 I=1,K	3150
191	A(I,M)=0.0	3160
	N= NSIZEF *NC	3170
	CALL MREAD (A(K,K2),NSIZE,N,IFORM,IROW,0,0,U,MAXR,NTAPE2,NTAPE3)	3180
	K=K+NSIZEF	3190
192	K2=K2+N	3200
	NSIZEF=K-1	3210
	N=K2-1	3220
193	IF (I-1) 199,194,190	3230
194	IF (NFUS) 195,197,195	3240
195	WRITE (NTAPE3,1)NSIZE	3250
		3260
		3270

CALL MPRINT (A,NSIZE,N,MAXR,NTAPE3)	3280
C*****	3290
C COMPUTE (DQ) = (HR)T * (CH) * (HR)	3300
K1=)	3310
K2=)	3320
M=NC-1	3330
READ (NTAPE4)NSIZE, L, ((U(L,J),L=1,NSIZE),J=1,NRIGID)	3340
CALL MMULTD (A,M,U,0,F,NSIZE,NSIZE,NRIGID,MAXR,MAXR,MAXR)	3350
DO 196 L=1,NSIZE	3360
DO 196 J=1,NRIGID	3370
196 A(J,L)=U(L,J)	3380
CALL MMULTD (A,0,F,M,DQ,NRIGID,NSIZE,NRIGID,MAXR,MAXR,MAXR)	3390
GOTO 210	3400
197 DO 198 L=1,NRIGID	3410
DO 198 J=1,NR2	3420
198 DQ(L,J)=0.0	3430
199 I=I-NFUS	3440
IF (ISW(L)) 202,200,202	3450
200 WRITE (NTAPE7)NSIZE, N, ((A(J,M),J=1,NSIZE),M=1,N)	3460
GOTO 208	3470
202 READ (NTAPE6)I, L, ((F(J,M),J=1,L),M=1,L)	3480
IF (NSIZE-L) 204,206,204	3490
204 WRITE (NTAPE3,11)NSIZE,L	3500
206 CALL MMULTD (F,0,A,NC-1,U,L,L,L,MAXR,MAXR,MAXR)	3510
WRITE (NTAPE7)NSIZE, N, ((U(J,M),J=1,NSIZE),M=1,N)	3520
208 WRITE (NTAPE3,17)VELC	3530
L=I-NFUS	3540
WRITE (NTAPE3,13)L, NSIZE	3550
CALL MPRINT (A,NSIZE,N,MAXR,NTAPE3)	3560
210 CONTINUE	3570
C*****	3580
C CARRY ON FROM HERE TO END ONCE FOR EACH DENSITY.	3590
215 DO 300 IRHO=1,NRHO	3600
K=NC*NPOINT	3610
DO 216 I=1,NPOINT	3620
DO 216 J=1,K	3630
216 U(I,J)=0.0	3640
REWIND NTAPE4	3650
REWIND NTAPE5	3660
REWIND NTAPE7	3670
CON=RHO(IRHO)*RR(1)**2*S(1) *32.174	3680
IF (NRIGID) 218,222,218	3690
218 DO 220 I=1,NRIGID	3700
DO 220 J=1,NR2*NCX	3710
DMBAR(I,J+1)=CON*DQ(I,J+1)	3720
K=J/NC+NC-1	3730
220 DMBAR(I,J)=DM(I,K)+CON*DQ(I,J)	3740
C*****	3750
C READ ENTIRE HR MATRIX.	3760
READ (NTAPE5)I, I, ((HR(I,J),I=1,NPOINT),J=1,NRIGID)	3770
222 K1=0	3780
DO 246 ISUR=1,NSUR	3790
K=ISUR+NFUS	3800
CON=RHO(IRHO)*RR(K)**2*S(K) *32.174	3810
C*****	3820
C READ (M) I	3830
READ (NTAPE4)NSIZE, NSIZE, ((F(I,J),I=1,NSIZE), I=1,NSIZE)	3840
IF (NAFRO) 221,221,223	3850
221 DO 226 I=1,NSIZE	3860
DO 226 J=1,NSIZE	3870
226 A(I,J)=F(I,J)	3880
	3890
	3900

```

      I=NSIZE
      GOTO 231
C*****
C      READ (W)*(CH) I
227 READ (NTAPE7)NSIZE, L, ((A(I,J),I=1,NSIZE),J=1,L)
C*****
C      COMPUTE (M BAR) = ((H)+RHO*RR**2*S*(W)*(CH) ) I
      DO 228 I=J,NSIZE
      DO 228 J=1,L,NCX
      K=J/2+1
      A(I,J)=CON*A(I,J)+F(I,K)
228 A(I,J+1)=CON*A(I,J+1)
C*****
C READ FIFXIBILITY MATRIX FOR SURFACE
231 READ (NTAPE5)NSIZE, NSIZE, ((F(I,J),I=1,NSIZE),J=1,NSIZE)
      K=NC*K1+1
      CALL MMULTD (F,0,A,NC-1,U(K1+1,K),NSIZE,NSIZE,NSIZE,MAXR,MAXR,
1          MAXR)
      IF (NRIGID) 232,246,232
C*****
C FIND (LITTLE M BAR) = (DELTA M) + (H R)TRANPOSED * (M BAR) * (H R)
232 DO 240 I=1,NSIZE
      K=K1+1
      DO 240 J=1,NRIGID
240 G(J,I)=HR(K,J)
      K=NC*K1+1
      CALL MMULTD (G,0,A,NC-1,HRT(1,K),NRIGID,NSIZE,NSIZE,MAXU,MAXR,
1          MAXU)
      CALL MMULTD (HRT(1,K),NC-1,HR(K1+1,1),0,A,NRIGID,NSIZE,NRIGID,
1          MAXU,MAXS,MAXR)
      DO 244 I=1,NRIGID
      DO 244 J=1,NR2
244 BARMRR(I,J)=BARMRR(I,J)+A(I,J)
246 K1=K1+NSIZE
      L=NC*NPOINT
      IF (NRIGID) 247,268,247
247 GOTO (252,248),NC
248 DO 250 I=1,NRIGID
      DO 250 J=1,NR2,NCX
      K=J/2+1
      G(I,K)=BARMRR(I,J+1)
250 BARMRR(I,K)=BARMRR(I,J)
C*****
C THEN (LITTLE M BAR) INVERSE AND FINAL U MATRIX STORED ON TAPE9.
252 CALL MNVRSX (BARMRR,0,A(1,1),A(1,MAXQ),NRIGID,IR,NC-1)
      IF (IR) 310,254,310
254 GOTO (260,256),NCX
256 DO 258 I=1,NRIGID
      DO 258 J=1,NR2,NCX
      K=NR2-J
      M=K/2+1
      BARMRR(I,K)=BARMRR(I,M)
258 BARMRR(I,K+1)=G(I,M)
260 CALL MMULTD (BARMRR,NC-1,HRT,NC-1,F,NRIGID,NRIGID,POINT,
1          MAXQ,MAXQ,MAXR)
      CALL MMULTD (F,NC-1,U,NC-1,HRT,NRIGID,NPOINT,NPOINT,MAXR,MAXR,
1          MAXQ)
      CALL MMULTD (HR,1,F,NC-1,A,NPOINT,NRIGID,NPOINT,MAXQ,MAXR,MAXR)
      DO 264 I=1,NPOINT
      DO 262 J=1,I
      F(I,J)=U(I,J)

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262	A(I,J)=-A(I,J)	4500
	K=I*NC-NC+1	4510
264	A(I,K)=1.0+A(I,K)	4520
	CALL MMULTD (A,NC-1,F,NC-1,U,NPOINT,NPOINT,NPOINT,MAXR,MAXR,MAXR)	4530
	IF (NAERO) 268,266,268	4540
266	READ (NTAPE5)A(1,1)	4550
	WRITE (NTAPE5)((HRT(I,J),I=1,NRIGID),J=1,NPOINT)	4560
268	WRITE (NTAPE9)NPOINT, L, ((U(I,J),I=1,NPOINT),J=1,L)	4580
300	CONTINUE	4600
	REWIND NTAPE5	4610
	REWIND NTAPE6	4620
	REWIND NTAPE7	4630
	REWIND NTAPE8	4640
	REWIND NTAPE9	4650
	KPART = 2	4660
	RETURN	4670
310	WRITE (NTAPE3,20)	4680
	GOTO 991	4690
320	REWIND NTAPE4	4700
	REWIND NTAPE5	4710
	IF (NRIGID) 330,332,330	4720
330	READ (NTAPE5)I,I, A(I,J)	4730
332	K1=1	4740
	DO 334 I=1,NPOINT	4750
	DO 334 J=1,NPOINT	4760
334	F(I,J)=0.0	4770
	DO 336 ISUR=1,NSUR	4780
	K2=K1+NSIZES(ISUR)-1	4790
	READ (NTAPE5)I,I, A(I,1)	4800
	READ (NTAPE4)NSIZE, NSIZE, ((F(I,J),I=K1,K2),J=K1,K2)	4810
336	K1=K1+NSIZE	4820
	READ (NTAPE4)NSIZE, MODE, ((A(I,J),I=1,NSIZE),J=1,MODE)	4830
	M=MODE/NC	4840
	CALL MMULTD (F,0,A,NC-1,U,NPOINT,NPOINT,M,MAXR,MAXR,MAXR)	4850
	IF (NDELM) 337,348,337	4860
337	IF (NRIGID) 338,348,338	4870
338	READ (NTAPE5)((DM(I,J),I=1,NRIGID),J=1,NRIGID)	4880
	READ (NTAPE5)((G(I,J),I=1,NRIGID),J=1,NPOINT)	4890
	DO 339 I=1,NRIGID	4900
	DO 339 J=1,NPOINT	4910
339	G(I,J)=-G(I,J)	4920
	CALL MMULTD (G,0,A,0,HRT,NRIGID,NPOINT,M,MAXQ,MAXR,MAXQ)	4930
	READ (NTAPE4) (HR(I,1),I=1,M)	4940
	DO 340 I=1,M	4950
	DO 340 J=1,NRIGID	4960
340	G(J,I) = HRT(J,I)/HR(I,1)	4970
	WRITE (NTAPE3,25)	4980
	CALL MPRINT (G,NRIGID,M,MAXQ,NTAPE3)	4990
	IF (NPUNCH) 343,345,343	5000
343	WRITE (NTAPE0,26)NRIGID, M, RCDZ, NCARDS	5010
	NCARD = NCARDS+1	5020
	CALL MPUNCH (G,NRIGID,M,0,1,1,RCDZ,MAXQ,NTAPE0,NCARD)	5030
	WRITE (NTAPE3,27)RCDZ, NCARDS, RCDZ, NCARD	5040
	NCARDS=NCARD+1	5050
345	CONTINUE	5060
	CALL MMULTD (DM,0,G,0,HRT,NRIGID,NRIGID,M,MAXQ,MAXQ,MAXQ)	5070
	DO 346 I=1,NRIGID	5080
	DO 346 J=1,MODE	5090
346	HR(J,I) = G(I,J)	5100
348	DO 350 I=1,NPOINT	5110
	DO 350 J=1,MODE	5120
		5130
		5140

350	F(J,I)=A(I,J)	5150
	CALL MMULTD (F,N,U,N,A,M,NPCINT,M,MAXR,MAXR,MAXR)	5160
	IF (NDELM) 352,358,352	5170
352	IF (NRRIGID) 354,358,354	5180
354	CALL MMULTD (HR,N,HRT,N,F,M,NRRIGID,M,MAXR,MAXO,MAXR)	5190
	DO 356 I=1,MODF	5200
	DO 356 J=1,M	5210
356	A(J,I) = A(J,I) + F(J,I)	5220
358	WRITE (NTAPE3,24) (I, A(I,I),I=1,M)	5230
	GOTO 991	5240
	END	5260
	FORTRAN LST00,DECK	
MREAD		
MREAD		
	MATRIX READ SUBROUTINE	
	CALL MREAD (A,M,N,IFORM,IROW,ITRA,IORG,T,MD,NTAPE2,NTAPE3)	M0010
		M0020
		M0030
		M0040
	A = MATRIX TO READ IN	M0050
	M = NUMBER OF ROWS	M0060
	N = NUMBER OF COLUMNS	M0070
	IFORM = -1, FORMAT(12A6)	M0080
	= 0, COLUMN BINARY	M0090
	= +1, FORMAT(6E12.8)	M0100
	IROW = .0, MATRIX BY COLUMNS	M0110
	= +1, MATRIX BY ROWS	M0120
	ITRA = 0, TRA CARD AFTER MATRIX	M0130
	= +1, TRA CARD AFTER EACH ROW	M0140
	(OR COLUMN)	M0150
	IORG = ORIGIN OF FIRST C.B. CARD	M0170
	T = MDXN TEMPORARY CELLS	M0180
	MD = DIMENSIONED NUMBER OF ROWS	M0190
	IN A	M0195
	NTAPE2 = INPUT TAPE	M0200
	NTAPE3 = OUTPUT TAPE	M0210
		M0220
		M0230
		M0240
		M0250
		M0260
		M0270
		M0280
		M0290
		M0300
		M0310
		M0320
		M0330
		M0340
		M0350
		M0360
		M0370
		M0380
		M0390
		M0400
		M0402
		M0404
		M0406
		M0410
		M0415
		M0420
		M0430
		M0440

```

SUBROUTINE MREAD (A,M,N,IFORM,IROW,ITRA,IORG,T,MD,NTAPE2,NTAPE3 )
DIMENSION A(1), T(1)
1 FORMAT (6E12.8)
2 FORMAT (12A6)
3 FORMAT ( // 26H THATS ALL YOUR DATA. )
4 FORMAT (4E16.8)
MN=MD*N
DO 5 I=1,MN
T(I)=0.0
5 A(I)=0.0
IF ( IFORM ) 39,15,6
6 IF ( IROW ) 8,7,8
7 K3=1
K4=N
K5=MD
K6=M-1
K2=1
GOTO 9
8 K2=MN
K3=MD
K4=M
K5=1
K6=0
9 DO 11 L=1,K4
K1=1*K5-K5+1
IF (K6) 10,11,10
10 K2=K1+K6
11 IF (IFORM = 1) 34,110,109
109 READ (NTAPE2,4) (A(L),L=K1,K2,K3)
GO TO 11
110 READ (NTAPE2,1)(A(L),L=K1,K2,K3)
11 CONTINUE
GOTO 36
15 K1=N
K2=M

```

```

      K3=1
      IF ( IORG-1 ) 16,17,17
16  K3=2
17  IF ( IROW ) 18,19,18
18  K2=N
      K1=M
19  IF ( ITRA ) 22,21,22
21  K1=1
22  K=0
      DO 23 I=1,K1
          K4=K+K3
          K5=1
          CALL RINRD ( T(K4), K5, L, NTAPE2, NTAPE3 )
          GOTO (23,38,23,23),1
23  K=K+K2
      IF ( IROW ) 28,24,28
24  L=0
      IF ( IORG-1 ) 26,26,25
25  L=IORG-1
26  DO 27 I=1,N
          J=I*MD-MD
          DO 27 K=1,M
              J=J+1
          L=L+1
27  A(J)=T(L)
          GOTO 36
28  L=0
      IF ( IORG-1 ) 30,30,29
29  L=IORG-1
30  DO 31 K=1,N
          J= K*MD-MD
          DO 31 I=K,MN,N
              J=J+1
              K1=L+1
31  A(J)=T(K1)
36  RETURN
38  WRITE (NTAPE3,3)
      STOP
39  READ (NTAPE2,2)(A(I),I=1,M)
      GOTO 36
      END

```

5 FORTRAN LSI00.DECK

```

C RINRD
  SURROUTINE RINRD ( T,K,L,NTAPE1,NTAPE2 )
  DIMENSION T(1)
  RETURN
  END

```

5 FORTRAN LSI00.DECK

```

C RDLN
  SURROUTINE RDLN ( NTAPE2, NTAPE3, I )
  1 FORMAT(80H
  1
  2 FORMAT(1H1)
  3 FORMAT ( 1H0 )
  READ (NTAPE2,1)
  GOTO (4,5),1
  4 WRITE (NTAPE3,2)
  GOTO 6
  5 WRITE (NTAPE3,3)
  6 WRITE (NTAPE3,1)
  RETURN

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M0450
M0460
M0470
M0480
M0490
M0500
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M0580
M0590
M0600
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M0670
M0680
M0690
M0700
M0710
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M0790
M0800
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0010
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0030
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0010
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0050
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	END	0130
	FORTRAN LST00.DECK	
C	MMULTD	
	SUBROUTINE MMULTD (A,N1,B,N2,C,M,N,K,MA,MB,MC)	0010
	DIMENSION A(1), B(1), C(1)	0020
	IC=1	0040
	IA=MC*K	0050
	IB=MA*N	0060
	ID=MA	0070
	IH=MC	0080
	IJ=MC	0090
	IF (N1) 4,5,4	0100
3	IF (N2) 7,8,7	0110
4	IB=2*IB	0120
	ID=2*ID	0130
	IF (N2) 5,6,5	0140
5	IC=2	0150
	GOTO 7	0160
6	IH=2*IH	0170
	IC=3	0180
7	IA=2*IA	0190
	IJ=2*IJ	0200
8	DO 18 I=1,M	0210
	INC=0	0220
	DO 11 J=1,IA,IH	0230
	C(J)=0.0	0240
	IN=INC	0250
	DO 10 L=1,IB,ID	0260
	IN=IN+1	0270
10	C(J)=C(J)+A(L)*R(IN)	0280
11	INC=INC+MB	0290
	INC=0	0300
	GOTO (18,12,15),IC	0310
12	DO 14 J=1,IA,IJ	0320
	IF=I+MA	0330
	IF=J+MC	0340
	IN=INC	0350
	DO 13 L=1,IB,ID	0360
	IN=IN+1	0370
	IG=IN+MB	0380
	C(IF)=C(IF)+A(L)*R(IN)	0390
13	C(J)=C(J)-A(L)*R(IG)	0400
14	INC=INC+MR	0410
	GOTO 18	0420
15	IF=I+MC	0430
	IF=I+MA	0440
	DO 17 J=IF,IA,IJ	0450
	IN=INC	0460
	C(J)=0.0	0470
	DO 16 L=1,IB,ID	0480
	IN=IN+1	0490
16	C(J)=C(J)+A(L)*R(IN)	0500
17	INC=INC+MR	0510
18	CONTINUE	0520
	RETURN	0530
	END	0540
	FORTRAN LST00.DECK	
C	MNVSX	
	SUBROUTINE MNVSX (AR,AI,R,C,KSZ,IGOOD,NOP)	0010
	DIMENSION AR(6,6), AI(6,6), R(6,6), C(6,6)	0020
	IGOOD=0	0040

IF (NOP) 10,101,102	0050
101 CALL INVERS (AR,KSZ,IGOJFD)	0060
GO TO 20	0070
102 CONTINUE	0080
DO 1 K=1,KSZ	0090
DO 1 L=1,KSZ	0100
1 R(K,L)=AR(K,L)	0110
NO=0	0120
CALL INVERS(R,KSZ,NO)	0130
IF (NO) 2,3,2	0140
C REAL MATRIX NOT SINGULAR	0150
C MULT R*AI STO. C	0160
3 DO 4 K=1,KSZ	0170
DO 4 L=1,KSZ	0180
C(K,L)=0.0	0190
DO 4 I=1,KSZ	0200
4 C(K,L)=C(K,L)+R(K,I)*AI(I,L)	0210
C MULT. AI*C + AR STO. B	0220
DO 5 K=1,KSZ	0230
DO 5 L=1,KSZ	0240
R(K,L)=AR(K,L)	0250
DO 5 I=1,KSZ	0260
5 R(K,L)=R(K,L)+AI(K,I)*C(I,L)	0270
NO=0	0280
CALL INVERS(R,KSZ,NO)	0290
IF (NO) 2,7,2	0300
C SECOND MATRIX NOT SINGULAR	0310
C MULT. -C*B STO. AI ALSO SET AR=B	0320
7 DO 8 K=1,KSZ	0330
DO 8 L=1,KSZ	0340
AI(K,L)=0.0	0350
AR(K,L)=B(K,L)	0360
DO 8 I=1,KSZ	0370
8 AI(K,L)=AI(K,L)-C(K,I)*B(I,L)	0380
GO TO 20	0390
C REAL MATRIX OR SECOND MATRIX SINGULAR TRY IMAG. ROUTE	0400
9 DO 9 K=1,KSZ	0410
DO 9 L=1,KSZ	0420
R(K,L)=AI(K,L)	0430
NO=0	0440
CALL INVERS(R,KSZ,NO)	0450
IF (NO) 10,11,10	0460
C IMAG. NOT SINGULAR	0470
C MULT. R*AR STO. C	0480
11 DO 12 K=1,KSZ	0490
DO 12 L=1,KSZ	0500
C(K,L)=0.0	0510
DO 12 I=1,KSZ	0520
12 C(K,L)=C(K,L)+R(K,I)*AR(I,L)	0530
C MULT. AR*C+AI STO B	0540
DO 13 K=1,KSZ	0550
DO 13 L=1,KSZ	0560
R(K,L)=AI(K,L)	0570
DO 13 I=1,KSZ	0580
13 R(K,L)=R(K,L)+AR(K,I)*C(I,L)	0590
NO=0	0600
CALL INVERS(R,KSZ,NO)	0610
IF (NO) 10,15,10	0620
C THIRD MATRIX NOT SINGULAR	0630
C MULT -L*B STO AR ALSO SET AI=-R	0640
15 DO 16 K=1,KSZ	0650

	DO 16 I=1,KSZ	0660
	AR(K,L)=0	0670
	AI(K,L)=-R(K,L)	0680
	DO 16 I=1,KSZ	0690
16	AR(K,L)=AR(K,I)+C(K,I)*R(I,L)	0700
	GO TO 20	0710
10	I GOOD D=1	0720
20	RETURN	0730
	END	0740
	FORTRAN LISTING DECK	
	INVERS	
	SUBROUTINE INVERS (A,N,I GOOD D)	0010
	DIMENSION A(6,6), L(6), M(6)	0020
	CALL OVERFI(K000FX)	0040
	GO TO(500,500),K000FX	0050
500	CALL OVERFL(K000FX)	0060
	GO TO(501,501),K000FX	0070
501	CALL DVCHK (K000FX)	0080
	GO TO(502,502),K000FX	0090
502	IGOOD=0	0100
	SEARCH FOR LARGEST ELEMENT	0110
	DO 20 K=1,N	0120
	L(K)=K	0130
	M(K)=K	0140
	RIGA=A(K,K)	0150
	DO 20 I=K,N	0160
	DO 20 J=K,N	0170
	IF(ABS(RIGA)-ABS(A(I,J)))L0,20,20	0180
10	RIGA=A(I,J)	0190
	L(K)=I	0200
	M(K)=J	0210
20	CONTINUE	0220
	INTERCHANGE ROWS	0230
	JROW=L(K)	0240
	IF(L(K)-K)35,35,25	0250
25	DO 30 I=1,N	0260
	HOLD=-A(K,I)	0270
	A(K,I)=A(JROW,I)	0280
30	A(JROW,I)=HOLD	0290
	INTERCHANGE COLUMNS	0300
35	ICOL=M(K)	0310
	IF(M(K)-K)45,45,37	0320
37	DO 40 J=1,N	0330
	HOLD=-A(J,K)	0340
	A(J,K)=A(J,ICOL)	0350
40	A(J,ICOL)=HOLD	0360
	DIVIDE COLUMN BY MINUS PIVOT	0370
45	DO 45 IC=1,N	0380
46	IF(IC-K)50,55,50	0390
50	A(IC,K)=A(IC,K)/(-A(K,K))	0400
55	CONTINUE	0410
	REDUCE MATRIX	0420
	DO 65 I=1,N	0430
	DO 65 J=1,N	0440
56	IF(I-K)57,65,57	0450
57	IF(J-K)60,65,60	0460
60	A(I,J)=A(I,K)*A(K,J)+A(I,J)	0470
65	CONTINUE	0480
	DIVIDE ROW BY PIVOT	0490
	DO 75 JR=1,N	0500
68	IF(JR-K)70,75,70	0510

77	A(K, JR)=A(K, JR)/A(K, K)	0520
75	CONTINUE	0530
C	CONTINUED PRODUCT OF PIVOTS	0540
C	REPLACE PIVOT BY RECIPROCAL	0550
	A(K, K)=1.0/A(K, K)	0560
C	CONTINUE COMPLETE OPERATION	0570
80	CONTINUE	0580
	CALL DVCHK (K000FX)	0590
	GO TO(510, 503), K000FX	0600
503	CALL OVERFL(K000FX)	0610
	GO TO(510, 504), K000FX	0620
504	CALL OVERFL(K000FX)	0630
	GO TO(510, 505), K000FX	0640
C	FINAL ROW AND COLUMN INTERCHANGE	0650
505	K=N	0660
100	K=(K-1)	0670
	IF(K)150, 150, 103	0680
101	I=I(K)	0690
	IF(I-K)120, 120, 107	0700
105	DO 110 J=1, N	0710
	HOLD=A(J, K)	0720
	A(J, K)=-A(J, I)	0730
110	A(J, I)=HOLD	0740
120	J=M(K)	0750
	IF(J-K)100, 100, 125	0760
125	DO 130 I=1, N	0770
	HOLD=A(K, I)	0780
	A(K, I)=-A(J, I)	0790
130	A(J, I)=HOLD	0800
	GO TO 100	0810
150	RETURN	0820
510	I GOOF D=1	0830
	GO TO 150	0840
	END	0850
*	LINK PAR2TT, PAR1TT	
*	FORTAN LST00, DFCK	
C	PART2	
	SUBROUTINE PART2	0010
C	PART2.....2 VIBRATION AND FLUTTER ANALYSIS BY A COLLOCATION METHOD.	0020
	DIMENSION IT(219), VELCTY(20), NSIZES(20), DM(6, 6), RHO(20)	
	COMMON/11/ U(49, 196), GUFSS(49, 2), H(49, 50), EIG(50),	
1	TEMP(2734), NAKSR(25), NAKDR(25), NITER(75),	0040
2	OMEGA(25), DAMP(25), VELC(25)	
C	THE FOLLOWING STATEMENT(S) HAVE BEEN MANUFACTURED BY THE TRANSLATOR TO	0070
C	COMPENSATE FOR THE FACT THAT EQUIVALENCE DOES NOT REORDER COMMON---	0080
	COMMON IT	0090
	EQUIVALENCE (IT(1), ISXST), (IT(21), ISW), (IT(41), RHO),	0150
1	(IT(61), NTAPE1), (IT(62), NTAPE2), (IT(63), NTAPE3),	0160
2	(IT(64), NTAPE4), (IT(65), NTAPE5), (IT(66), NTAPE6),	0170
3	(IT(67), NTAPE7), (IT(68), NTAPE8), (IT(69), NTAPE9),	0180
4	(IT(70), NSUR), (IT(71), NRIOID), (IT(72), HREF),	0190
5	(IT(73), NAFRO), (IT(74), NFUS), (IT(75), NDENS),	0200
6	(IT(76), MODES), (IT(77), NPOINT), (IT(78), NPUNCH),	0210
7	(IT(79), MAXR), (IT(80), MAXQ), (IT(81), MAXS),	0220
8	(IT(82), NC), (IT(83), NSURFS), (IT(84), NP2),	0230
9	(IT(85), HR), (IT(106), S)	0240
	EQUIVALENCE (IT(127), VELCTY), (IT(147), NTAPE0), (IT(148), NRHO),	0250
1	(IT(149), NITRSP), (IT(150), NITRDP), (IT(151), EPSP),	0260
2	(IT(152), FPDP), (IT(153), PICON), (IT(154), NVEL),	0270
3	(IT(155), NCARDS), (IT(156), AITKEN), (IT(157), NGO),	0280
4	(IT(158), FK), (IT(159), SORCON), (IT(160), NSIZES),	0290

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6          (IT(180),DM),(IT(217),AITKD), (IT(218),KPART)          031
200 FORMAT (1H: 48X, 12H OUTPUT DATA /// 1H 11X, 5H FLUTTER      0320
1          52H ANALYSIS BY A COLLOCATION METHOD, USING AERODYNAMIC    0330
2          24H INFLUENCE COEFFICIENTS // 1H0 14X, 11H DENSITY =    0340
3          1E20.0, 5X, 20H REDUCED VELOCITY = 1E20.0, // 1H0 33X,   0350
4          116. 32H RIGID BODY DEGREES OF FREEDOM ///// )          0360

201 FORMAT (1H1 20X, 5H MODE 7X, 12H OMEGA (CPS) 10X, 6H DAMPING    0370
1          4X, 17H VELOCITY (KNOTS) /// ( 1H 20X, 114,            0380
2          3E20.0) )          0390
202 FORMAT ( 214, 62X, 1A6, 114 )          0400
203 FORMAT ( 1H0 33X, 23H PUNCHED CARDS NUMBERS 1A6, 114, 6H THRU  0410
1          1A6, 114 )          0420
204 FORMAT (1H1 45X, 16H DYNAMIC MATRIX )          0430
205 FORMAT (31H FLEXIBLE MODE SHAPES, SURFACE 114 )          0440
206 FORMAT (5H MODE 116, 32H, GIVES AN IMAGINARY FREQUENCY. )      0450
DATA Q000CT/02020.30440005/
RCDZ =Q000CT          0470
NVFL=NVEL          0480
MAXP=49          0490
K=NC*NPOINT          0500
DO 290 I=1,NPOINT          0510
DO 290 J=1,K          0520
290 U(I,J)=0.0          0530
REWIND NTAPE0          0540
DO 314 IRHO=1,NRHO          0550
MODE=MODES          0560
READ (NTAPE0)NSIZE, NSIZE?, ((U(I,J),I=1,NSIZE),          0570
1          J=1,NSIZE?)          0580
IF ( NPUNCH )          302,304,304          0590
302 WRITE (NTAPE1,204)          0600
CALL MPRINT (U,NPOINT,K,MAXP,NTAPE3)          0610
304 WRITE (NTAPE3,200)RHO(IRHO), VELCTY(NVEL), NRIGID          0620
DO 305 I=1,MODE          0630
NAKDR(I)=0          0640
305 NAKSR(I)=0          0650
CALL MITERS (U,GUESS ,0 ,NPOINT,MODE ,MAXP ,NC ,EPSP ,          0660
1          FPOP ,NAKSR ,NAKDR ,NITRSP,NITRDP,AITKE0,AITKD,          0670
2          IR ,TEMP ,H ,EIG ,MITER ,NTAPE0,NTAPE3)          0680
IF ( NAERO )          3055,3054,3055          0690
3054 WRITE (NTAPE4) NPOINT, MODE, ((H(I,J),I=1,NPOINT),J=1,MODE)    0700
WRITE (NTAPE4) (EIG(I),I=1,MODE),NPOINT,MODE,NPOINT,MODE,MODE      0710
3055 CONTINUE          0720
MODES2 = NC*MODE          0730
DO 310 I=1,MODES2,NC          0740
K=I/NC +NC -1          0750
I' (EIG(I))          3051,3052,3052          0760
3051 WRITE (NTAPE1,206)K          0770
OMEGA(K)=0.0          0780
GOTO 3053          0790
3052 OMEGA(K)= SURCON / ( SORT( FK*EIG(I)) )          0800
3053 GOTO (306,308),NC          0810
306 DAMP(K)=0.0          0820
VELC(K)=0.0          0830
GOTO 310          0840
308 DAMP(K)= EIG(I+1) / EIG(I)          0850
VELC(K)= PICON*OMEGA(K)*RREF* VELCTY(NVEL)          0860
310 CONTINUE          0870
WRITE (NTAPE1,201)(K, OMEGA(K), DAMP(K), VELC(K) ,          0880
1          K=1,MODE )          0890
IF ( NPUNCH )          312,314,312          0900

```

312	K1=1	0910
	WRITE (NTAPE0,202)NSIZES(1), MODES2, BCDZ, NCARDS	0920
	NCRDS = NCARDS+1	0930
	CALL MPUNCH (OMEGA,MODES2,1,0,1,1,BCDZ,MAXP,NTAPE0,NCRDS)	0940
	WRITE (NTAPE1,203)BCDZ, NCARDS, BCDZ, NCRDS	0950
	NCARDS=NCARDS+1	0960
	DO 313 ISUR =1,NSUR	0970
	IF (ISUR=1) 3121,3122,3121	0980
3121	WRITE (NTAPE0,202)NSIZES(ISUR), MODES2,BCDZ-NCARDS	0990
	NCRDS=NCARDS+1	1000
	GO TO 3123	1010
3122	NCRDS=NCARDS	1020
3123	CALL MPUNCH (H(K1,1),NSIZES(ISUR),MODES2,0,1,1,BCDZ,MAXP,NTAPE0,	1030
	1 NCRDS)	1040
	WRITE (NTAPE1,205)ISUR	1050
	WRITE (NTAPE1,203)BCDZ,NCARDS,BCDZ,NCRDS	1060
	NCARDS=NCARDS+1	1070
313	K1=K1+NSIZES(ISUR)	1080
314	CONTINUE	1090
	REWIND NTAPE0	1100
	NGO = 98765	1110
	KPART = 1	1120
	RETURN	1130
	END	1140
* TRAN LST00.DFCK		
C NORM7		
	SUBROUTINE NORM (A,H,N,C,INDEX,MAXR,NC,NP)	MTR40002
	DIMENSION A(1), H(1), C(1), T(2)	MTR40004
	IF (INDEX) 100,200,200	MTR40006
100	GO TO (110,140),NP	MTR40007
110	GO TO (500,120),NC	MTR40008
120	RIG = C(1)**2+C(2)**2	MTR40009
	GO TO 400	MTR40010
140	CALL DNORM (A,R,N,C,MAXR,NC,T)	MTR40012
	GO TO 700	MTR40013
200	INDEX=1	MTR40015
	NSTART=NP+1	MTR40016
	NSTOP=N*NP	MTR40017
	K=NP*MAXR	MTR40018
	IF (NSTART-NSTOP) 205,205,400	MTR40019
205	GO TO (20,300),NC	MTR40020
210	RIG=ABS A(1))	MTR40022
	DO 230 I=NSTART,NSTOP,NP	MTR40023
	IF (RIG-ABS(A(I))) 220,220,230	MTR40025
220	INDEX=I	MTR40026
	RIG=ABS(A(I))	MTR40027
230	CONTINUE	MTR40028
	GO TO 400	MTR40029
300	RIG = A(1)**2 + A(K+1)**2	MTR40031
	DO 330 I=NSTART,NSTOP,NP	MTR40032
	J=K+1	MTR40033
	IF (RIG-(A(I)**2+A(J)**2)) 320,320,330	MTR40034
320	RIG = A(I)**2 + A(J)**2	MTR40035
	INDEX = I	MTR40036
330	CONTINUE	MTR40038
400	J=NP*NC	MTR40040
	I=INDEX+(NC-1)*K+(NP-1)	MTR40041
	C(J)=A(I)	MTR40042
	J=J-(NP-1)	MTR40043
	I=I-(NP-1)	MTR40044
	C(J)=A(I)	MTR40045


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I=INDEX+(NP-1)
C(NP)=A(I)
C(1)=A(INDEX)
GO TO (410,140),NP
410 GO TO (500,600),NC
500 DO 510 I=1,N
510 R(I)=A(I)/C(1)
GO TO 700
600 BIG = C(1)**2+C(2)**2
DO 610 I=1,N
J=I+MAXR
T = A(I)*C(1)+A(J)*C(2)
R(J) = ( A(J)*C(1)-A(I)*C(2) ) / BIG
610 R(I) = T/BIG
700 INDEX = INDEX/NP + NP-1
RETURN
END

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MTR40046
MTR40047
MTR40048
MTR40050
MTR40051
MTR40053
MTR40054
MTR40055
MTR40057
MTR40058
MTR40060
MTR40061
MTR40062
MTR40063
MTR40064
MTR40065
MTR40067

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C
FORTRAN LISTING DECK

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DNORMZ

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SUBROUTINE DNORM (A,B,N,C,MAXR,NC,T)
DOUBLE PRECISION A(1), B(1),C(1),T(1)
410 GO TO (500,600),NC
500 DO 510 I=1,N
510 R(I)=A(I)/C(1)
GO TO 700
600 BIG=C(1)*C(1) + C(2)*C(2)
DO 610 I=1,N
J=I+MAXR
T = A(I)*C(1)+A(J)*C(2)
R(J) = ( A(J)*C(1)-A(I)*C(2) ) / BIG
610 R(I) = T/BIG
700 RETURN
END

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MTR40069
MTR40071
MTR40072
MTR40074
MTR40075
MTR40076
MTR40078
MTR40079
MTR40080
MTR40081
MTR40082
MTR40083
MTR40084
MTR40086

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C
FORTRAN LISTING DECK

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POHS

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SUBROUTINE POH (LMBDN,LMBD1,LMBD2,HN,HN1,H1,H2,N,NC)
DIMENSION LMBDN(1), LMBD1(1), LMBD2(1), HN(1), HN1(1), H1(1),
1 H2(1), A(2)
DOUBLE PRECISION LMBDN, LMBD1, LMBD2, HN, HN1, H1, H2, A
GO TO (200,100),NC
110 I=1,N
K=I+N
A(1) = LMBDN(1)*HN(I)-LMBDN(2)*HN(K)
A(2) = LMBDN(1)*HN(K)+LMBDN(2)*HN(I)
H1(I) = LMBD2(1)*HN1(I)-LMBD2(2)*HN1(K)-A(1)
H1(K) = LMBD2(1)*HN1(K)+LMBD2(2)*HN1(I)-A(2)
H2(I) = A(1)-LMBD1(1)*HN1(I)+LMBD1(2)*HN1(K)
110 H2(K) = A(2)-LMBD1(1)*HN1(K)-LMBD1(2)*HN1(I)
RETURN
200 DO 210 I=1,N
A(1) = LMBDN(1)*HN(I)
H1(I) = LMBD2(1)*HN1(I)-A(1)
210 H2(I) = A(1)-LMBD1(1)*HN1(I)
RETURN
END

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MTR40089
MTR40091
MTR40092
MTR40093
MTR40095
MTR40097
MTR40099
MTR40101
MTR40102
MTR40104
MTR40105
MTR40107
MTR40108
MTR40110
MTR40112
MTR40114
MTR40116
MTR40117
MTR40119
MTR40121

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C
FORTRAN LISTING DECK

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AITKNS

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SUBROUTINE AITKNS (HN,HN1,HN2,HNEW,R,N,MAXR,NC,NP,IR)
DIMENSION HN(1), HN1(1), HN2(1), HNEW(1), A(2), B(4), C(2), D(2)
IR=0
I=NP*N

```

MTR40123
MTR40125
MTR40127
MTR40129

```

C(1) = R**2
DO 110 I=1,I.NP
  D(1) = 0
  D(2) = 0
  DO 100 J=1,NC
    K=(J-1)*MAXR+1
    D(1) = D(1) + (HN1(K)-HN2(K))**2
100   D(2) = D(2) + (HN(K)-HN1(K))**2
    IF ( D(1) ) 105,110,105
105  CONTINUE
    IF (D(2)/D(1) - C(1)) 110,110,800
110  CONTINUE
GO TO (300,200),NP
200 CALL AITKND (HN,HN1,HN2,HNEW,N,MAXR,NC,A,B,C,D)
GO TO 700
300 DO 600 I=1,N
  GO TO (400,500),NC
400 C(1) = HN(I)-2.*HN1(I)+HN2(I)
  IF ( C(1) ) 410,600,410
410 HNEW(I) = HN2(I) - ( (HN1(I)-HN2(I))**2 / C(1) )
  GO TO 600
500 A(1) = 0.
  C(1) = 2.
  D(1) = 0.
  DO 510 J=1,2
    K = I+(J-1)*MAXR
    R(J) = HN(K)-2.*HN1(K)+HN2(K)
    C = C*(HN1(K)-HN2(K))
    A = -(HN1(K)-HN2(K))**2 - A
510   D = R(J)**2 + D
    IF ( D ) 520,600,520
520 HNEW(I) = HN2(I) - (R(1)*A(1)+R(2)*C(1))/ D(1)
    HNEW(K) = HN2(K) - (R(1)*C(1)+R(2)*A(1))/ D(1)
600 CONTINUE
710 IP = 1
900 RETURN
END
*
C AITKND
SUBROUTINE AITKND (HN,HN1,HN2,HNEW,N,MAXR,NC,A,B,C,D)
DIMENSION HN(1), HN1(1), HN2(1),HNEW(1), A(1), B(2) C(1), D(1)
DOUBLE PRECISION HN, HN1, HN2, HNEW, A, B, C, D
300 DO 600 I=1,N
  GO TO (400,500),NC
400 C(1) = HN(I)-2.*HN1(I)+HN2(I)
  IF ( ABS(C(1)) - .0000000000 ) 410,600,410
410 HNEW(I)=HN2(I) - ( (HN1(I)-HN2(I))*(HN1(I)-HN2(I)) / C(1) )
  GO TO 600
500 A(1) = 0.
  C(1) = 2.
  D(1) = 0.
  DO 510 J=1,2
    K = I+(J-1)*MAXR
    R(J) = HN(K)-2.*HN1(K)+HN2(K)
    C = C*(HN1(K)-HN2(K))
    A = -( (HN1(K)-HN2(K))*(HN1(K)-HN2(K)) ) - A
510   D = R(J)*R(J) + D
    IF ( D ) 520,600,520
520 HNEW(I) = HN2(I) - (R(1)*A(1)+R(2)*C(1))/ D(1)
    HNEW(K) = HN2(K) - (R(1)*C(1)+R(2)*A(1))/ D(1)
600 CONTINUE

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MTR40130
MTR40131
MTR40133
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MTR40201
MTR40203
MTR40204
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MTR40206
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MTR40210
MTR40211
MTR40212

700	IR = 1	MTR40215
800	RETURN	MTR40217
	END	MTR40219
	FORTRAN LISTING DECK	
C	LEGIS	
	SUBROUTINE LEGIS (LAMBDA, POS, E1, E2, NC, IR)	MTR40222
	DIMENSION LAMBDA(1), POS(1)	MTR40224
	DOUBLE PRECISION LAMBDA, POS, R1, R2A, R2B	MTR40225
	IR=0	MTR40227
	GO TO (100,200),NC	MTR40229
100	R1 = (DABS(LAMBDA(1)-LAMBDA(2))) / E1	MTR40231
	R2A = DABS(DABS(POS(2)/POS(1)) - 1.) / E2	MTR40232
	R2A = DABS(DABS(POS(4)/POS(1)) - 1.) / E2	MTR40233
	CALL MPRINT (R1,2,1,2,6)	MTR40234
	CALL MPRINT (R2A,2,1,2,6)	MTR40235
	CALL MPRINT (R2B,2,1,2,6)	MTR40236
110	IF (R1-R2A)	120,140,140
120	IF (R1-R2B)	130,140,140
130	IR=NC	MTR40238
140	RETURN	MTR40240
200	R1 = DSORT((LAMBDA(1)-LAMBDA(3))*(LAMBDA(1)-LAMBDA(2)) + (LAMBDA	MTR40242
1	(2)-LAMBDA(4))*(LAMBDA(2)-LAMBDA(4))) / F1	MTR40243
	R2A = DABS(DSORT(((POS(3)*POS(1)+POS(2)*POS(4))*(POS(3)+POS(1) +	MTR40245
1	POS(2)*POS(4)) + (POS(3)+POS(2)-POS(4)*POS(1))*(POS(3)+	MTR40249
2	POS(2)-POS(4)*POS(1))) / (POS(1)+POS(1)+POS(2)+POS(2)))	MTR40250
3	-1.) / F2	MTR40251
	R2B = DABS(DSORT(((POS(7)*POS(5)+POS(6)*POS(8)) / (POS(5)+POS	MTR40253
1	(5) + POS(6)*POS(6)))*((POS(7)+POS(5)+POS(6)+POS(8)) /	MTR40254
2	(POS(5)+POS(5) + POS(6)+POS(6))) + ((POS(7)+POS(6) - POS	MTR40255
3	(8)+POS(5)) / (POS(5)+POS(5) + POS(6)+POS(6))) * ((POS(7)	MTR40256
4	+POS(6) - POS(8)+POS(5)) / (POS(5)+POS(5) + POS(6)+POS(6))	MTR40257
5)) - 1.) / F2	MTR40258
	GO TO 110	MTR40260
	END	MTR40262
	FORTRAN LISTING DECK	
C	MAD7	
	SUBROUTINE MAD7 (A,B,C,NSIZE,NC)	MTR40264
	DOUBLE PRECISION A(1), B(1), C(1)	MTR40265
	K=NC+NSIZE	MTR40267
	DO 100 I=1,K	MTR40269
100	C(I)=A(I)-B(I)	MTR40271
	RETURN	MTR40272
	END	MTR40273
	FORTRAN LISTING DECK	
C	MULTS	
	SUBROUTINE MULT (A,B,C,LIZ,NIZ,MIZ,MAXA,MAXB,MAXC,NC,NP)	MTR40275
	DIMENSION A(1), B(1), C(1)	MTR40277
	KA=NC*MAXA	MTR40279
	KB=NC*MAXB	MTR40280
	KC=NC*MAXC	MTR40281
	GO TO (200,100),NP	MTR40283
100	CALL DMULT (A,B,C,LIZ,NIZ,MIZ,KA,KB,KC,NC)	MTR40285
	GO TO 700	MTR40286
200	DO 600 I=1,MIZ	MTR40288
	DO 500 M=1,MIZ	MTR40290
	K = (M-1)*KB + 1	MTR40292
	L = (M-1)*KC + 1	MTR40293
	C(I)=0.	MTR40295
	GO TO (300,400),NC	MTR40297
300	DO 310 N=1,NIZ	MTR40299
	J=(N-1)*KA+1	MTR40301

	JB = (N-1)*K	MTR40302
310	C(I)=C(I)+A(J)*B(JB)	MTR40303
	GO TO 500	MTR40304
400	IC = I+MAXC	MTR40306
	C(IC) = 0.	MTR40307
	DO 410 N=1,NIZ	MTR40309
	J= (N-1)*KA+L	MTR40311
	JH= (N-1) +K	MTR40312
	JC= J+MAXA	MTR40313
	JRC= JB+MAXH	MTR40314
	C(I)=C(I)+A(J)*H(JB)-A(JC)*H(JRC)	MTR40316
410	C(IC)=C(IC)+A(J)*H(JRC)+A(JC)*H(JH)	MTR40317
500	CONTINUE	MTR40319
600	CONTINUE	MTR40321
700	RETURN	MTR40323
	END	MTR40325
S	FORTRAN LST00,DECK	
C	DMULTS	
	SUBROUTINE DMULT (A,B,C,LIZ,NIZ,MIZ,KA,KB,KC,NC)	MTR40327
	DOUBLE PRECISION A(1), B(1), C(1)	MTR40329
	MAXA=KA/2	MTR40330
	MAXB=KB/2	MTR40331
200	DO 600 L=1,LIZ	MTR40332
	DO 500 M=1,MIZ	MTR40334
	K= (M-1)*KB +1	MTR40336
	I= (M-1)*KC +L	MTR40337
	C(I)=0.	MTR40339
	GO TO (300,400),NC	MTR40341
300	DO 310 N=1,NIZ	MTR40343
	J=(N-1)*KA+L	MTR40345
	JB = (N-1)+K	MTR40346
310	C(I)=C(I)+A(J)*B(JB)	MTR40347
	GO TO 500	MTR40348
400	IC=I+KC/2	MTR40350
	C(IC) = 0.	MTR40351
	DO 410 N=1,NIZ	MTR40353
	J= (N-1)*KA+L	MTR40355
	JR= (N-1) +K	MTR40356
	JC= J+MAXA	MTR40357
	JRC= JB+MAXB	MTR40358
	C(I)=C(I)+A(J)*H(JB)-A(JC)*H(JRC)	MTR40360
410	C(IC)=C(IC)+A(J)*B(JRC)+A(JC)*H(JB)	MTR40361
500	CONTINUE	MTR40363
600	CONTINUE	MTR40365
700	RETURN	MTR40367
	END	MTR40369
S	FORTRAN LST00,DECK	
C	POLMS	
	SUBROUTINE POLM (PN,PN1,ON,ON1,E2,LMBD1,LMBD2,NC,IR,IG0)	MTR40372
	DIMENSION PN(1), PN1(1), ON(1), ON1(1), E2(1), LMBD1(1), LMBD2(1)	MTR40374
	DOUBLE PRECISION PN, PN1, ON, ON1, LMBD1, LMBD2, A(2)	MTR40375
	IR=0	MTR40376
	DO 10 (100,100,100),IG0	MTR40377
100	DO 10 (110,200),NC	MTR40379
110	IF (DAHS((PN-PN1)/(DSORT(DAHS(ON))) -E2) 12,120,112	MTR40381
112	IF (DAHS(PN-PN1) - E2**2) 120,120,170	MTR40382
120	IF (DAHS((ON/ON1)-1.) - E2) 13,130,170	MTR40384
130	LMBD2 = (PN*PN - 4.*ON)	MTR40386
	LMBD2 = DSORT (DAHS(LMBD2))	MTR40387
	LMBD1 = (-PN + LMBD2) /2.	MTR40388
	LMBD2 = (-PN - LMBD2) /2.	MTR40389

```

IF ( ABS(LMRD1) - ABS(LMRD2) ) 140,150,160 MTR40391
140 A= LMRD1 MTR40392
   LMRD1=LMBD2 MTR40393
   LMRD2=A MTR40394
   GO TO 160 MTR40395
150 IF ( LMRD1 ) 140,160,160 MTR40396
160 IR=NC MTR40398
170 RETURN MTR40400
180 GO TO (130,220),NC MTR40401
200 A=DSORT( QN(1)*QN(1) + QN(2)*QN(2) ) MTR40403
   IF ( DSORT( ( (PN-PN1)*(PN-PN1) + (PN(2)-PN1(2))*(PN(2)-PN1(2)) ) MTR40405
1 / A ) -E2) 210,210,170 MTR40406
210 A = QN1*QN1 + QN1(2)*QN1(2) MTR40407
   IF ( ( ( QN*QN1-QN(2)*QN1(2) )/A )*( ( QN*QN1-QN(2)*QN1(2) )/A ) + MTR40409
1 ( ( QN*QN1(2)+QN1*QN(2) )/A )*( ( QN*QN1(2)+QN1*QN(2) )/A ) MTR40410
2 -1. ) - E2) 220,220,170 MTR40411
220 A(1) = PN*PN - PN(2)*PN(2) -4.*QN MTR40412
   A(2) = 2.*(PN*PN(2)-2.*QN(2)) MTR40413
   IF ( A(1) ) 230,250,250 MTR40415
230 A(1) = DSORT( (-A(1)+DSORT( A(1)*A(1)+A(2)*A(2) ) ) /2. ) MTR40417
   A(2) = A(2) / (2.*A(1)) MTR40418
232 LMRD1(1) = (-PN+A(2))/2. MTR40420
   LMRD1(2) = (-PN(2)+A(1))/2. MTR40421
   LMRD2(1) = (-PN-A(2))/2. MTR40422
   LMRD2(2) = (-PN(2)-A(1))/2. MTR40423
   IF ( DSORT( LMRD1*LMRD1+LMRD1(2)*LMRD1(2) ) - DSORT( LMRD2*LMRD2 MTR40425
1 LMRD2(2)*LMRD2(2) ) ) 240,160,160 MTR40426
240 A=LMRD1(2) MTR40427
   LMRD1(2)=LMRD2(2) MTR40428
   LMRD2(2)= A MTR40429
   GO TO 140 MTR40430
250 A(1) = DSORT( (A(1)+DSORT( A(1)*A(1)+A(2)*A(2) )) /2. ) MTR40432
   A(2) = A(2) / (2.*A(1)) MTR40433
   LMRD1=A(1) MTR40434
   A(1)=A(2) MTR40435
   A(2)=LMRD1 MTR40436
   GO TO 232 MTR40437
   FND MTR40439
   FORTRAN LISTING DECK
POS
SURROUTINE PD (FL, HN, HN1, HN2, HN3, P, Q, NC, MAXR ) MTR40441
DIMENSION FL(1), HN(1), HN1(1), HN2(1), HN3(1), P(1), Q(1), MTR40442
1 A(3), R(3) MTR40443
DOUBLE PRECISION FL, HN, HN1, HN2, HN3, P, Q, A, R MTR40445
MAXR = MAXR/2 MTR40447
GO TO (200,100), NC MTR40448
100 A(1) = FL(1)*HN - FL(2)*HN(MAXR+1) MTR40450
   A(2) = FL(3)*HN1 - FL(4)*HN1(MAXR+1) MTR40451
   A(3) = FL(5)*HN2 - FL(6)*HN2(MAXR+1) MTR40452
   R(1) = FL(1)*HN(MAXR+1)+ FL(2)*HN MTR40454
   R(2) = FL(3)*HN1(MAXR+1)+FL(4)*HN1 MTR40455
   R(3) = FL(5)*HN2(MAXR+1)+FL(6)*HN2 MTR40456
   P(1) = A(3)*HN1 - R(3)*HN1(MAXR+1)-A(1)*HN3 + B(1)*HN3(MAXR+1) MTR40458
   P(2) = A(3)*HN1(MAXR+1)+R(3)*HN1 - A(1)*HN3(MAXR+1)-R(1)*HN3 MTR40459
   Q(1) = A(1)*HN2 - R(1)*HN2(MAXR+1)-A(2)*HN1 + B(2)*HN1(MAXR+1) MTR40461
   Q(2) = A(1)*HN2(MAXR+1)+R(1)*HN2 - A(2)*HN1(MAXR+1)-R(2)*HN1 MTR40462
   A(1) = A(2)*HN1 - R(2)*HN1(MAXR+1)-A(3)*HN2 + B(3)*HN2(MAXR+1) MTR40464
   R(1) = A(2)*HN1(MAXR+1)+R(2)*HN1 - A(3)*HN2(MAXR+1)-R(3)*HN2 MTR40465
   A(2) = A(1)*P(1) + R(1)*P(2) MTR40467
   R(2) = A(1)*P(2) - R(1)*P(1) MTR40468
   A(3) = A(1)*Q(1) + R(1)*Q(2) MTR40469

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R(3) = A(1)*Q(2) - B(1)*Q(1)
A(1) = A(1)*A(1) + R(1)*R(1)
A(2) = A(2)/A(1)
R(2) = R(2)/A(1)
A(3) = A(3)/A(1)
R(3) = R(3)/A(1)
P(1) = FL(3)*A(2) - FL(4)*R(2)
P(2) = FL(3)*R(2) + FL(4)*A(2)
A(2) = FL(3)*FL(5) - FL(4)*FL(6)
R(2) = FL(4)*FL(5) + FL(3)*FL(6)
Q(1) = A(2)*A(3) - R(2)*R(3)
Q(2) = A(2)*R(3) + A(3)*R(2)
MAXR = 2*MAXR
RETURN
200 A(1) = (FL(2)*HN1*HN3 - FL(3)*HN2*HN2)
P(1) = (FL(3)*HN2(1)*HN1(1) - FL(1)*HN(1)*HN3(1)) / A(1)
Q(1) = (FL(1)*HN(1)*HN2(1) - FL(2)*HN1(1)*HN1(1)) / A(1)
P(1) = P(1)*FL(2)
Q(1) = Q(1)*FL(2)*FL(3)
MAXR = 2*MAXR
RETURN
END

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MTR40470
MTR4047
MTR4047
MTR40474
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MTR4049
MTR40499
MTR4050

S FORTRAN LSTOU,DECK

C CLOSES

C SUBROUTINE CLOSIF. COMPUTES 2 CLOSE ROOTS.

```

C
C U = MATRIX, DIMENSIONED (MAXR,2*NC*MAXR)
C H = STARTING GUESS, DIMENSIONED((MAXR,2*NC*4)+2*NC*N)
C NSIZE = SIZE OF MATRIX
C MAXR = DIMENSIONED NUMBER OF ROWS OF U AND H
C MAXTRY = MAXIMUM NUMBER OF DOUBLE PRECISION ITERATIONS.
C EPS1 = SINGLE ROOT CONVERGENCE CRITERIA
C EPS2 = DOUBLE ROOT CONVERGENCE CRITERIA
C R = AITKENS CONVERGENCE CRITERIA
C IRR = ERROR RETURN INDICATOR. =1, OVERFLOW
C =2, DIVIDE CHECK
C =3, BOTH OVERFLOW AND DIVIDE CHECK.
C
C ITERS= NUMBER OF ITERATIONS PERFORMED, - FOR DOUBLE ROOT
C + FOR SINGLE ROOT
C
C NC = 1, REAL 2, COMPLEX
C
C SUBROUTINE CLOSIF (U,H,NSIZE,MAXR,R,EPS1,EPS2,NC,IRR,MAXTRY,ITERS,
C NAITKN,INDEX1,INDEX2,VALUE,MSIZE)
C
C DIMENSION U(1), H(1), VALUE(1)
C CALL OVERFL ( IOVFLW )
C CALL DVCHK ( IDVDCY )
C IRR=0
C NX=2*NSIZE
C N2C=2*NC
C CALL CHANGE (U,MSIZE,NC*MSIZE,MAXR,1)
C CALL CHANGE (H,MSIZE,NC,NSIZE,1)
C I6=N2C*NSIZE
C I1=1
C I2=I1+16
C I3=I2+16
C I4=I3+16
C I5=I4+16
C K1=I1
C K4=I2
C K3=I3
C K2=I4

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MTR4050
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MTR40538
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MTR40544

	ITFRS = 0		MTR40545
100	K=0		MTR40547
	IG0 = 1		MTR40548
120	ITFRS=ITFRS+1		MTR40549
	IF (ITFRS-MAXTRY)	140,140,130	MTR40550
130	IF (K=0)	132,140,132	MTR40551
132	ITFRS = ITFRS-1		MTR40552
	GO TO 800		MTR40553
140	K=K+1		MTR40555
	I=K1		MTR40556
	K1=K4		MTR40557
	K4=K3		MTR40558
	K3=K2		MTR40559
	K2=I		MTR40560
	CALL MULT (I) ,H(K2),H(K1),NSIZE,NSIZE,I,MAXR,NSIZE,NSIZE,		MTR40562
1	NC,2)		MTR40563
	INDEX=0		MTR40564
	IK=I5+(4-K)*N2C		MTR40565
	CALL NORM (H(K1),H(K1),NSIZE,H(IK),INDEX,NSIZE,NC,2)		MTR40566
	CALL OVERFL (IOVFLW)		MTR40568
	GOTO (150,160) ,IOVFLW		MTR40569
150	IRR=IRR+1		MTR40570
160	CALL DVCHK (IDVCT)		MTR40571
	GOTO (170,180) ,IDVCT		MTR40572
170	IRR=IRR+2		MTR40573
180	IF (IRR)	200,200,640	MTR40574
C	TEST FOR CONVERGENCE TO A SINGLE ROOT		MTR40576
200	DO 220 I=1,16,2		MTR40578
	J2 = K2+I-1		MTR40579
	J3 = K1+I-1		MTR40580
	IF (ABS(H(J2)-H(J3))-EPS1)	220,220,300	MTR40581
220	CONTINUE		MTR40582
	GOTO 750		MTR40583
300	GOTO (120,120,120,320),K		MTR40585
320	J1=15+(IG0+J)*N2C		MTR40587
	J2=15+(IG0+5)*N2C		MTR40588
	J=2*INDEX-2		MTR40590
	J3=K1+J		MTR40591
	J5=K2+J		MTR40592
	J7=K3+J		MTR40593
	J9=K4+J		MTR40594
C	COMPUTE P N AND Q N.		MTR40596
	CALL PD (H(I5), H(J3), H(J5), H(J7), H(J9), H(J1), H(J2), NC, NX)		MTR40597
	GOTO (350,340),IG0		MTR40600
340	J1= 15+4*N2C		MTR40601
	J2= J1+N2C		MTR40602
	J3= J2+N2C		MTR40603
	J4= J3+N2C		MTR40604
	J5= 15+N2C		MTR40605
	J6= J5+N2C		MTR40606
C	TEST FOR DOUBLE ROOT CONVERGENCE AND IF SO, COMPUTE LAMBDA 1 AND 2.		MTR40608
	CALL POLM (H(J2),H(J1),H(J4),H(J3),EPS2,H(J5),H(J6),NC,IR,IG0)		MTR40610
	GOTO (344,344,400),IG0		MTR40611
344	IF (IR)	346,346,400	MTR40612
346	IF (ITFRS-MAXTRY)	347,800,800	MTR40613
347	DO 348 I=1,N2C		MTR40614
	H(J1)=H(J2)		MTR40615
	H(J3)=H(J4)		MTR40616
	J1=J1+1		MTR40617
	J2=J2+1		MTR40618
	J3=J3+1		MTR40619

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348 J4=J4+1
350 K=3
      IGO=2
      DO 354 J=1,3
      L=15+(3-J)*N2C
      L1=15+(4-J)*N2C
      DO 354 I=1,NC
      L=L+(I-1)*NC
      L1=L1+(I-1)*NC
      H(L1)=H(L)
354 H(L1+1)=H(L+1)
      CALL AITKNS (H(K1), H(K2), H(K3), H(K4), R, VALUE, NSIZE, NC, 2,
1 IR )
      IF ( IR ) 360,120,360
360 I=K1
      K1=K4
      K4=K3
      K3=K2
      K2=1
      NAITKN = NAITKN+1
      GOTO 100
400 CALL POH (H(J5), H(J6), H(K1), H(K2), H(K3), H(K4), NSIZE,
1 NC)
      GOTO (404,402),NC
402 VALUE(2)=H(J5+2)
      VALUE(4)=H(J6+2)
404 INDEX=0
      VALUE(1)=H(J5)
      VALUE(NC+1)=H(J6)
      CALL NORM (H(K3),H(K3),NSIZE,H(J1),INDEX,NSIZE,NC,2)
      INDEX1 = INDEX
      ITERS = -ITERS
      I=K4+2+INDEX-2
      H(J1)=H(I)
      H(J1+1)=H(I+1)
      GOTO (420,410),NC
410 I = I+NX
      H(J1+2)=H(I)
      H(J1+3)=H(I+1)
420 INDEX=-INDEX
      CALL NO.M (H(K4),H(K4),NSIZE,H(J1),INDEX,NSIZE,NC,2)
      IF ( K - 2 ) 440,500,480
440 J3=13
442 J4=14
450 K=1
460 DO 462 J=1,16
      J1=J3+J-1
      J2=J4+J-1
462 H(J1)=H(J2)
      GOTO (520,510,514,600),K
470 J3=11
      GOTO 442
480 IF ( K3-13 ) 490,490,470
490 K=3
      J3=11
      J4=13
      GOTO 460
500 K=2
      J3=13
      J4=11
      GOTO 460
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510	J3=11		MTR40688
512	J4=12		MTR40689
	GOTO 450		MTR40690
514	J3=13		MTR40691
	GOTO 512		MTR40692
520	CALL MADS (H(I1),H(I3),H(I2),NSIZE,NC)		MTR40693
600	CALL CHANGE (H(I1),NSIZE,2*NC,NSIZE,2)		MTR40695
604	J=NC*NSIZE+1		MTR40697
	INDEX=0		MTR40698
	CALL NORM (H(J),H(J),NSIZE,H(I5),INDEX,NSIZE,NC,1)		MTR40700
	J=J+INDEX-1		MTR40701
	J1=J+(NC-1)*NSIZE		MTR40702
	H(J)=0.		MTR40703
	H(J1)=0.		MTR40704
	INDEX2 = INDEX		MTR40705
606	CALL OVERFL (IOVFLW)		MTR40707
	GOTO (610,620) ,IOVFLW		MTR40708
610	IRR=IRR+1		MTR40709
620	CALL DVCHK (IDVDCT)		MTR40711
	GOTO (630,640) ,IDVDCT		MTR40712
630	IRR=IRR+2		MTR40713
640	CALL CHANGE (0,MSIZE,NC*MSIZE,MAXR,?)		MTR40715
700	RETURN		MTR40717
750	IK=I5+(4-K)*N2C		MTR40719
	VALUE(1) = H(IK)		MTR40720
	IK=IK+2*(NC-1)		MTR40721
	VALUE(NC)=H(IK)		MTR40722
	INDEX1=INDEX		MTR40723
	K=4		MTR40724
	J3=11		MTR40725
	J4=K1		MTR40726
	IF (K1-11)	460,600,460	MTR40727
800	IG0=3		MTR40729
	INDEX1=INDEX		MTR40730
	J=I5		MTR40731
	J1 = I5+4*N2C		MTR40732
806	CALL LEGIS (H(J),H(J1),FPS1.EPS2,NC,IR)		MTR40733
	IF (IR)	340,340,750	MTR40734
	END		MTR40736
	* FORTRAN LISTING DECK		
	* MITERS		
	A IS STORED IN CORE AT A. (MAXR X NC*NP*NSIZE)		MTR40738
	NTAPUT IS A UTILITY TAPE, FOR CHECK VECTORS IF DESIRED.		MTR40739
	EPSP = EPSILON ONE = SINGLE PRECISION CONVERGENCE TEST NUMBER		MTR40740
	EPDP = EPSILON TWO = DOUBLE PRECISION		MTR40741
	NC = 1, IF REAL NP = 1, IF SINGLE PRECISION		MTR40742
	2, IF COMPLEX = 2, IF DOUBLE ..		MTR40743
	NGUESS = 0, IF FIRST GUESS IS TO BE A COLUMN OF ONES.		MTR40744
	MODOUT = NO. OF MODES TO BE COMPUTED.		MTR40745
	NAKSR - NO. TIMES AITKENS ACCELERATION WAS USED IN SINGLE PRECISION.		MTR40746
	NAKDR = DOUBLE ..		MTR40747
	MAXSR = MAXIMUM ITERATIONS ALLOWED IN SINGLE PRECISION.		MTR40748
	MAXDR = DOUBLE ..		MTR40749
	IRP = ERROR RETURN = 1, FOR OVERFLOW		MTR40750
	2, FOR DIVIDE CHECK		MTR40751
	3, FOR BOTH OVERFLOW AND DIVIDE CHECK		MTR40752
	NSIZE = NO. OF ROWS AND COLUMNS OF A		MTR40753
	RSP = R, AITKENS ACCELERATION CONVERGENCE CONTROL FOR SINGLE PRECIS.		MTR40754
	RDP = R AITKENS ACCELERATION CONVERGENCE CONTROL FOR DOUBLE PRECIS.		MTR40755
	MAXR = DIMENSIONED NUMBER OF ROWS OF A AND GUESS		MTR40756
	SUBROUTINE MITERS(A,GUESS,NGUESS,NSIZE,MODOUT,MAXR,NC,FPS1,EPDP,		MTR40758


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NDRAK=0
ITFRSR=0
ITFRDR=0
K1=11
K2=13
K3=12
DO 150 K=1,NC
  J1=(K-1)*NSIZE
  J=(K-1)*MSIZE+K1-1
  DO 150 I=1,MSIZE
    J=J+1
    J1=J1+1
150 H(J)=GUFSS(J1)
152 NAK=0
150 NAK=NAK+1
152 ITFRSR=ITFRSR+1
  IF ( ITFRSR-MAXSR ) 170,170,250
170 I=K1
  K1=K3
  K3=K2
  K2=I
C SET ... NOW MAKE ONE ITERATION.
C
CALL MULT (A,H(K2),H(K1),MSIZE*MSIZE,1,MAXR,MSIZE,MSIZE,NC,1)
INDEX=0
IK= I+KSIZE+NC*(1-NAK)
CALL NORM (H(K1),H(K1),MSIZE,H(IK),INDEX,MSIZE,NC,1)
CALL OVERFL ( IOVFLW )
CALL DVCHK ( IDVCT )
GOTO (180,182) ,IOVFLW
180 IRR=IRR+1
182 GOTO (184,186) ,IDVCT
184 IRR=IRR+2
186 IF ( IRR ) 190,190,600
190 GOTO (160,200,200),NAK
200 DO 210 I=1,KSIZE
  J1=K1+I-1
  J2=K2+I-1
  IF ( ABS(H(J1))-H(J2))-EPSP ) 210,210,220
210 CONTINUE
  GOTO 400
220 GOTO (160,160,230),NAK
230 CALL AITKNS ( H(K1), H(K2), H(K3), H(K3), RSP, MSIZE, MSIZE, NC,
  I, IR )
  IF ( IR ) 240,232,240
232 I=2*NC
  J=IK+1
  DO 234 I=1,I,NC
    J1=J+NC-I
    J2=J-I+1
    J3=J1-NC
    J4=J2-NC
    H(J1)=H(J3)
234 H(J2)=H(J4)
  GOTO 162
240 I=K1
  K1=K3
  K3=K2
  K2=I
  NSRAK=NSRAK+1
  GOTO 152

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MTR40836
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MTR40912

250	CALL OVERFL (IOVFLW)		MTR40914
	CALL DVCHK (IOVDCT)		MTR40915
	GOTO (260,262) ,IOVFLW		MTR40916
260	IRR=IRR+1		MTR40917
262	GOTO (264,266) ,IOVDCT		MTR40918
264	IRR=IRR+2		MTR40919
266	IF (IRR)	270,270,600	MTR40920
270	IF (K1-I1)	272,280,272	MTR40922
272	DO 274 I=1, KSIZE		MTR40924
	J=K1+I-1		MTR40925
	J1=I1+I-1		MTR40926
274	H(J1) = H(J)		MTR40927
280	J=(MODE-1)*NC+1		MTR40928
	ITERSR=ITERSR-1		MTR40929
	CALL CLOSES(A, H(I1), MSIZE, MAXR, RDP, EPSP, EPDP, NC, IRR, MAXDR, ITERDR,		MTR40930
1	NDRAK, INDEX1, INDEX2, VALUE(J), NSIZE)		MTR40931
	IF (IRR)	282,282,610	MTR40945
282	IF (ITERDR)	283,288,288	MTR40946
283	IF (KSIZE-ISIZE)	284,288,288	MTR40940
284	I1 = I1+2*KSIZE		MTR40950
	I2 = I2+KSIZE		MTR40951
	DO 286 I=1, KSIZE		MTR40952
	J1= J1-1		MTR40953
	J2= J2-1		MTR40954
286	H(J2)=H(J1)		MTR40955
288	INDEX = INDEX1		MTR40957
	INDIX = INDEX		MTR40958
290	M1 = NSIZE-1		MTR40959
	J1=INDEX		MTR40960
	IF (J1-M1)	292,292,298	MTR40961
292	DO 296 K=1, ISIZE		MTR40962
	L=(K-1)*MAXR		MTR40963
	L1=L+INDEX		MTR40964
	HOLD= A(L1)		MTR40965
	DO 294 J=J1, M1		MTR40966
	I=L+J		MTR40967
294	A(I) = A(I+1)		MTR40968
296	A(I+1)=HOLD		MTR40969
298	I=NSIZE-MODE+1		MTR40970
	J = (MODE-1) * NC * MAXR +1		MTR40972
	CALL SWAPX (VECTOR(J), A, H, A(L), VALUE, MODE, MSIZE, MAXR, NC,		MTR40977
1	INDIX, EPSP, NSIZE, NITER(MODOUT+1) , IRR)		MTR40978
	CALL OVERFL (IOVFLW)		MTR40979
	CALL DVCHK (IOVDCT)		MTR40980
	GOTO (300,302) ,IOVFLW		MTR40982
300	IRR=IRR+1		MTR40983
302	GOTO (304,306) ,IOVDCT		MTR40984
304	IRR=IRR+2		MTR40985
306	IF (IRR)	310,310,620	MTR40986
310	I=(NC-1)*NSIZE		MTR40988
	DO 312 J=INDEX, NSIZE		MTR40989
	I=I+J		MTR40990
	GUESS(I)=GUESS(L+1)		MTR40991
312	GUESS(J)=GUESS(J+1)		MTR40992
	MSIZE = MSIZE-1		MTR40994
	NITER(MODE) = ITERSR+ITERDR		MTR40995
	NAKSR(MODE)= NSRAK		MTR40996
	NAKDR(MODE)= NDRAK		MTR40997
	IF (ITERDR)	320,360,360	MTR40998
320	MODE=MODE+1		MTR40999
	ITERDR=-ITERDR		MTR41000

```

NITER(MODE-1) = 0.
INDEX=INDEX2
IF ( INDEX-NSIZE )
326 IF ( INDEX1-INDEX2 )
330 INDEX=-INDEX
    -INDEX=INDEX-1
    GOTO 342
340 INDEX=-INDEX
342 CONTINUE
    I1=I1+ISIZE
    I2=I2+ISIZE
    I3=I3+ISIZE
    NAKSR(MODE-1) = 0.
    NAKDR(MODE-1) = 0.
    GOTO 290
350 I1=I1+ISIZE
    I2=I1+ISIZE
    I3=I2+ISIZE
    GOTO 130
400 IF ( K1-I1 )
410 DO 412 I=1,KSIZE
    J=K1+I-1
    J1=I1+I-1
412 H(J1)=H(J)
413 DO 414 J=1,NC
    I= NC*(MODE-1)+1
    J1=IK+J-1
414 VALUE(I)= H(J1)
    INDEX=INDEX
    GOTO 290
500 MODE=MODE-1
    IF ( MODE )
502 IF ( NTAPUT )
504 READ ( NTAPUT ) (A(I),I=1,M)
    CALL MULT (A,VECTOR, H,NSIZE,NSIZE,MODE,MAXR,MAXR,MAXR ,NC,1)
    DO 506 I=1,MODE
    J= (I-1)*ISIZE
    J1 = (I-1)*NC+1
    INDEX=0
506 CALL NORM (H(J),H(J1),NSIZE,GUESS(J1),INDEX,MAXR ,NC,1)
510 IF ( NTAPUT )
512 WRITE (NTAPUT,10 )
    DO 522 I=1,MODE
    J1= MAXSR
    J2= NITER(I)-MAXSR
    IF ( J2 )
514 J1=NITER(I)
    J2=0
    GO TO 517
515 IF ( J2-MAXDR )
516 WRITE (NTAPUT,20)
517 GO TO (518,520) ,NC
518 WRITE (NTAPUT,11)
    GOTO 522
520 J= 2*I
    WRITE (NTAPUT,12)
522 CONTINUE
    J=NC*MODE
    WRITE (NTAPUT,20)
    CALL MPRINT (VECTOR,NSIZE,J,MAXR,NTAPUT)

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MTR41001
MTR41002
MTR41003
MTR41004
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      IF ( NTAPOT )
524 WRITE (NTAPOT,22) ((GUESS(I),I=1,J))
      CALL MPRINT ( H,NSIZE,J,MAXR,NTAPOT)
530 RETURN
540 NITER(MODE) = ITERS+ITERDR
      NAKSR(MODE) = NSRAK
      NAKDR(MODE) = NDRAK
      IF ( NTAPOT )
541 J=1
      J1=4
      GOTO (602,604,606),IRR
542 J1=2
      GOTO 606
544 J=3
546 WRITE (NTAPOT,26) (ATITLE(I),I=J,J1)
      GOTO 630
548 J2=6
549 NITER(MODE) = ITERS+ITERDR
      NAKSR(MODE) = NSRAK
      NAKDR(MODE) = NDRAK
      IF ( NTAPOT )
550 J=1
      J1=4
      GOTO (614,616,618),IRR
551 J1=2
      GOTO 618
552 J=3
553 WRITE (NTAPOT,26) (ATITLE(I),I=J,J1), (ATITLE(5)),
      (ATITLE(J2)), (ATITLE(I),I=8,9)
      IF ( J2=6 )
554 J2=7
      GOTO 612
555 WRITE (NTAPOT,18) MODE
      IRR=0
      J= (MODE-1)*NC+MAXR
      DO 624 I=1,ISIZE
      J1=J+1
      J2=J+(NC-1)*MAXR+1
      VECTOR(J2)=0.
556 VECTOR(J1)=0.
      GOTO 310
557 I=MODE-
      WRITE (NTAPOT,16) I
      GOTO 500
      END
*
* FORTRAN LISTING DECK
*
* SWEEPS
*
* S W E E P X S U B R O U T I N E
*
* COMPUTES TRUE MODE AND SWEEPS IT FROM THE MATRIX. (REAL OR COMPLEX)
*
* HTRUE = TRUE MODAL COLUMNS, AS COMPUTED. U = DYNAMIC MATRIX.
* H = SERIES OF MODIFIED MODAL COLUMNS. FL= COLUMN OF EIGENVALUES.
* US = SERIES OF MODIFIED MODAL ROWS OF U.
* MODE = MODE NOW BEING COMPUTED. N = SIZE
* MD = DIMENSIONED NUMBER OF ROWS OF U,US,H,HTRUE
* NX = 1 IF PROBLEM IS REAL.
* : 2 IF PROBLEM IS COMPLEX.
*
* SUBROUTINE SWEEPX (HTRUE, U, H, US, FL, MODE, N, NC, INDIX,
* EP, MSIZE, INDIS, IRR)
*
* DIMENSION H(1), US(1), U(1), HTRUE(1), FL(1), G(4) INDIS(1)

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INDEX=IARS(INDEX)
INDIS(MODE) = INDEX
M=MODE-1
K1=M*NC*MD
NN=NC*MD
K2=MSIZE-M
IF ( M ) 70,70,K0
70 GOTO (140,72) ,NC
72 IF ( MSIZE-MD ) 74,140,140
74 L=K1+2*N+1
K=K1+MD+N+1
DO 76 I=1,N
    K=K-1
    L=L-1
    H(K)=H(L)
76 H(L)=0.
GOTO 140
80 DO 90 I=1,M
    J1=MODE+I
90 INDIS(J1)=INDIS(I)
100 IF ( INDEX ) 102,104,104
102 K2=K2+1
M=M-1
104 J1=K1+K2*NC+1
J2=K1+MSIZE*NC
IF ( J1-J2 ) 105,105,107
105 DO 106 I=J1,J2
106 H(I)=0.
107 GO TO (114,108),NC
108 J1=K1+K2*MD+1
J2=K1+K2*NC+1
DO 110 I=1,K2
    J1=J1-1
    J2=J2-1
110 H(J1)=H(J2)
IF ( M ) 118,118,111
111 DO 112 I=1,M
    H(J2)=0.
112 J2=J2+1
114 IF ( M ) 118,118,120
120 I=1
DO 120 I=1,M
121 DO 122 J=1,M
    J1=MODE+J
    IF ( I - INDIS(J1) ) 122,124,122
122 CONTINUE
    I=I+1
GOTO 121
123 INDIS(J1)=0
I ( INDIS(MODE)-I ) 125,124,124
124 INDIS(MODE) = INDIS(MODE)+1
125 I=MSIZE-I
I ( I ) 129,129,126
126 J1= K1+MSIZE
J2= K1 +MSIZE +(NC-1)*MD
DO 128 J=1,I
    J1=J1-1
    J2=J2-1
128 H(J2+1) = H(J2)
H(J1+1) = H(J1)
129 J1=K1+I

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J2=J1+(NC-1)*MD		MTR41217
H(J1)=0.		MTR41218
H(J2)=0.		MTR41219
130 CONTINUE		MTR41220
IF (INDEX)	119,130,131	MTR41221
118 M=M+1		MTR41222
131 DO 132 I=1,M		MTR41223
J1=MODE+I		MTR41224
132 INDIS(J1)=INDIS(I)		MTR41225
II=1		MTR41226
DO 133 I=1,M		MTR41227
133 DO 134 J=1,M		MTR41228
J1=MODE+J		MTR41229
IF (II-INDIS(J1))	1134,1135,1134	MTR41230
1134 CONTINUE		MTR41231
II=II+1		MTR41232
GOTO 133		MTR41233
1135 L1=(NC*MSIZE-1)*MD+MODE+1		MTR41234
L3=(MSIZE-1)*NN		MTR41235
INDIS(J1) = 0		MTR41236
DO 138 J=1,NC		MTR41237
J2=L1-(J-1)*MD-1		MTR41238
IF (L3-NN)	138,134,134	MTR41239
134 DO 136 I=1,L3,NN		MTR41240
J1=L1-I		MTR41241
J2=J1-NN		MTR41242
136 US(J1)=US(J2)		MTR41243
II=L1-MD		MTR41244
138 US(J2)=0.		MTR41245
140 DO 142 I=1,NN		MTR41246
J1=K1+I		MTR41247
142 HTRUE(I)=H(J1)		MTR41248
IF (M)	31,31,R	MTR41249
R DO 25 I=1,M		MTR41250
K=MODE-I		MTR41251
L1=NC*MD*(K-1)		MTR41252
CALL MULT (US(K), HTRUE, G, 1, MSIZE, 1, MD, M, 1, NC, 1)		MTR41253
IF (G(1))	12,9,12	MTR41259
9 GO TO (11,10),NC		MTR41260
10 IF (G(1))	12,11,12	MTR41261
11 IRR=IRR+2		MTR41262
12 CONTINUE		MTR41263
GOTO (14,19),NC		MTR41264
14 IF (ABS(FI(K)/FL(MODE)-1.0) - FP)	15,15,16	MTR41262
15 G=1.0		MTR41266
GOTO 17		MTR41267
16 G=(FI(K)-FI(MODE)) / G		MTR41268
17 DO 18 J=1,MSIZE		MTR41269
I=L1+J		MTR41270
18 HTRUE(J)=H(I)-G(1)*HTRUE(J)		MTR41271
GOTO 25		MTR41272
19 K=2*K		MTR41273
I=2*MODE		MTR41274
IF (ABS((FI(K-1)*FI(J-1)+FL(K)*FL(J))/(FL(J-1)**2+FI(J)**2)-1.0)		MTR41275
-FP)	20,20,20	MTR41276
20 IF (ABS((FI(K)*FI(J-1)-FI(K-1)*FL(J)) / (FL(J-1)**2+FL(J)**2))		MTR41277
-FP)	21,21,22	MTR41278
21 G(1)=1.0		MTR41279
G(2)=0.0		MTR41280
GOTO 23		MTR41281
22 G(3)=G(1)**2+G(2)**2		MTR41282


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G(4)=(FL(K)-FL(J))*G(1)-(FL(K-1)-FL(J-1))*G(2)
G(1)=((FL(K-1)-FL(J-1))*G(1)+(FL(K)-FL(J))*G(2)) / G(3)
G(2)= G(4) / G(3)
23 DO 24 J1=1,MSIZE
    K2=J1+MD
    L=L1+J1
    I2=I+MD
    G(3)=HTRUF(J1)
    HTRUE(J1) = H(L) + G(2)*HTRUF(K2) -G(1)*HTRUE(J1)
    HTRUE(K2)= H(L2)- G(1)*HTRUE(K2)-G(2)*G(3)
24 CONTINUE
25 CONTINUE
I=0
CALL NORM ( HTRUF,HTRUE,MSIZE,G,I,MD,NC,1)
31 J1 = 1
    J2 = 1
    L4 = MODE
    DO 43 I=1,MSIZE
        I1=J1
        I2=J2
        I3=K1+1
        DO 33 MM=1,MODE
            IF ( I -INDIS(MM) ) 33,39,33
33 CONTINUE
        DO 37 J=1,MSIZE
            DO 35 MM=1,MODE
                IF ( J-INDIS(MM) ) 35,37,35
35 CONTINUE
                U(L1) = U(I2) - H(I3)*US(L4)
                GOTO (38,36),NC
36 J3= L1+MD
                J4= L2+MD
                J5= L4+MD
                J6= L3+MD
                U(J3)=U(J4)-H(I3)*US(J5) - H(J6)*US(L4)
                U(L1)= U(I1) + H(J6)*US(I5)
38 CONTINUE
                L1=L1+1
                L2=L2+1
                L3=L3+1
37 GOTO 41
39 IF ( I-INDIS(MODE) ) 43,42,43
41 J1=J1+NN
42 J2=J2+NN
43 L4=L4+NN
L4=(MSIZE-MODE)*NN+1
DO 52 J=1,NC
    L4 = L4 + (J-1)*MD
L1=L4+(MSIZE-MODE)-1
DO 52 I=L4,11
52 U(I)=0.
RETURN
END
FORTRAN LISTING DECK
C CHANGES
SUBROUTINE CHANGE (A,M,N,MAXR,ICHU2)
DIMENSION A(1)
NR=2*MAXR
DO 10 (10,20),ICHU2
10 DO 12 I=1,N
    K=(N-1)*MAXR+M+1

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      KK=(N-1)*MR+2*M+1
      DO 12 J=1,M
        IGFT=K-J
        IPUT=KK-2*J
        A(IPUT)=A(IGFT)
12     A(IPUT+1)=0.
      GO TO 100
20     K=0
      KK=0
      DO 24 I=1,N
        DO 22 J=1,M
          IGFT = KK+2*J-1
          IPUT=K+J
22     A(IPUT) = A(IGFT)
        K=K+MAXK
24     KK=KK+MB
100    RETURN
      END

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SECTION 9

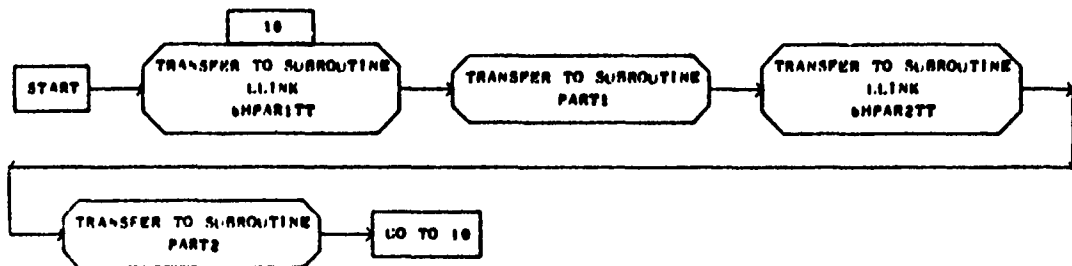
FLOW DIAGRAMS

MAIN FLUTTER OVERLAY

JAN 13, 1967

COMMON 17(216)

PAGE 1



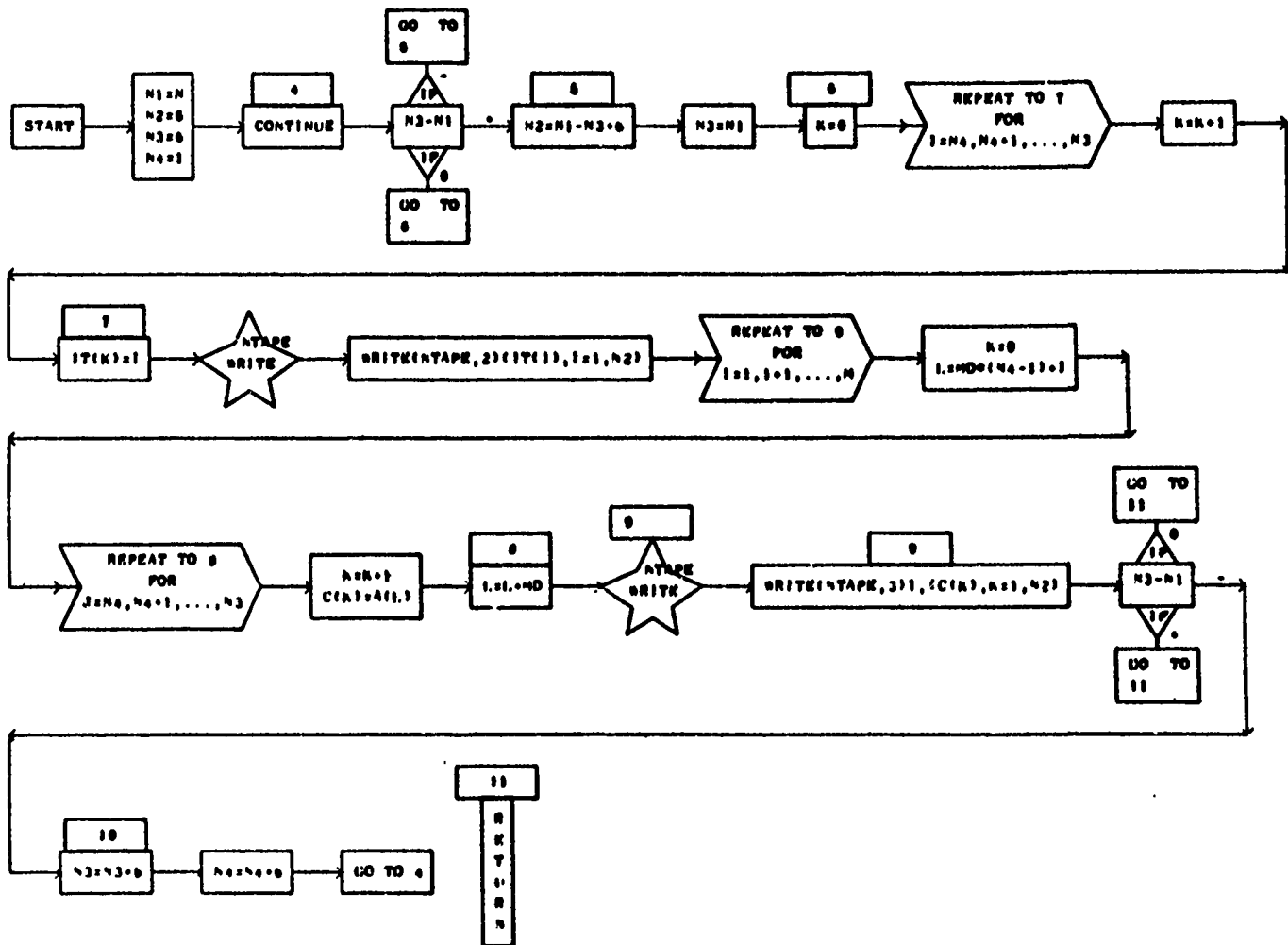
MPRINT

DIMENSIONED VARIABLES

SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE
A	1	IT	6	C	6				

SUBROUTINE MPRINT (A,N,M,ND,NTAPE)

PAGE 1



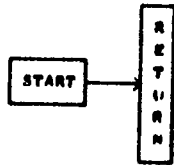
MPINCH

D I M E N S I O N E D V A R I A B L E S

SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE
A	1								

SUBROUTINE MPINCH(A,M,N,IOUT,ITRA,IONG,ICDZ,MAXM,NTAPE,NCARDS)

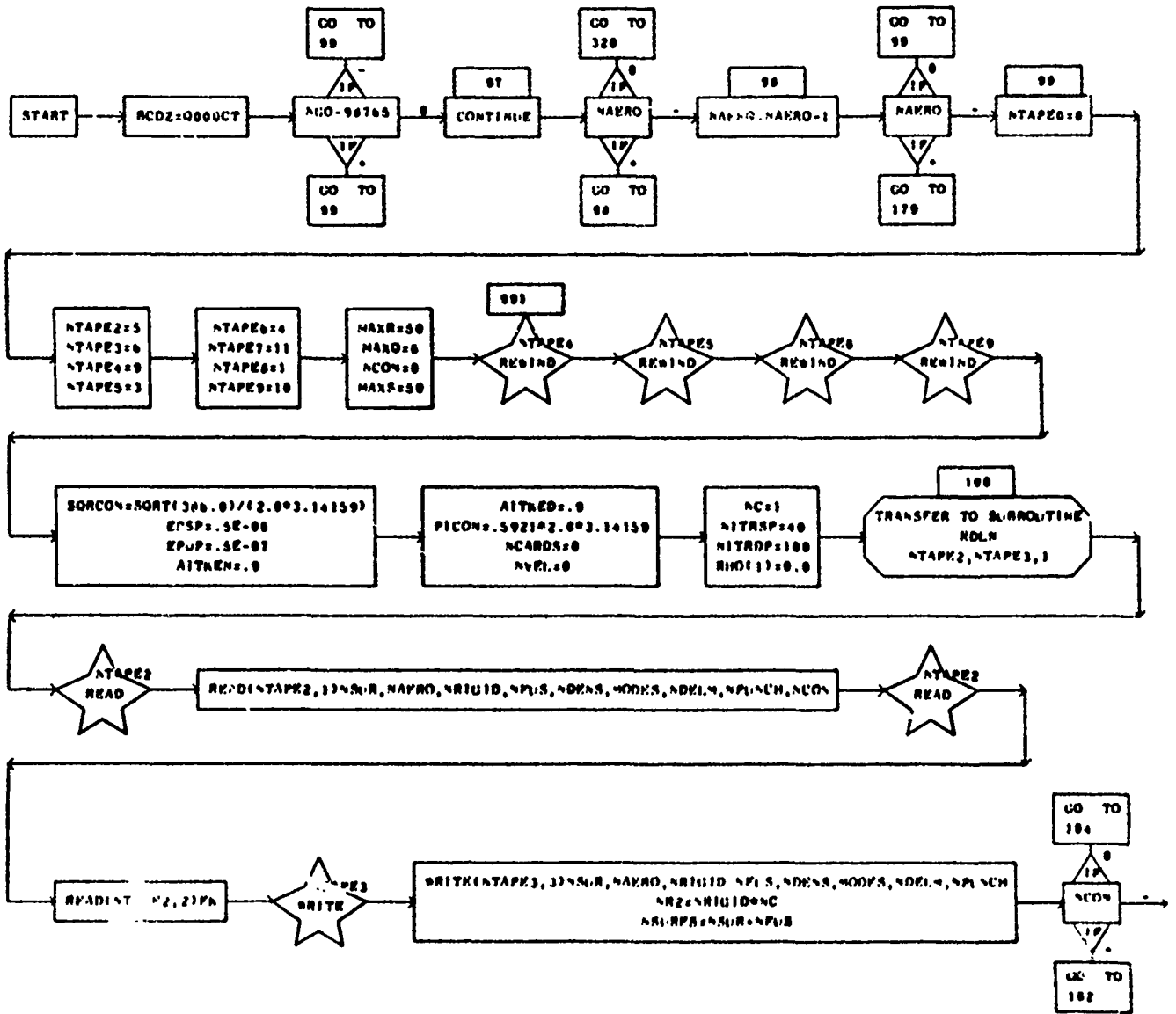
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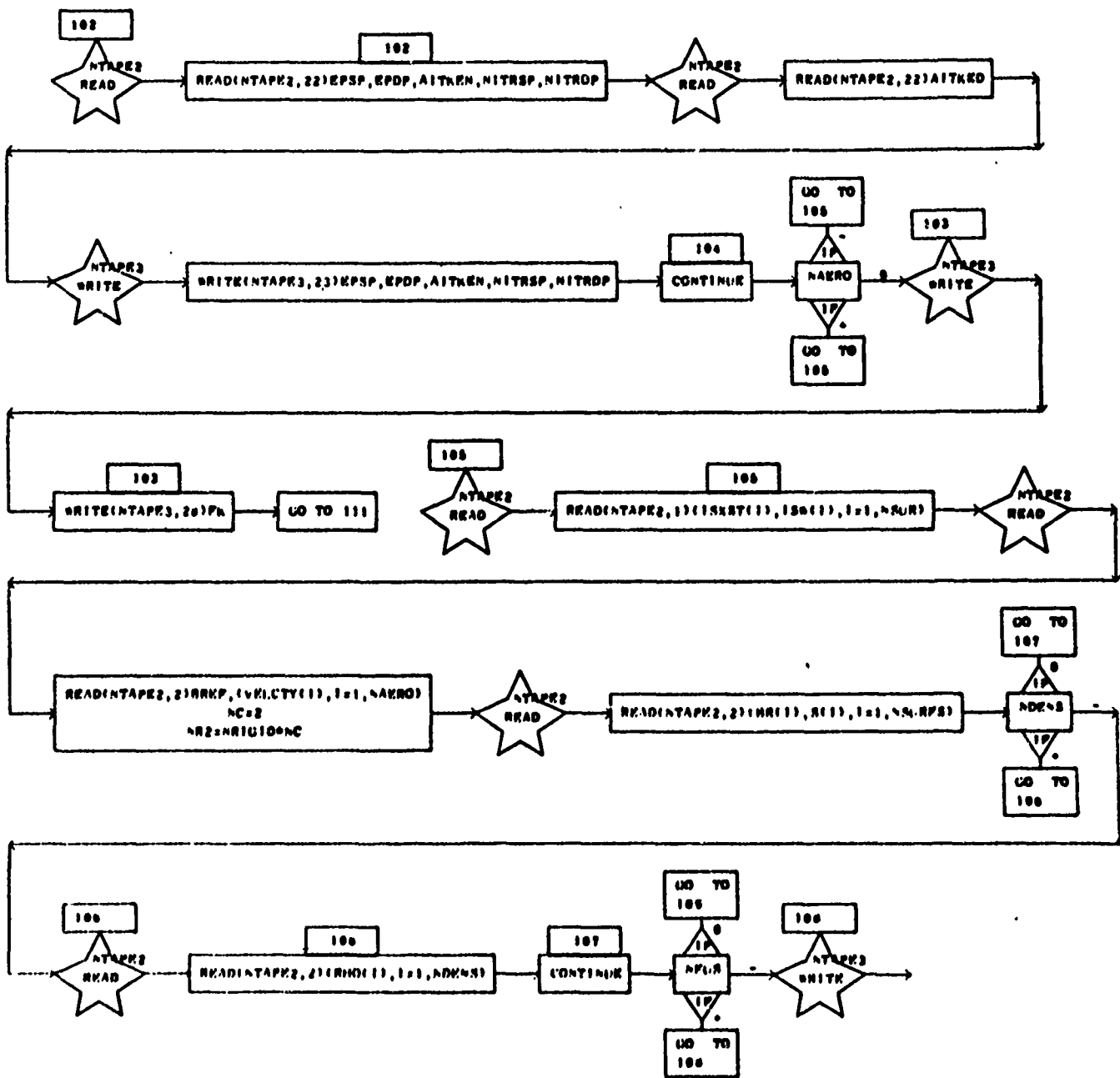


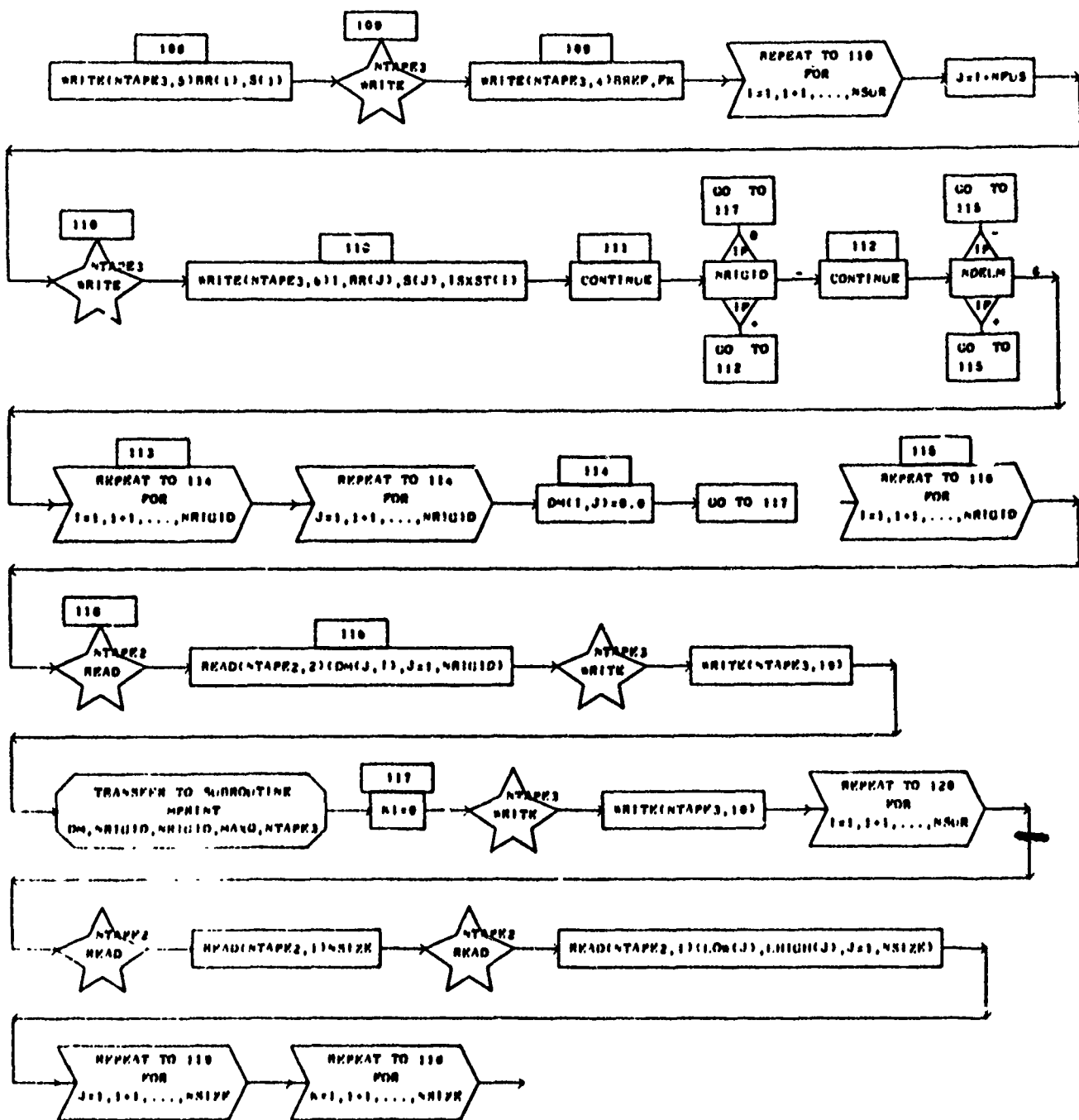
PARTS

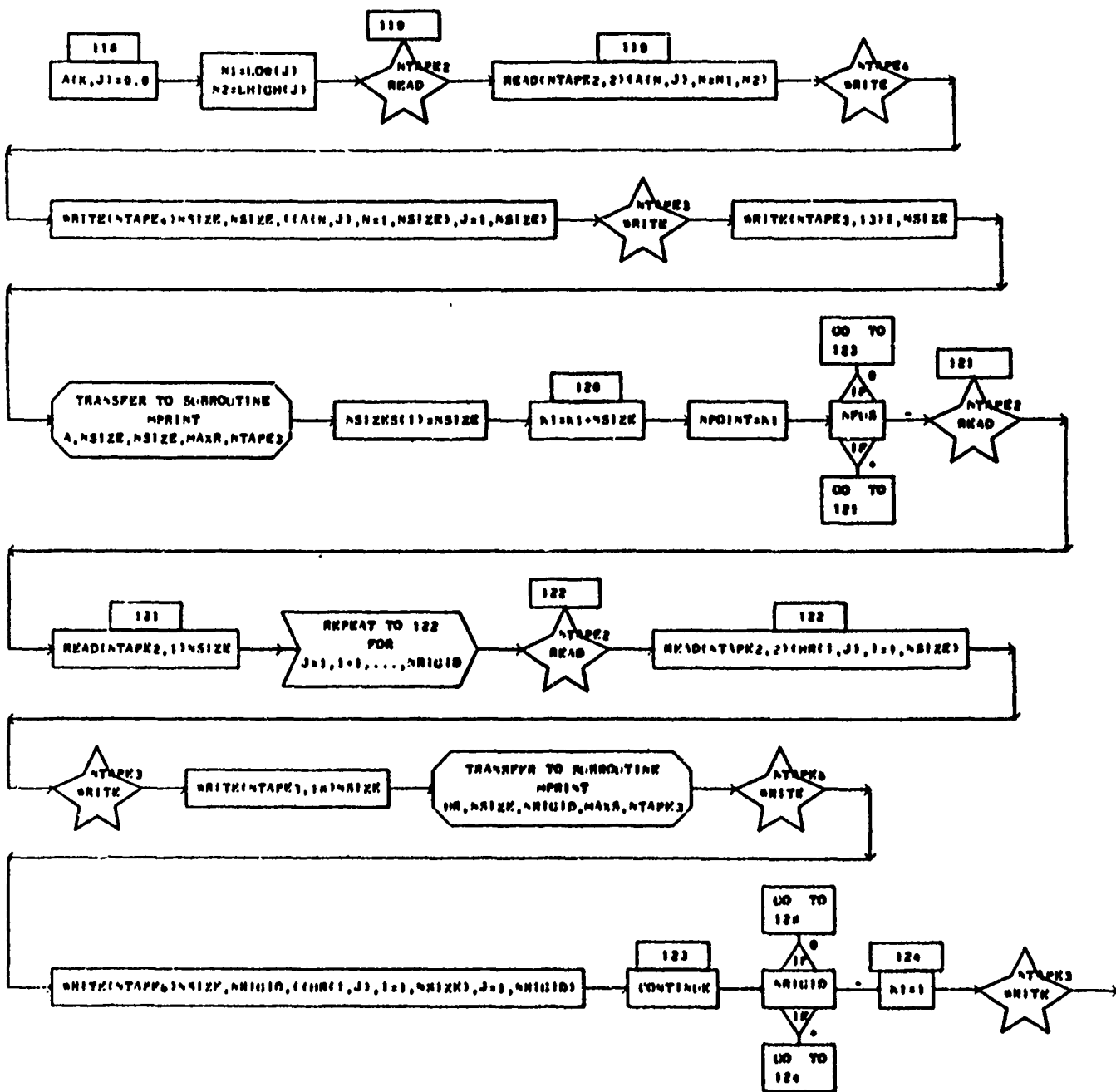
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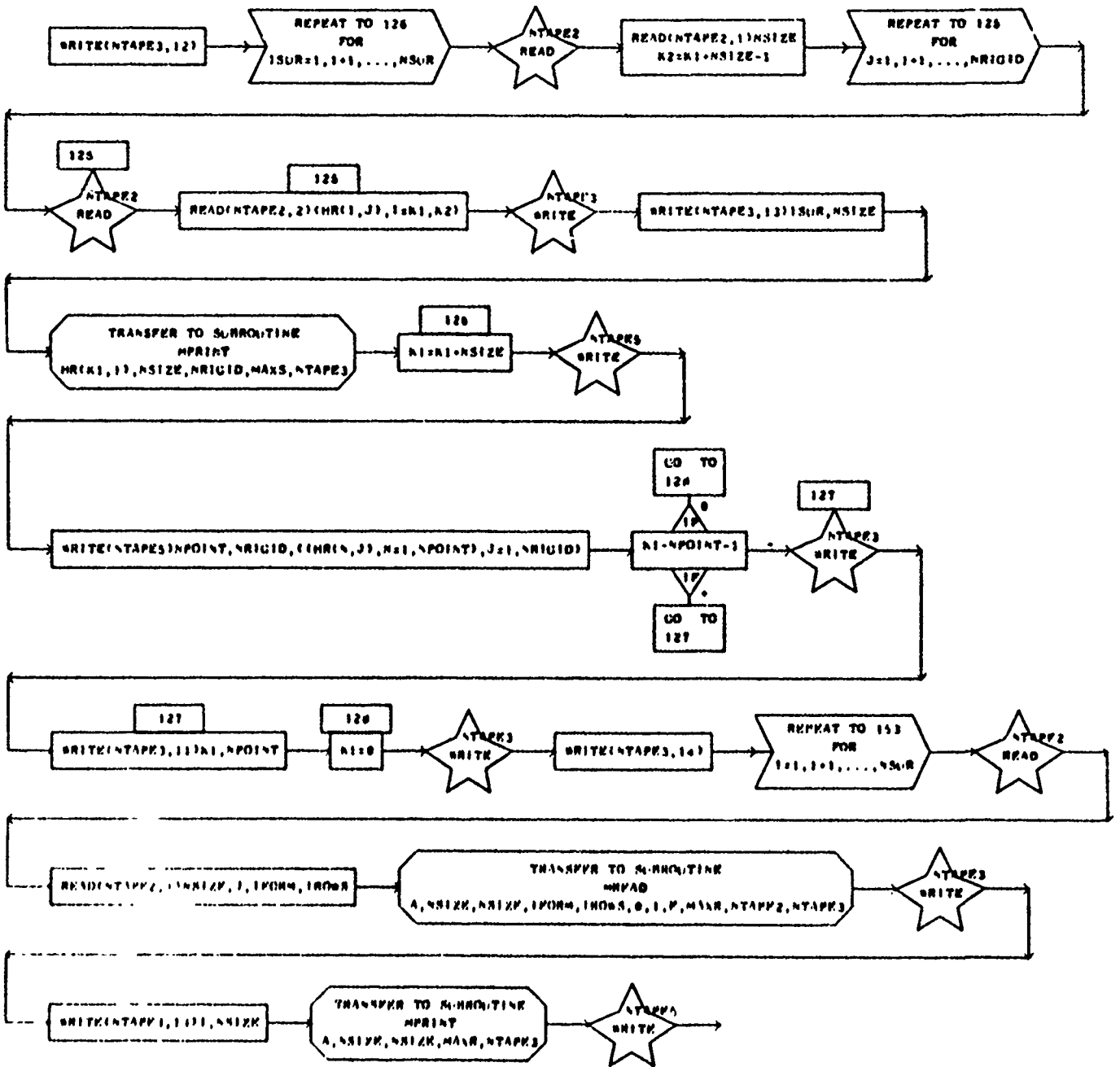
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ISIST	20	IS0	20	BR	21	S	21	RHO	20
DM	6,6	DO	6,12	DMSR	6,12	RARMR	6,12	LOS	50
I.HIGH	50	IT	210	VRLCTV	20	NRIZES	22	A	50,100
P	50,100	U	5,100	NR	50,6	HRT	6,100	MY	6,100
G	6,100								

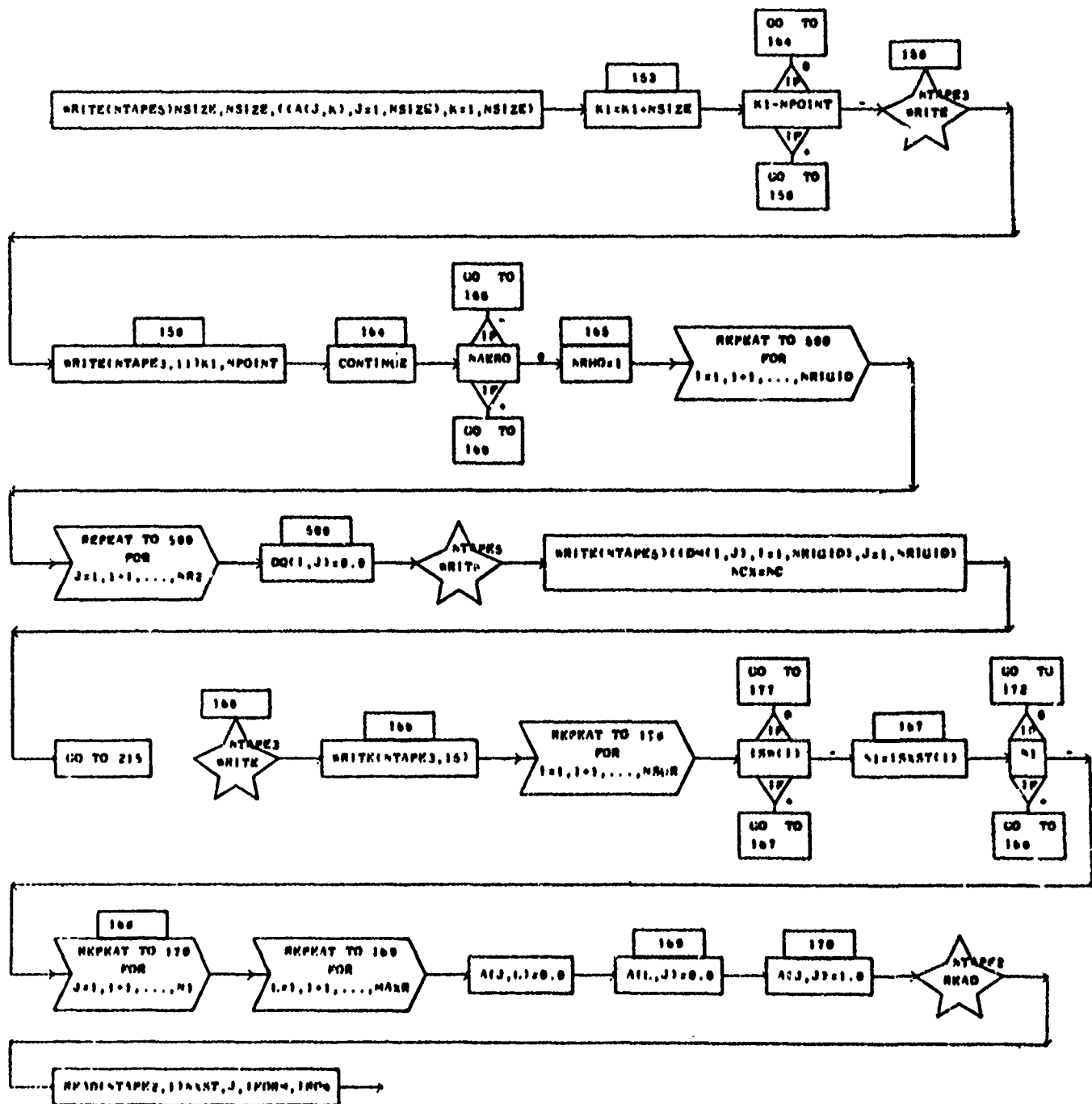


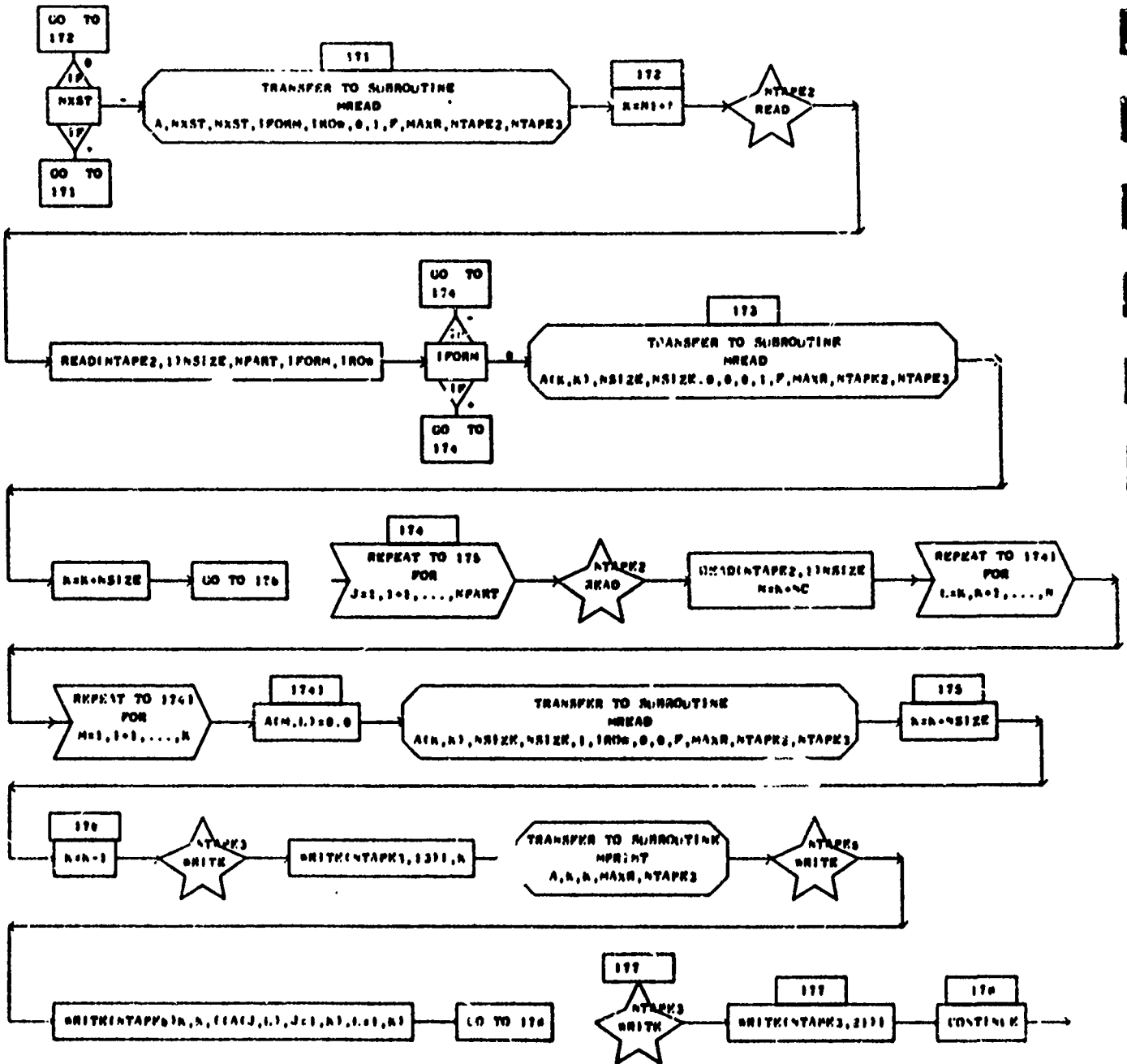


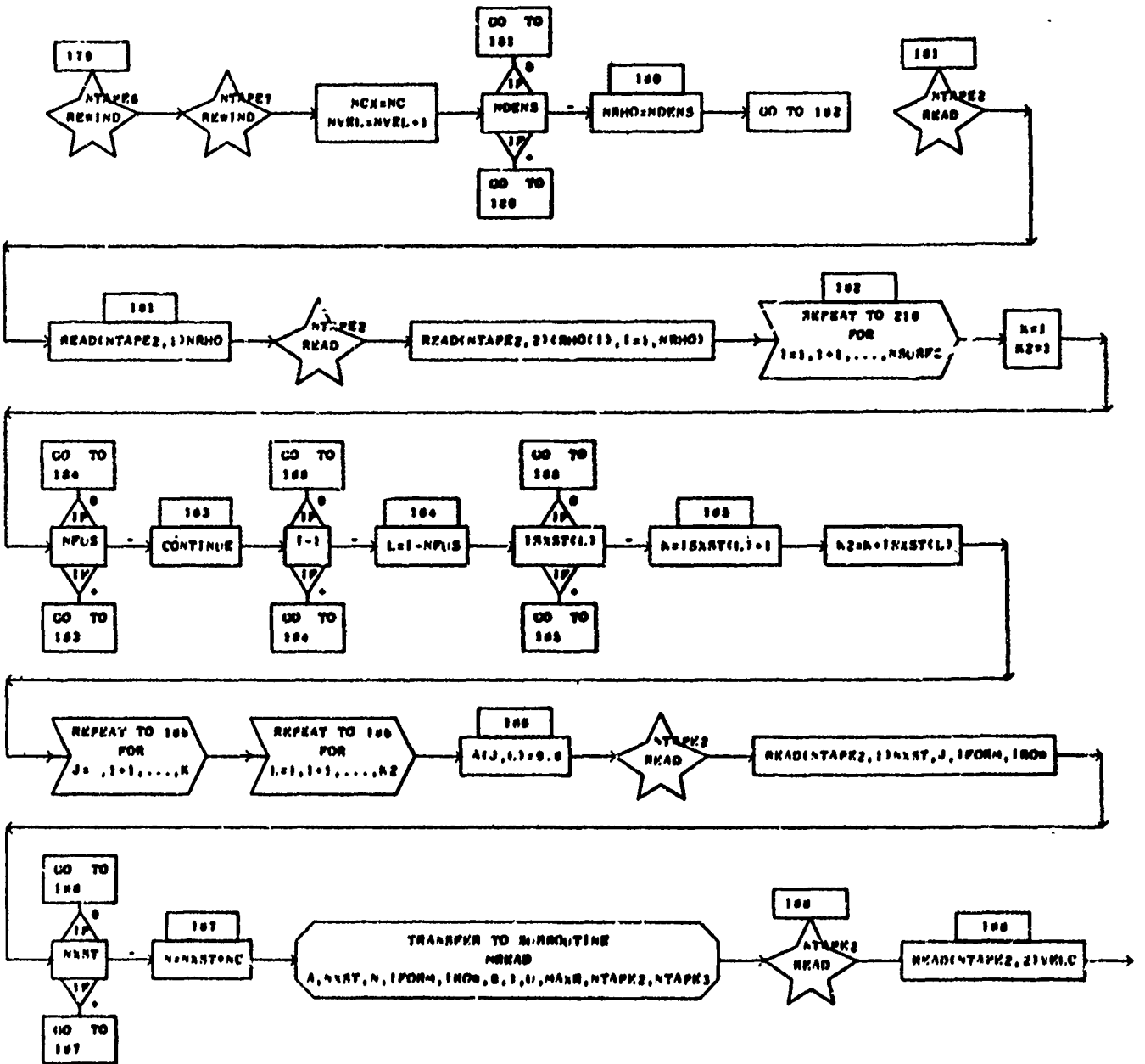


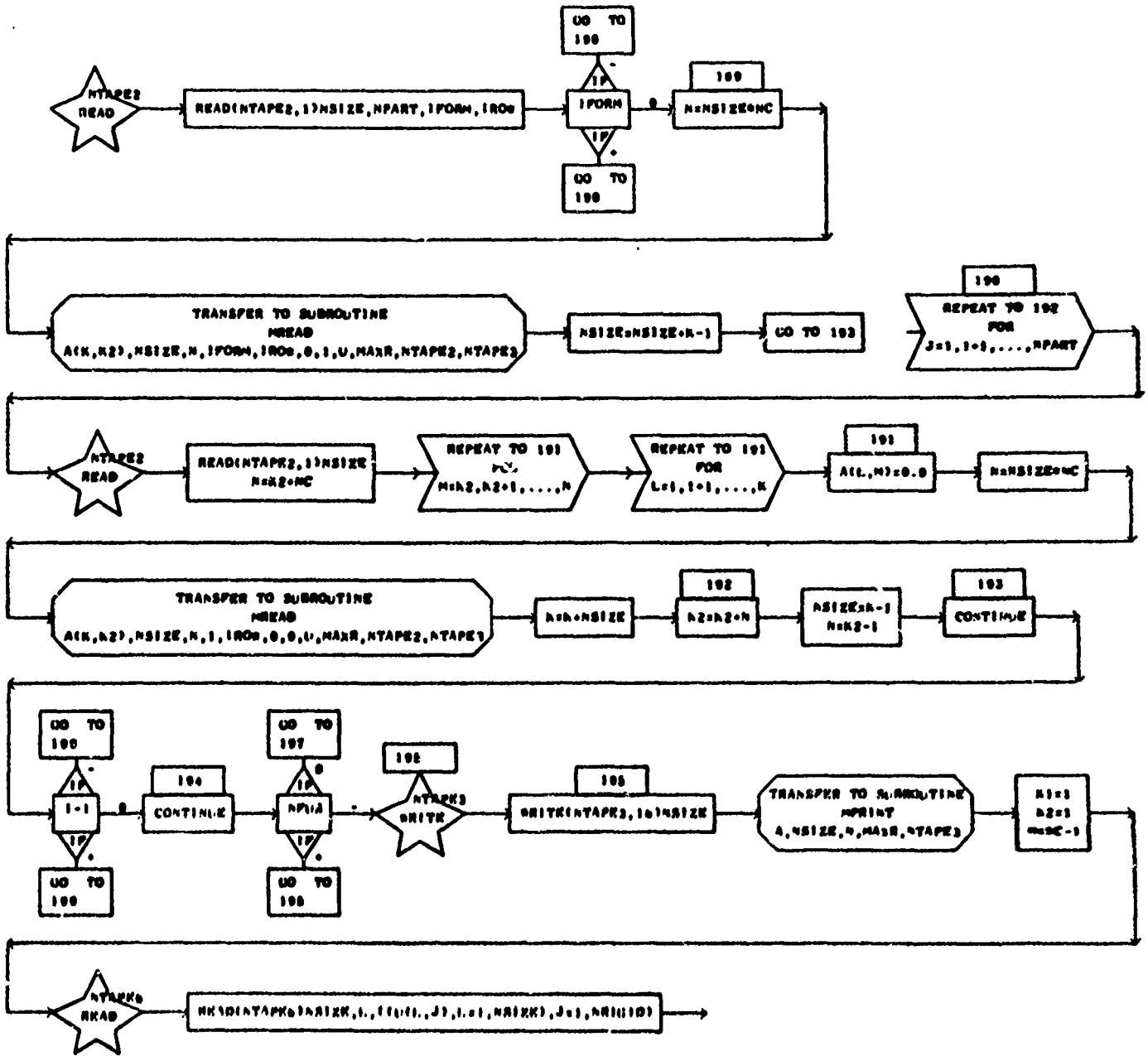


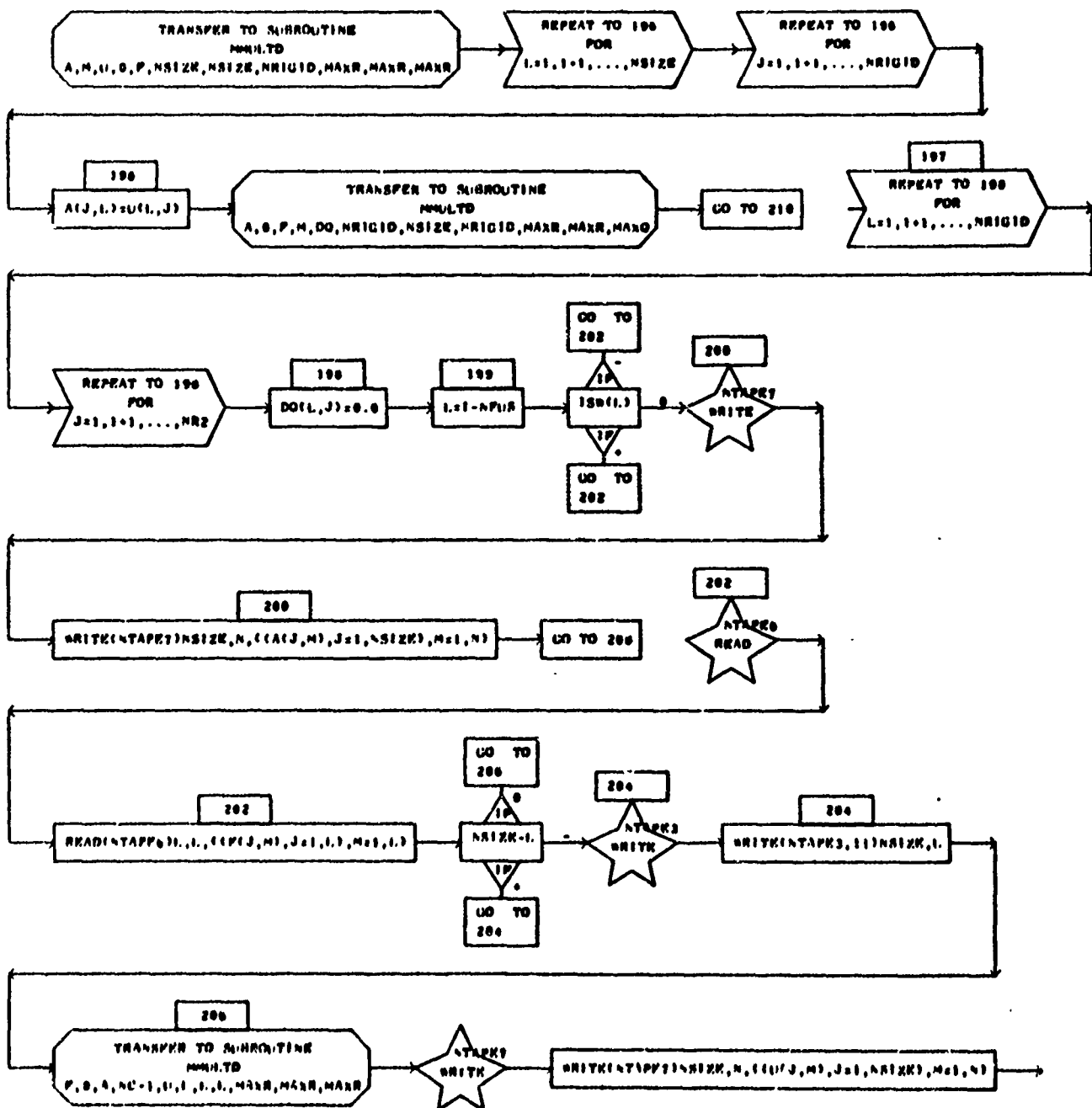


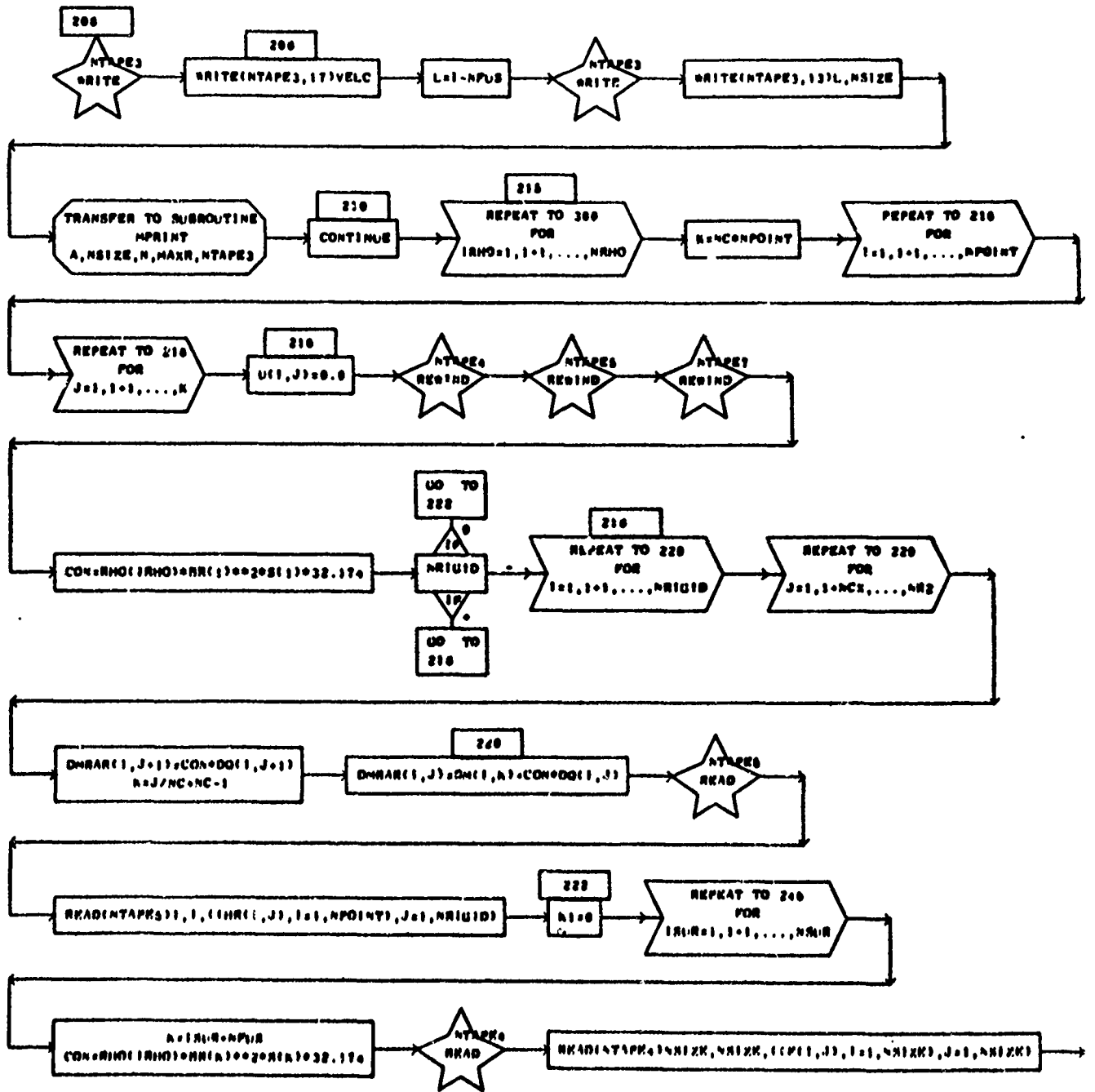


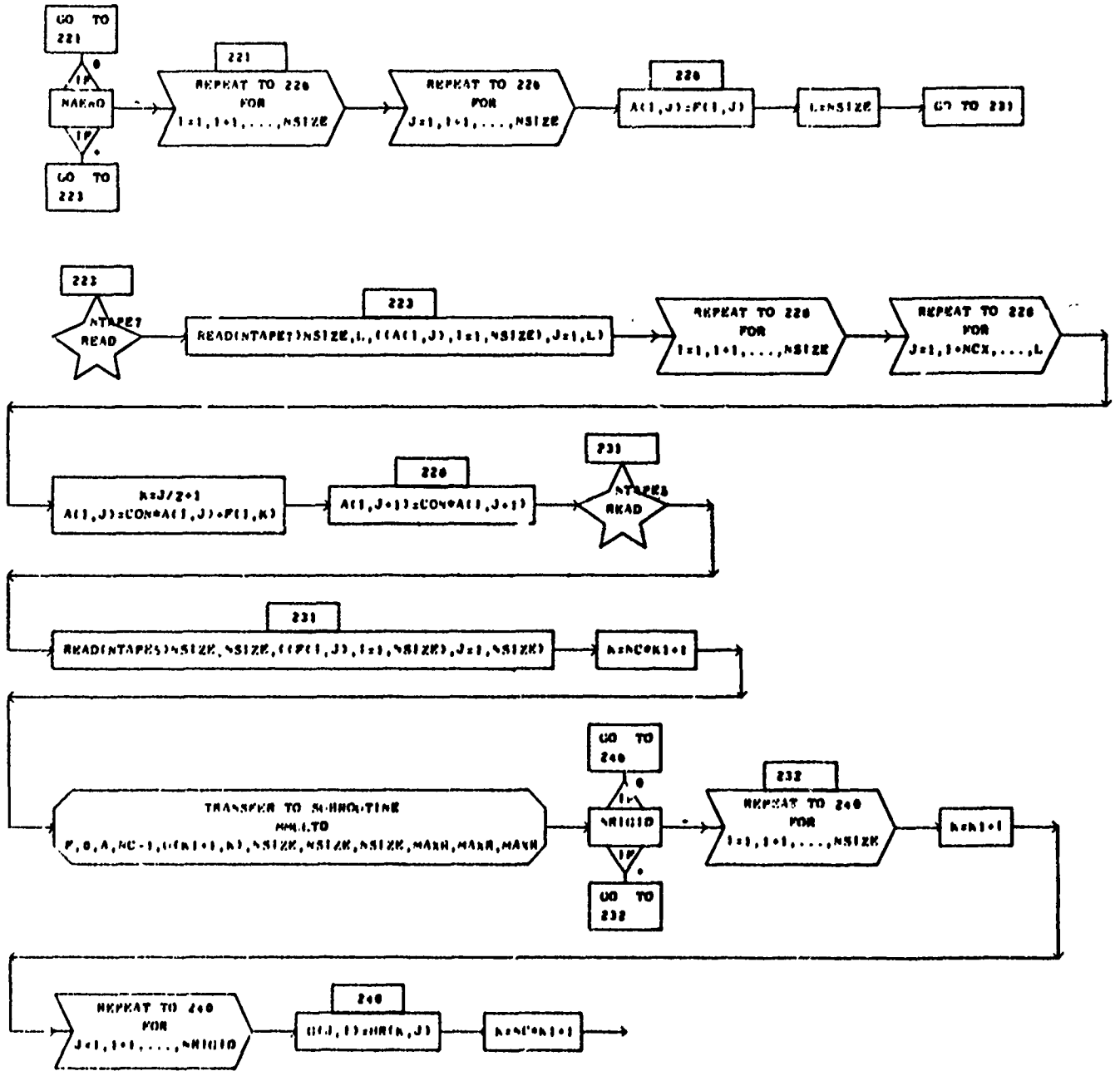


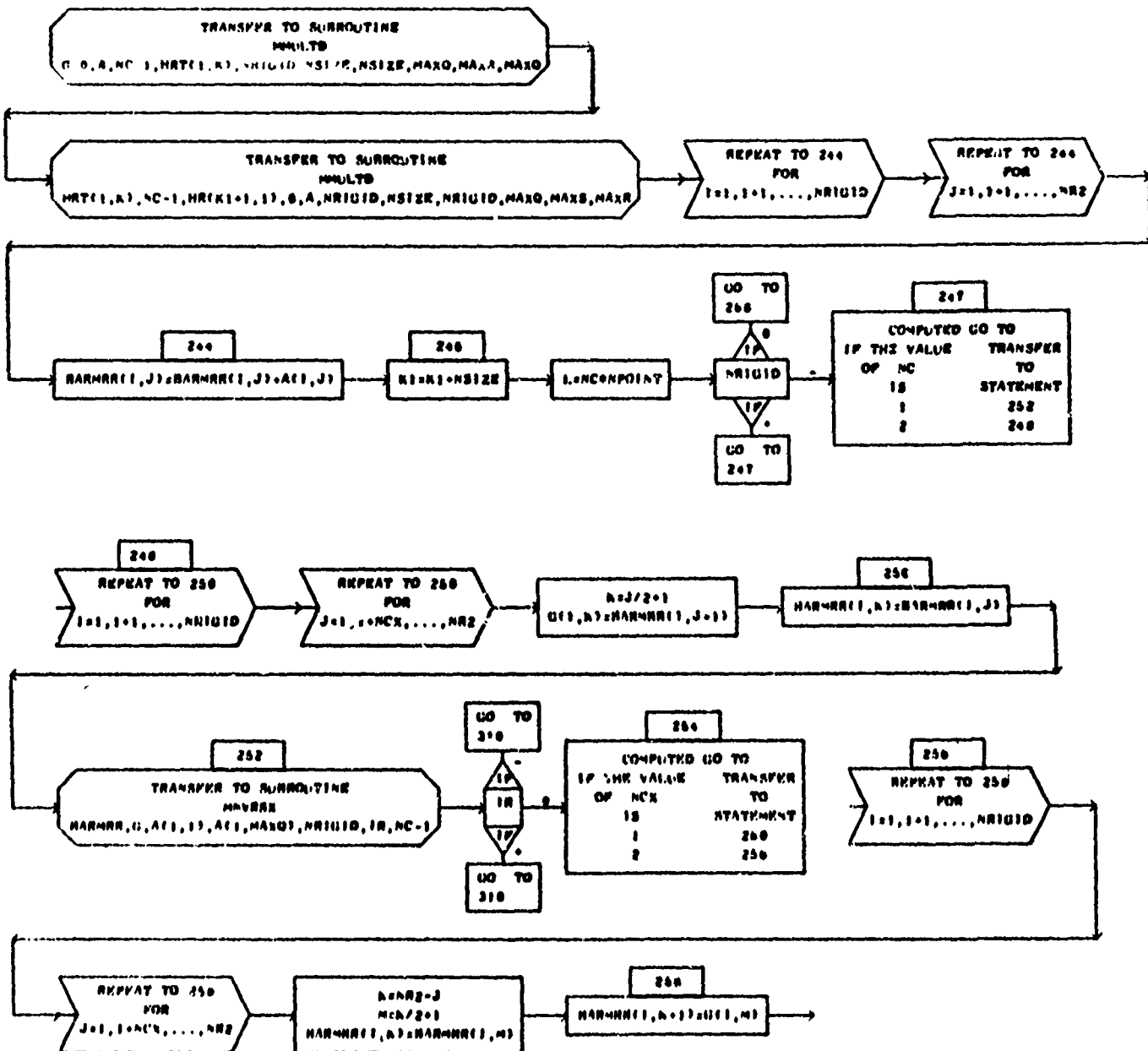


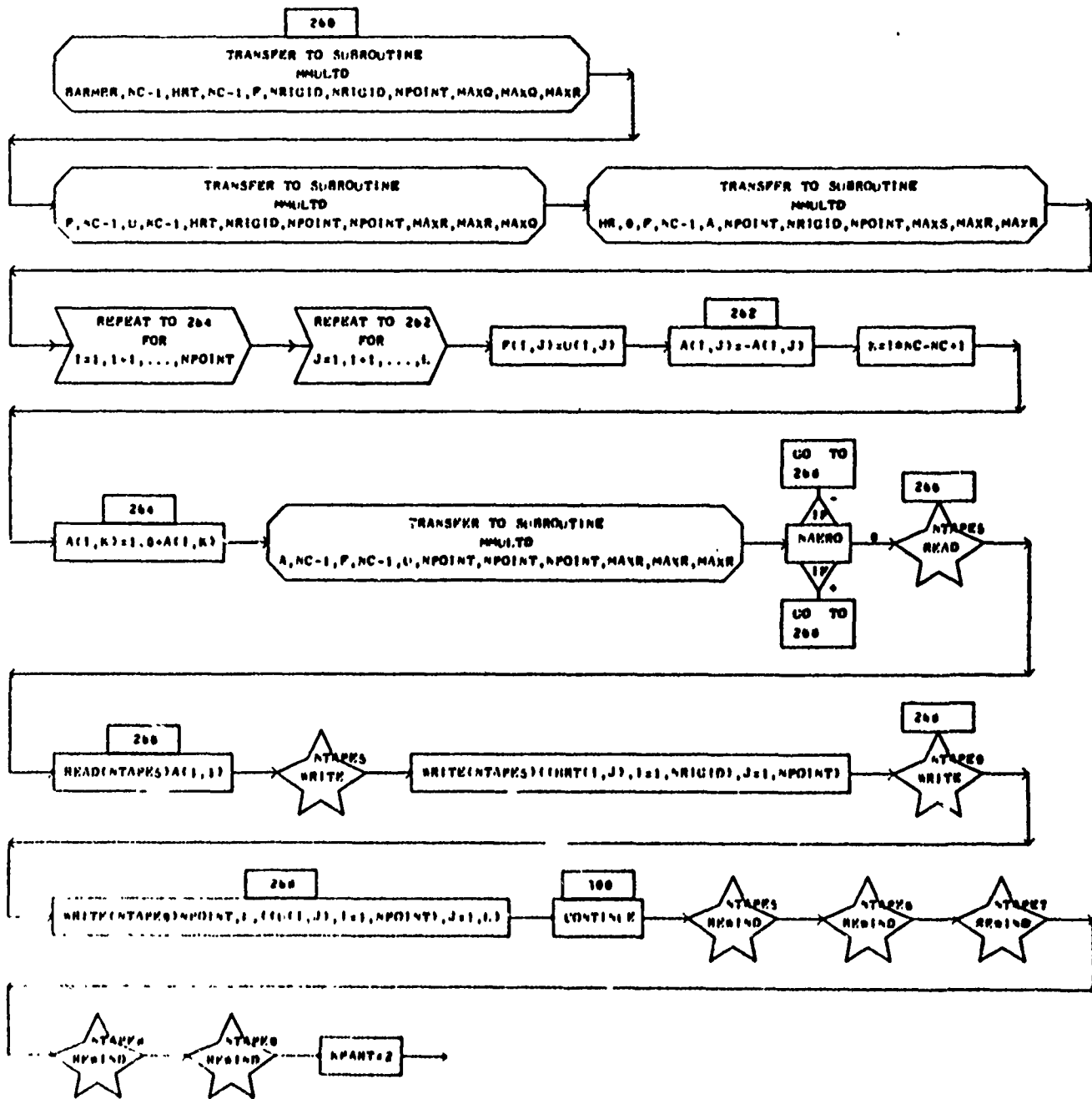


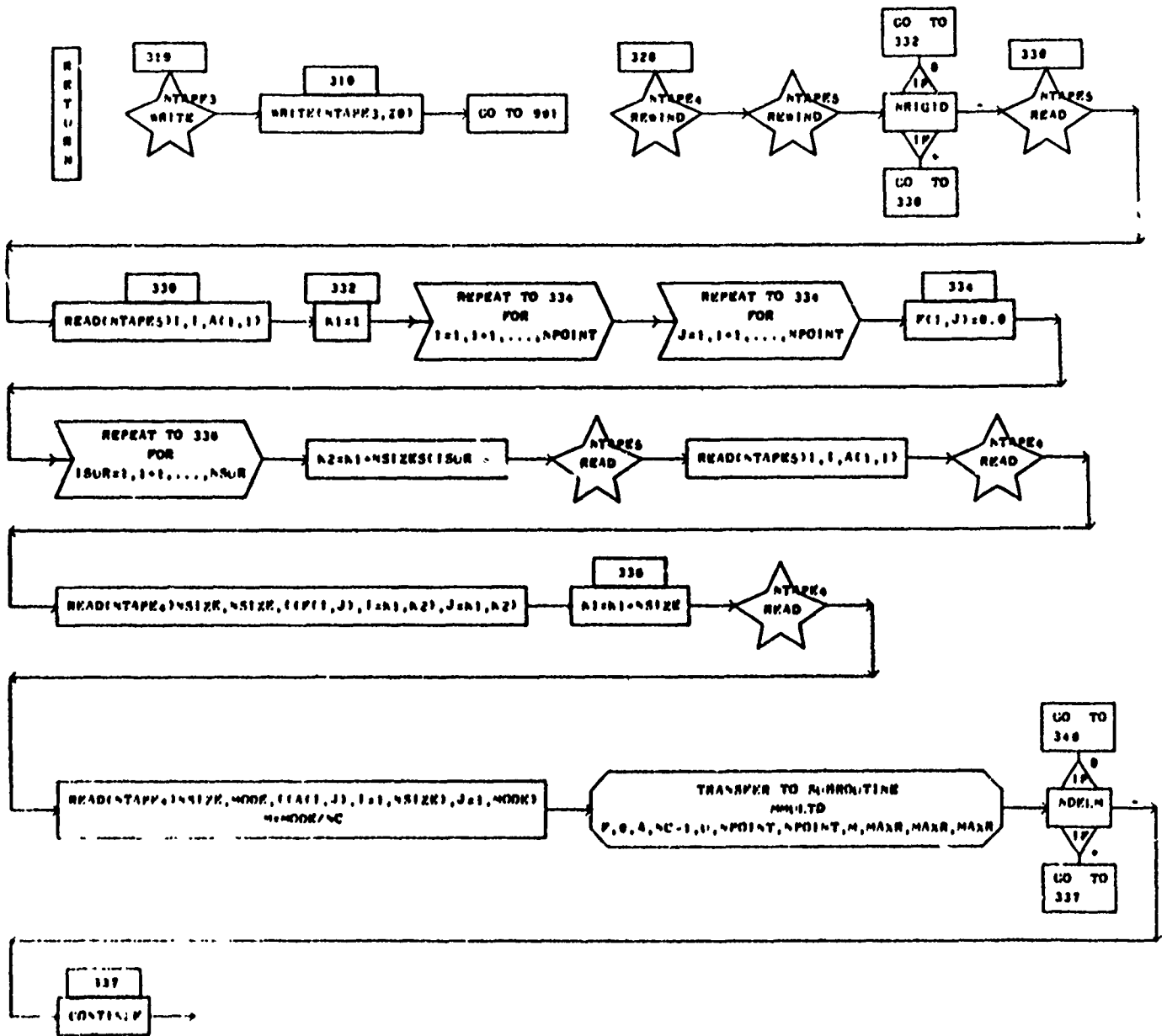


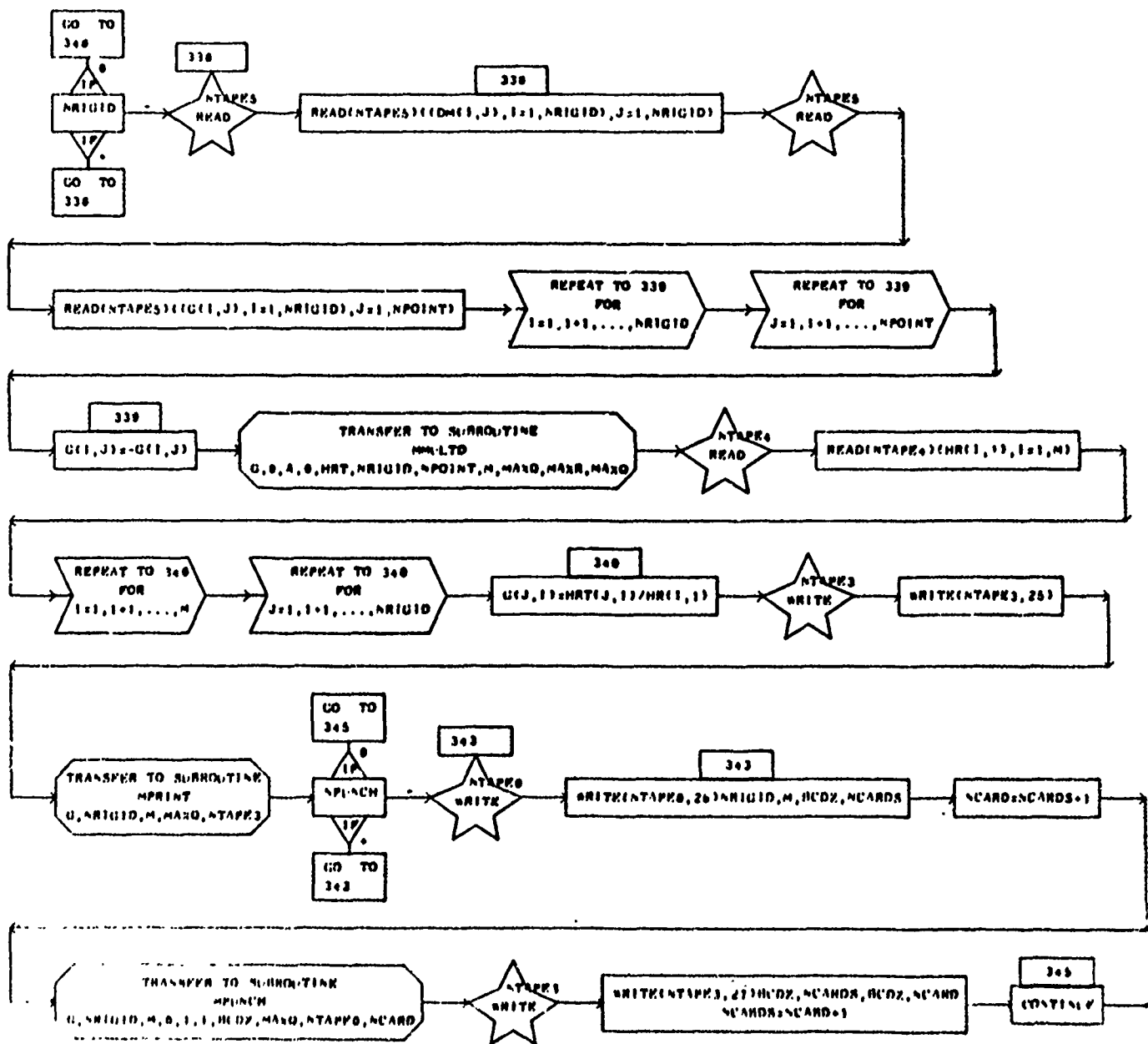


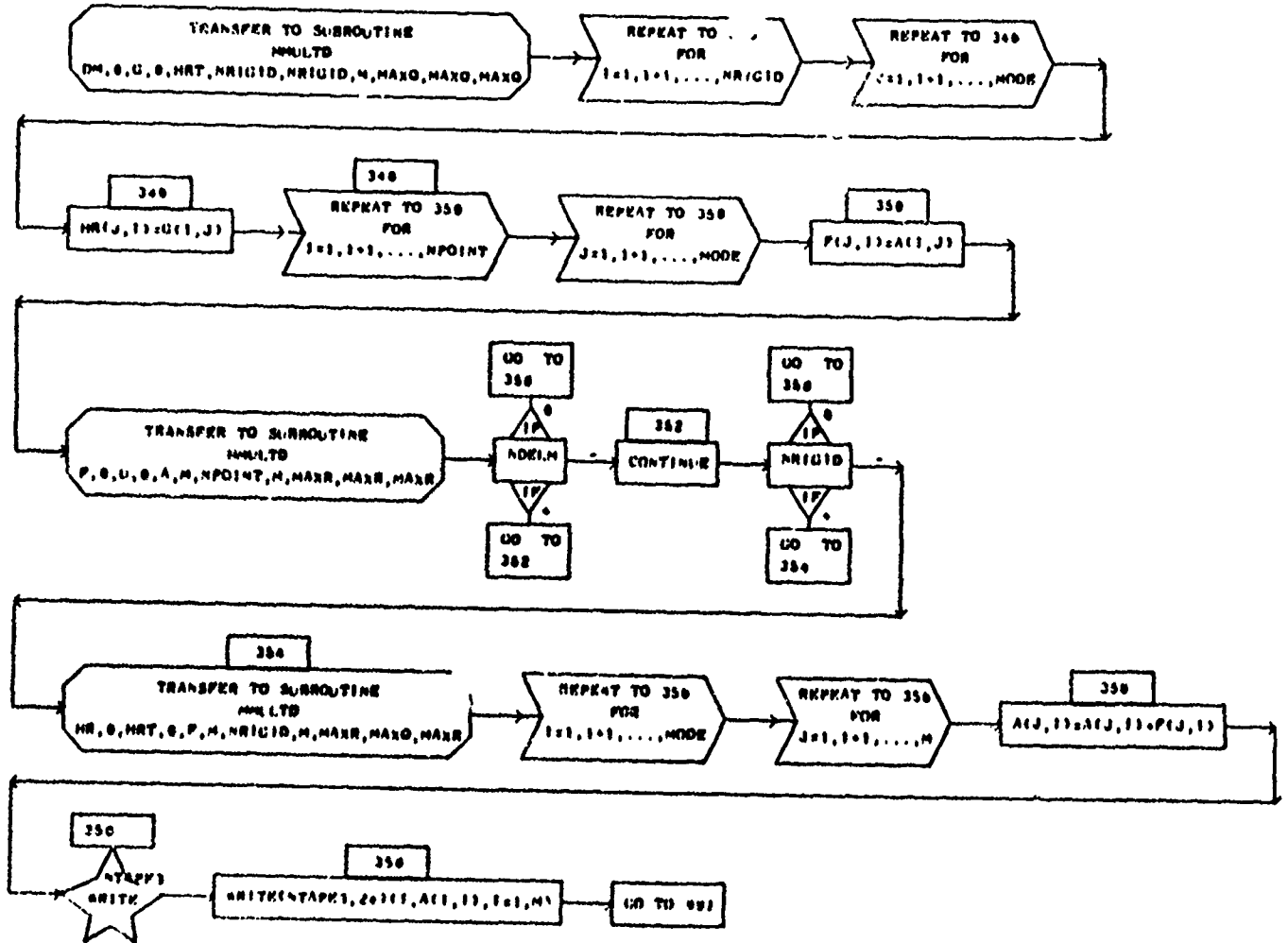












MREAD

MREAD

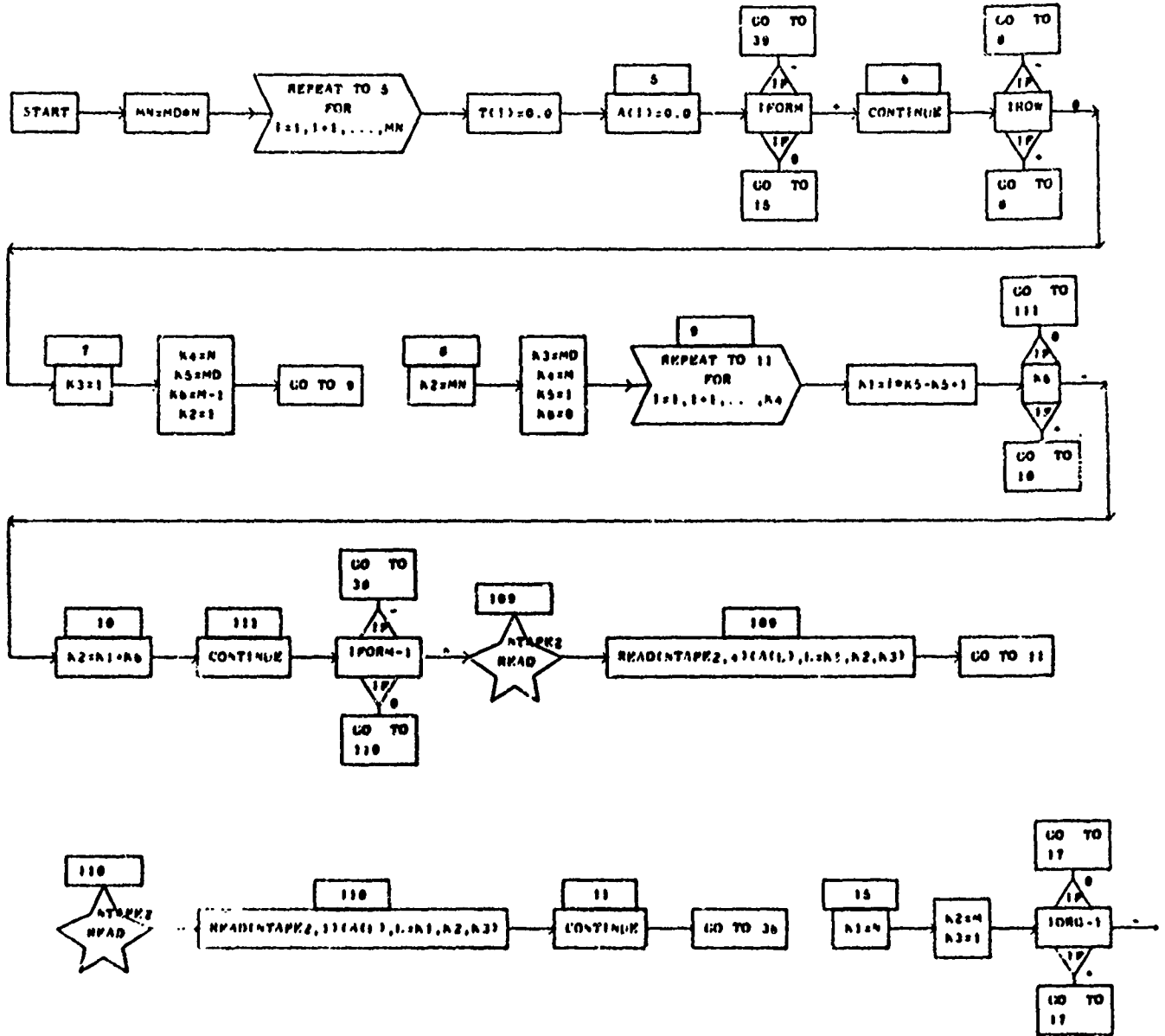
MATRIX READ SUBROUTINE

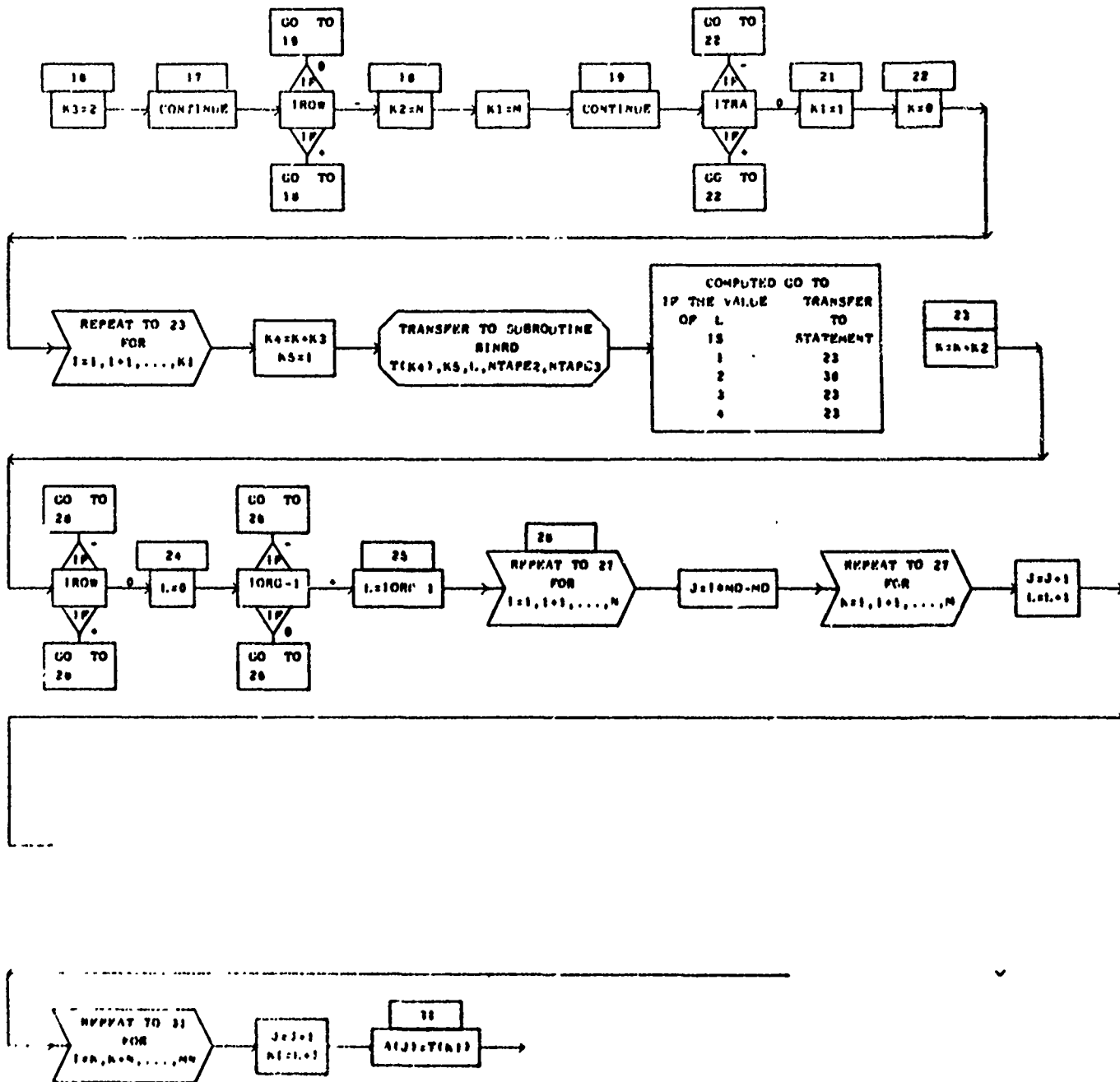
CALL MREAD (A,M,N,IFORM,IROW,ITRA,IORU,T,MO,NTAPE2,NTAPE3)

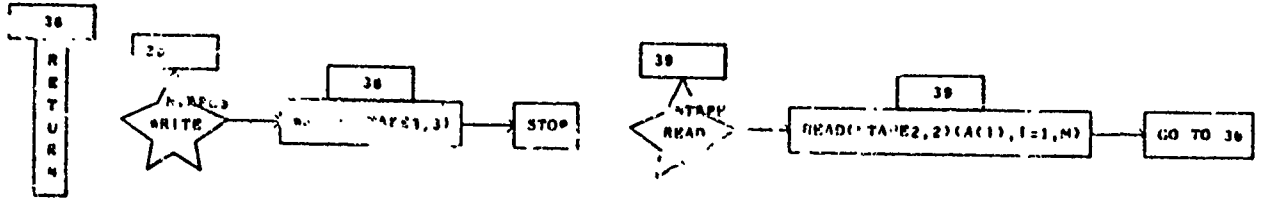
A = MATRIX TO READ IN ITRA = 0, TRA CARD AFTER MATRIX
M = NUMBER OF ROWS =+1, TRA CARD AFTER EACH ROW
N = NUMBER OF COLUMNS (OR COLUMN)
IFORM = -1, FORMAT(12A6) IORU = ORIGIN OF FIRST C.B. CARD
 = 0, COLUMN BINARY T = ONLY TEMPORARY CELLS
 = +1, FORMAT(5E12.6) MO = DIMENSIONED NUMBER OF ROWS
IROW = .0, MATRIX BY COLUMNS IN A
 = +1, MATRIX BY ROWS NTAPE2 = INPUT TAPE
 NTAPE3 = OUTPUT TAPE

D I M E N S I O N E D V A R I A B L E S

SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE
A	1	T	1						







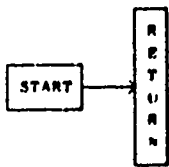
RINRD

D I M E N S I O N E D V A R I A B L E S

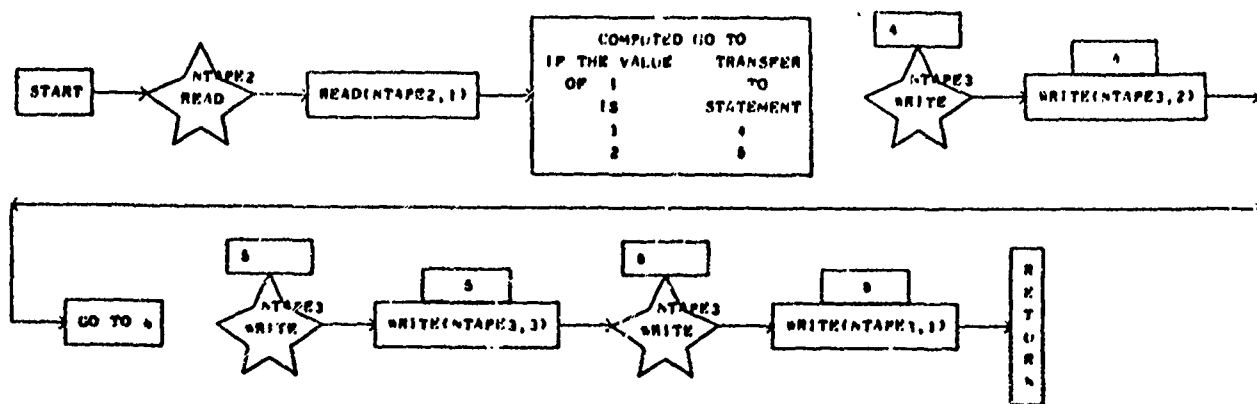
SYMBOL.	STORAGES	SYMBOL.	STORAGES	SYMBOL.	STORAGES	SYMBOL.	STORAGES	SYMBOL.	STORAGES
T	1								

SUBROUTINE INRO (T,K,L,NTAPE1,NTAPE2)

PAGE 1



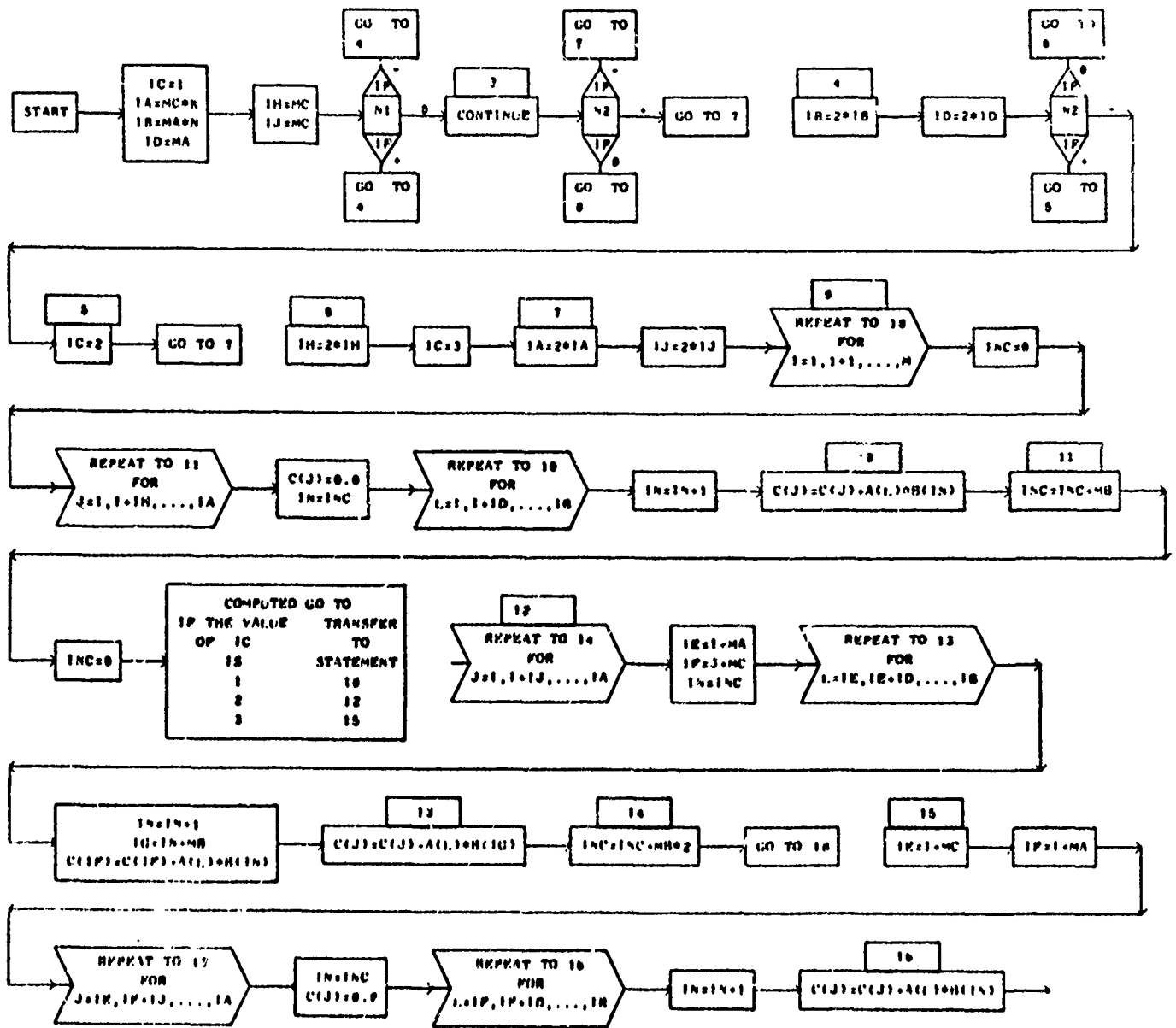
SUBROUTINE RDLN (NTAPE2, NTAPE3, I)

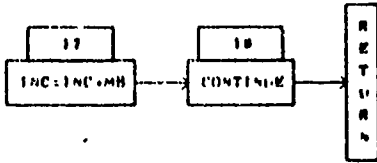


MULTO

D I M E N S I O N E D V A R I A B L E S

SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE
A	1	B	1	C	1				

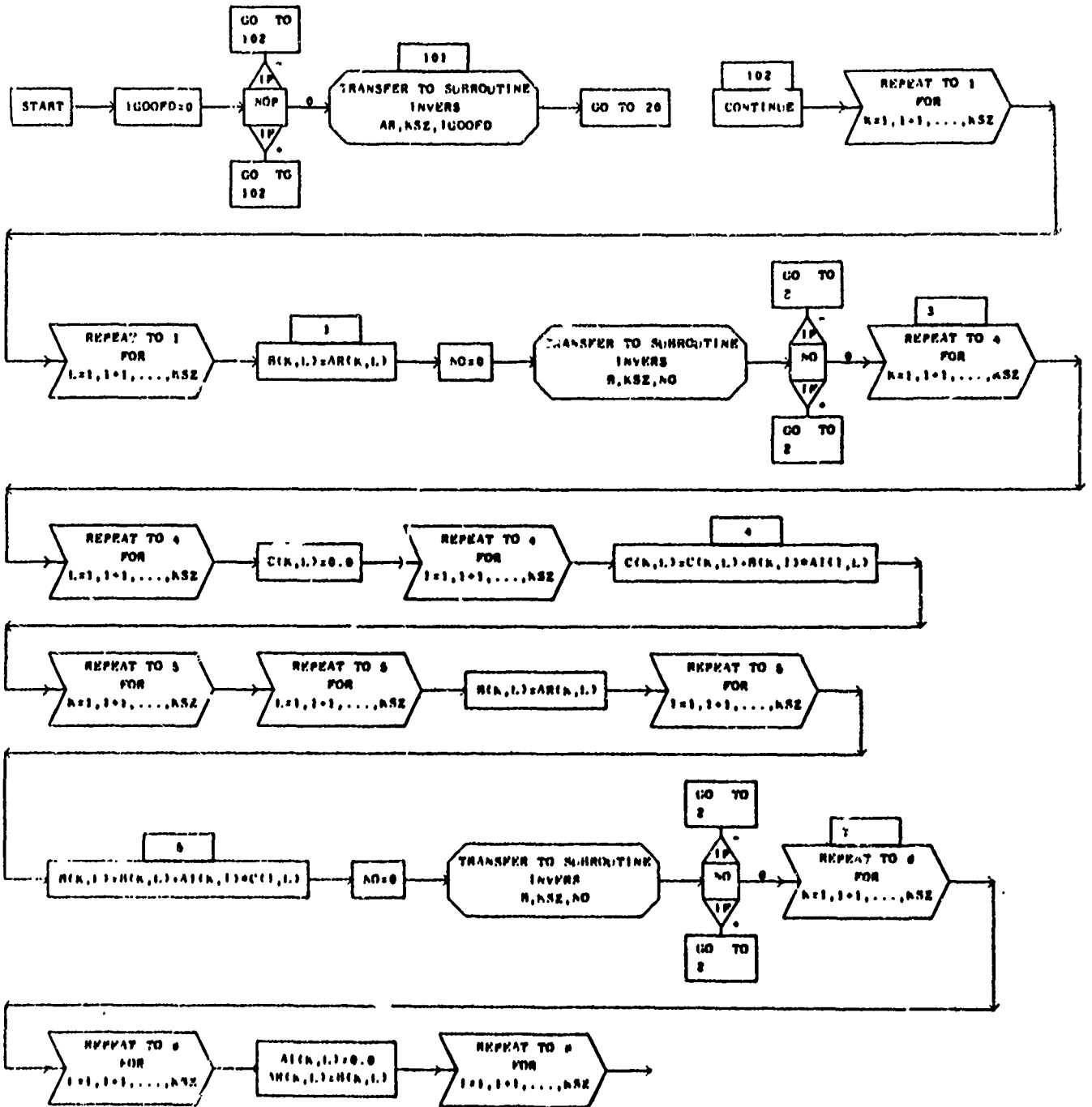


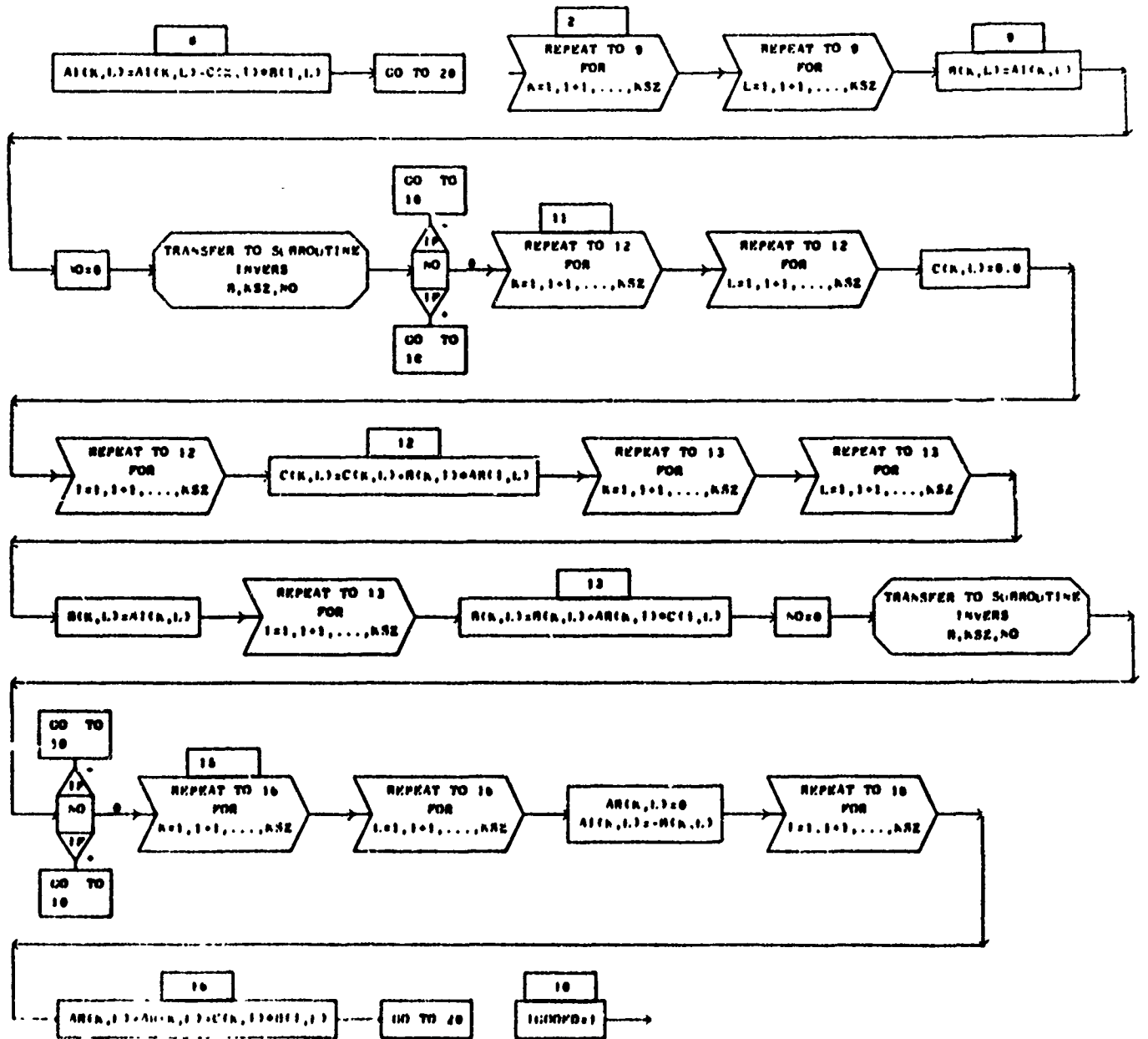


MNVRSS

D I M E N S I O N E D V A R I A B L E S

SYMBOL	STORAGES	SYMBOL	STORAGES	SYMBOL	STORAGES	SYMBOL	STORAGES	SYMBOL	STORAGES
AR	0,0	AI	0,0	B	0,0	C	0,0		





SUBROUTINE MNVRSX (AR,A1,B,C,KSZ,IGOOPD,NOP)

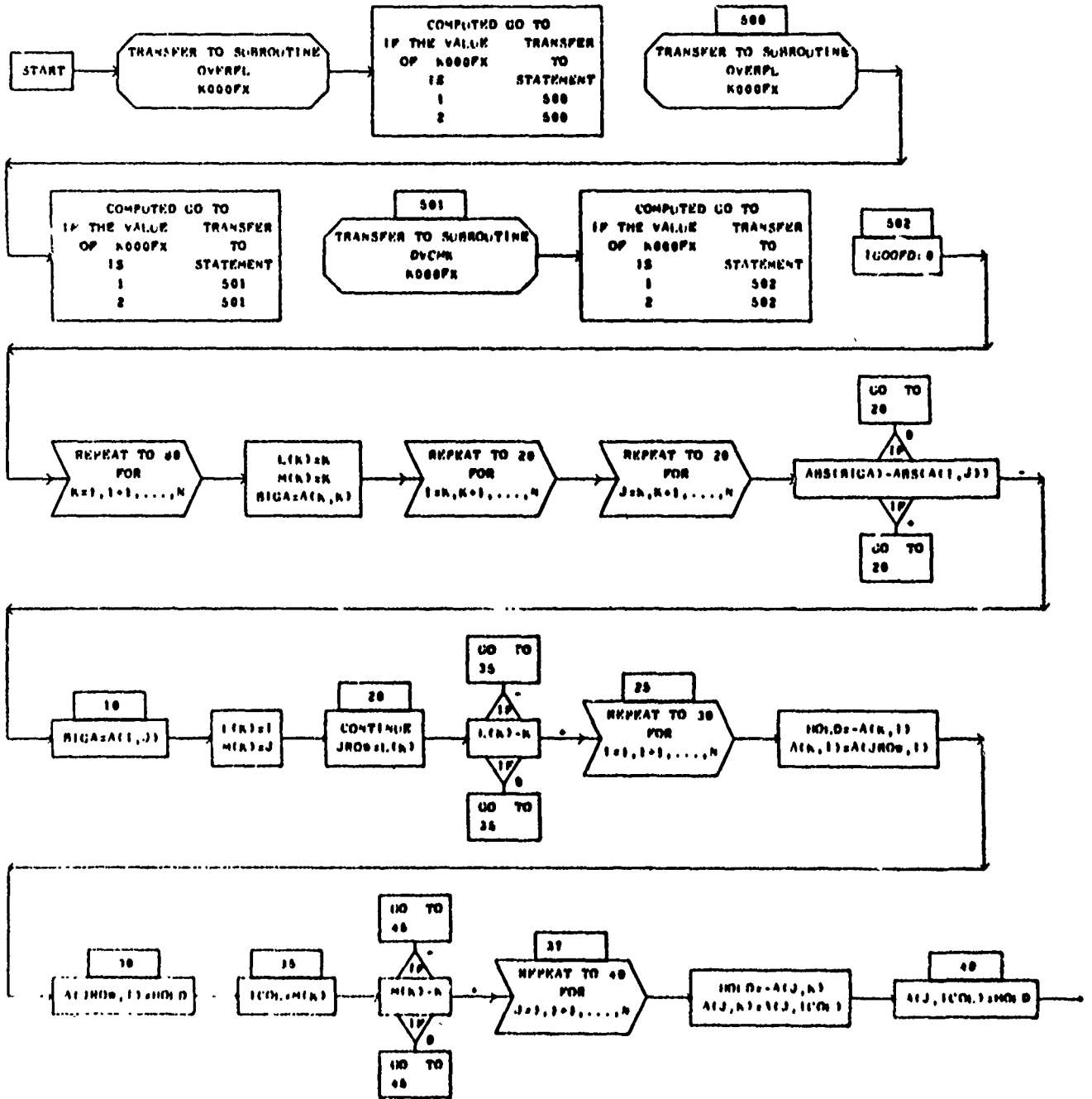
PAGE 3

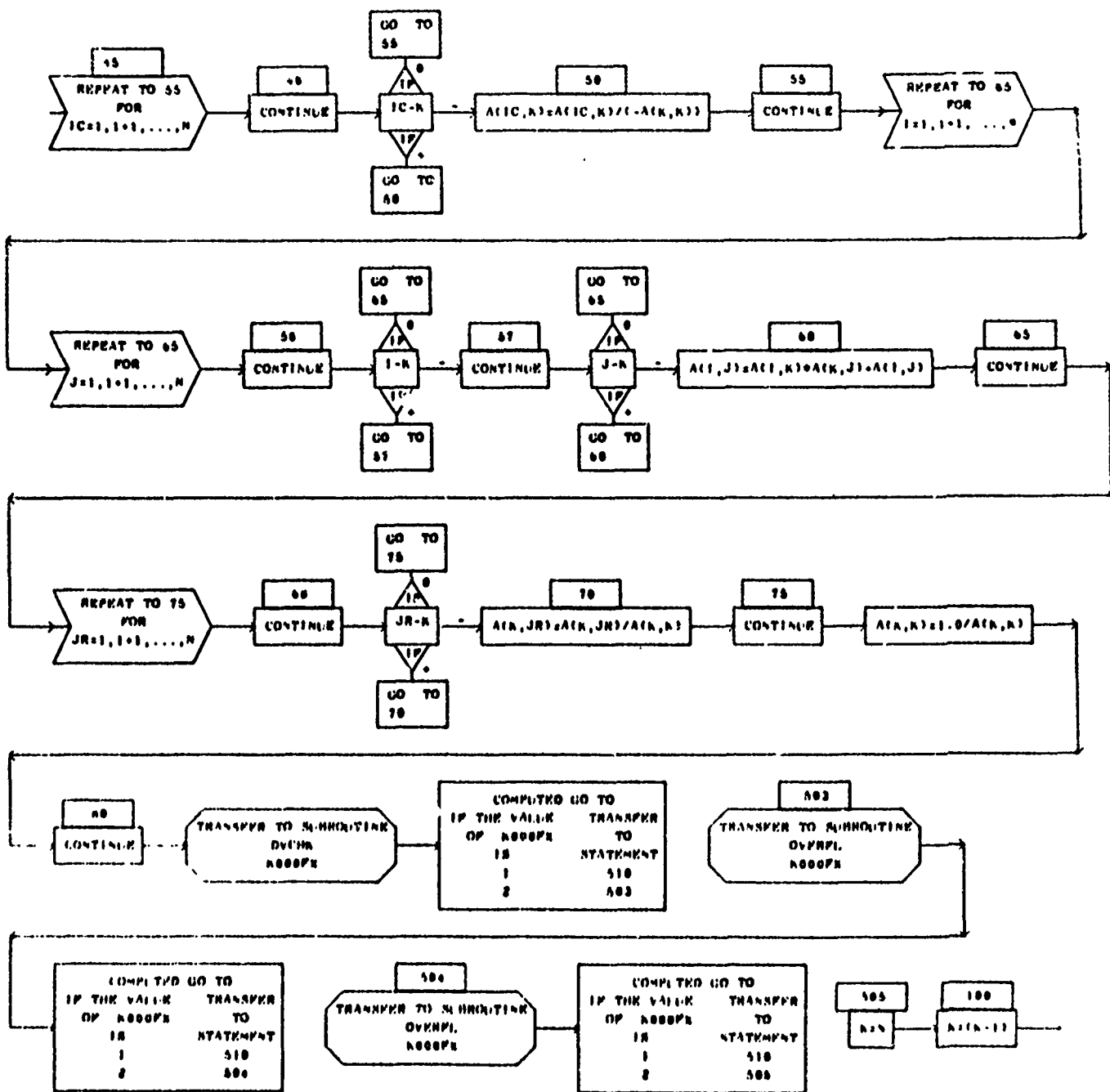
20
R
E
T
U
R
N

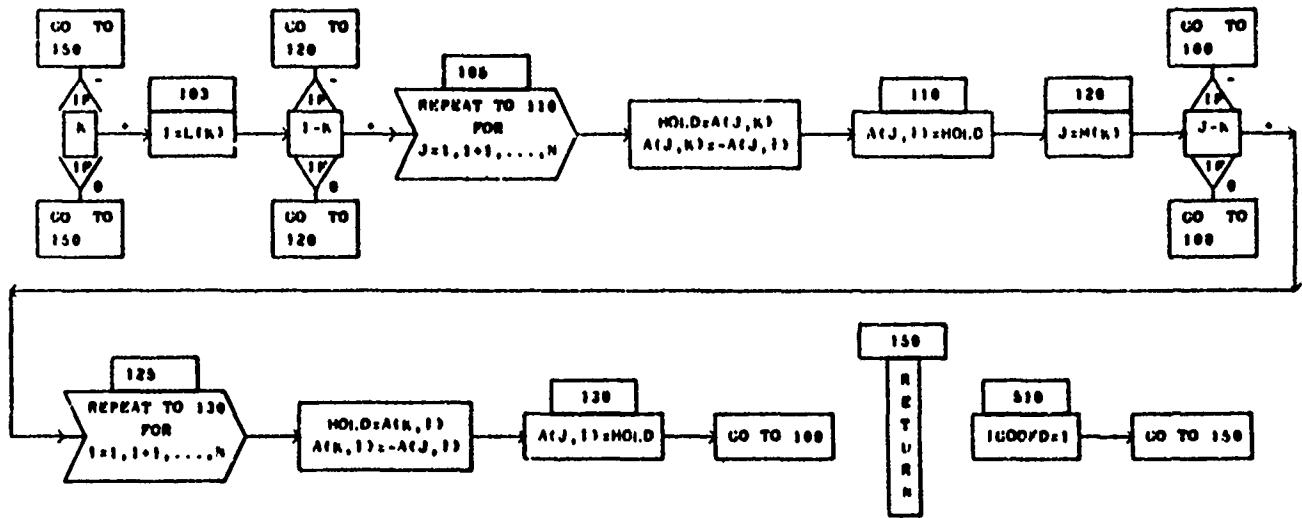
INVERS

D I M E N S I O N E D V A R I A B L E S

SYMBOL.	STORAGES	SYMBOL.	STORAGES	SYMBOL.	STORAGES	SYMBOL.	STORAGES	SYMBOL.	STORAGES
A	0,0	L	0	M	0				



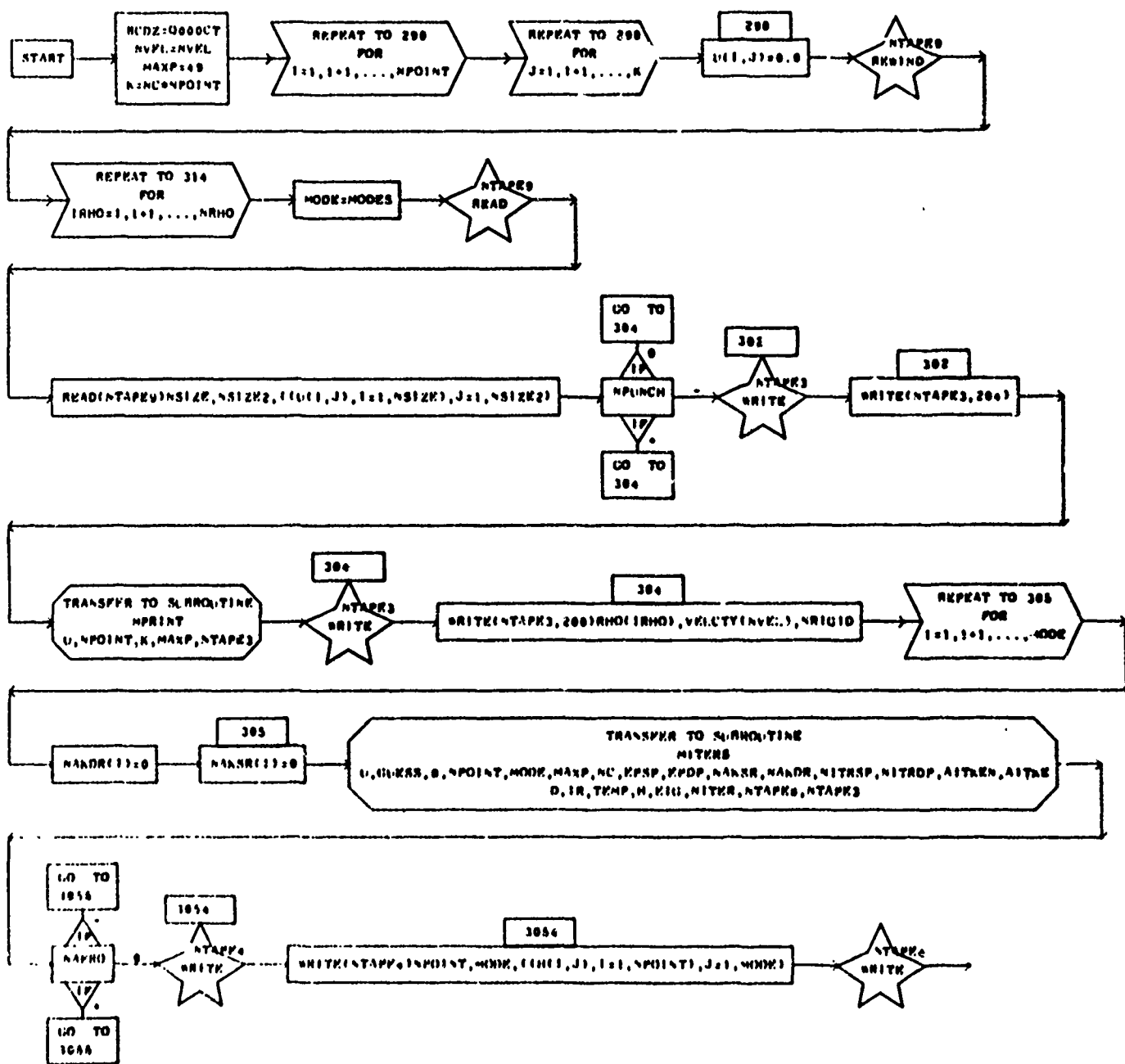


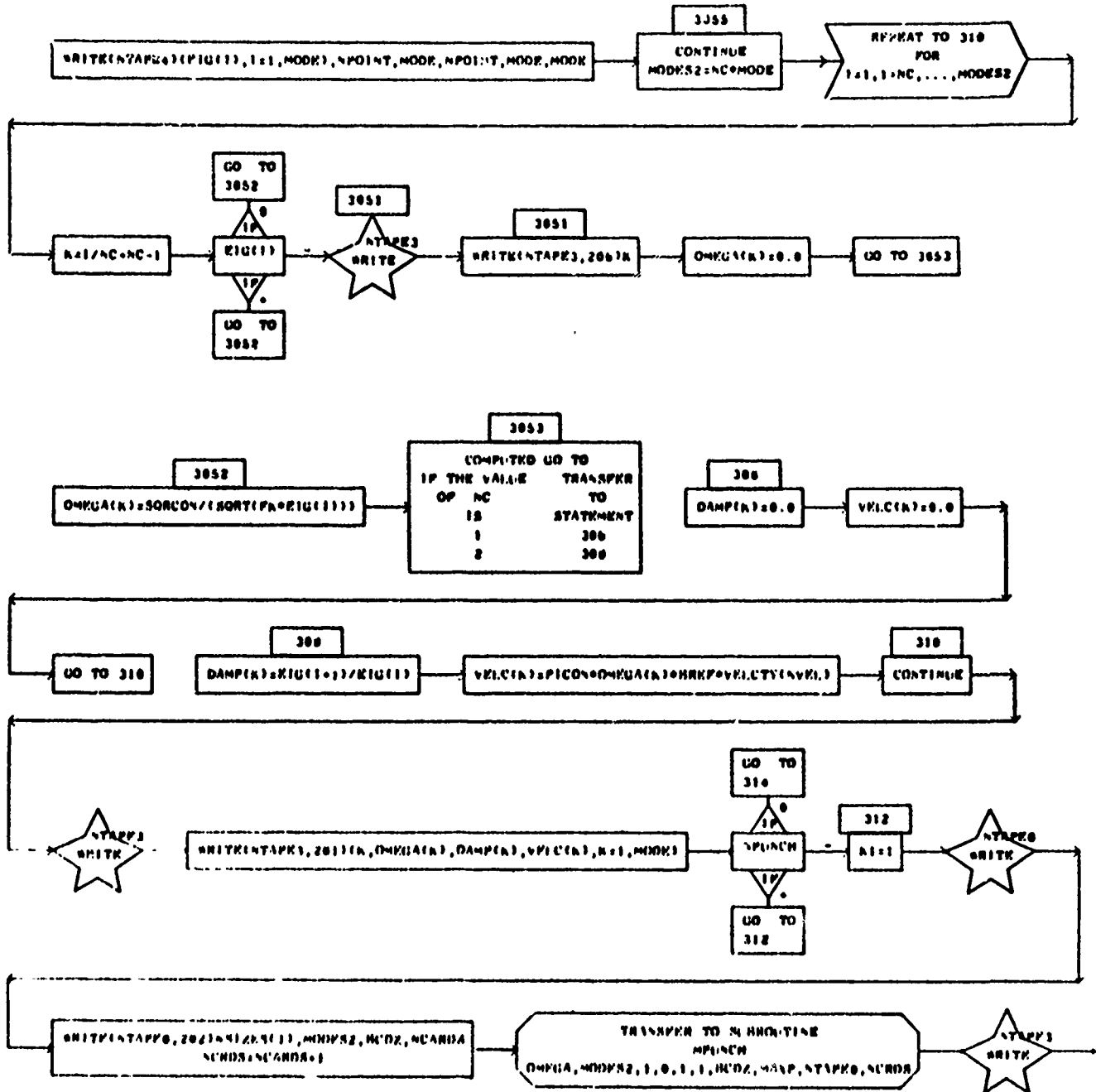


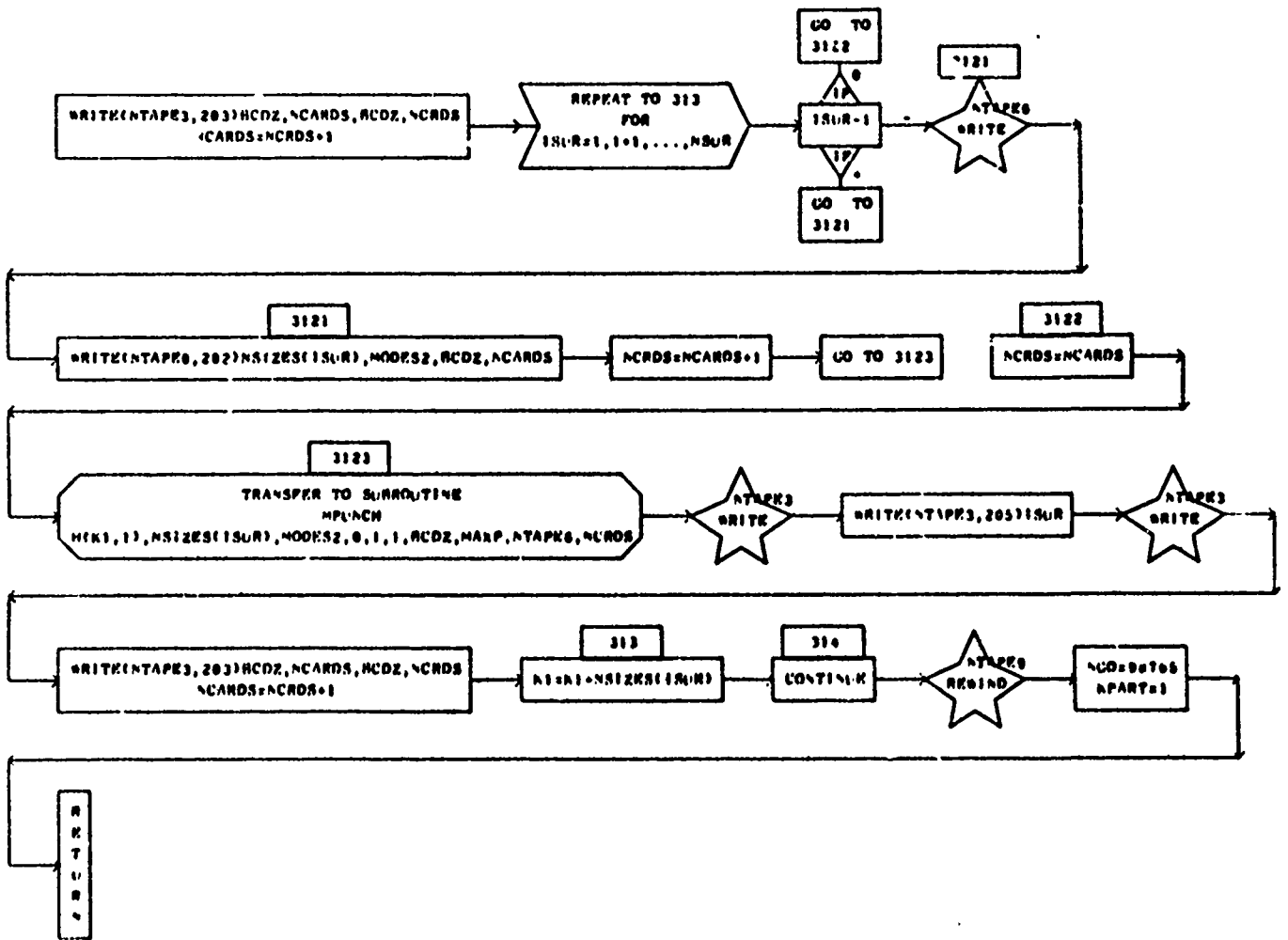
PART 2

D I M E N S I O N E D V A R I A B L E S

SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE
IT	216	VFLCTY	20	NSIZES	20	DN	6.0	RND	20



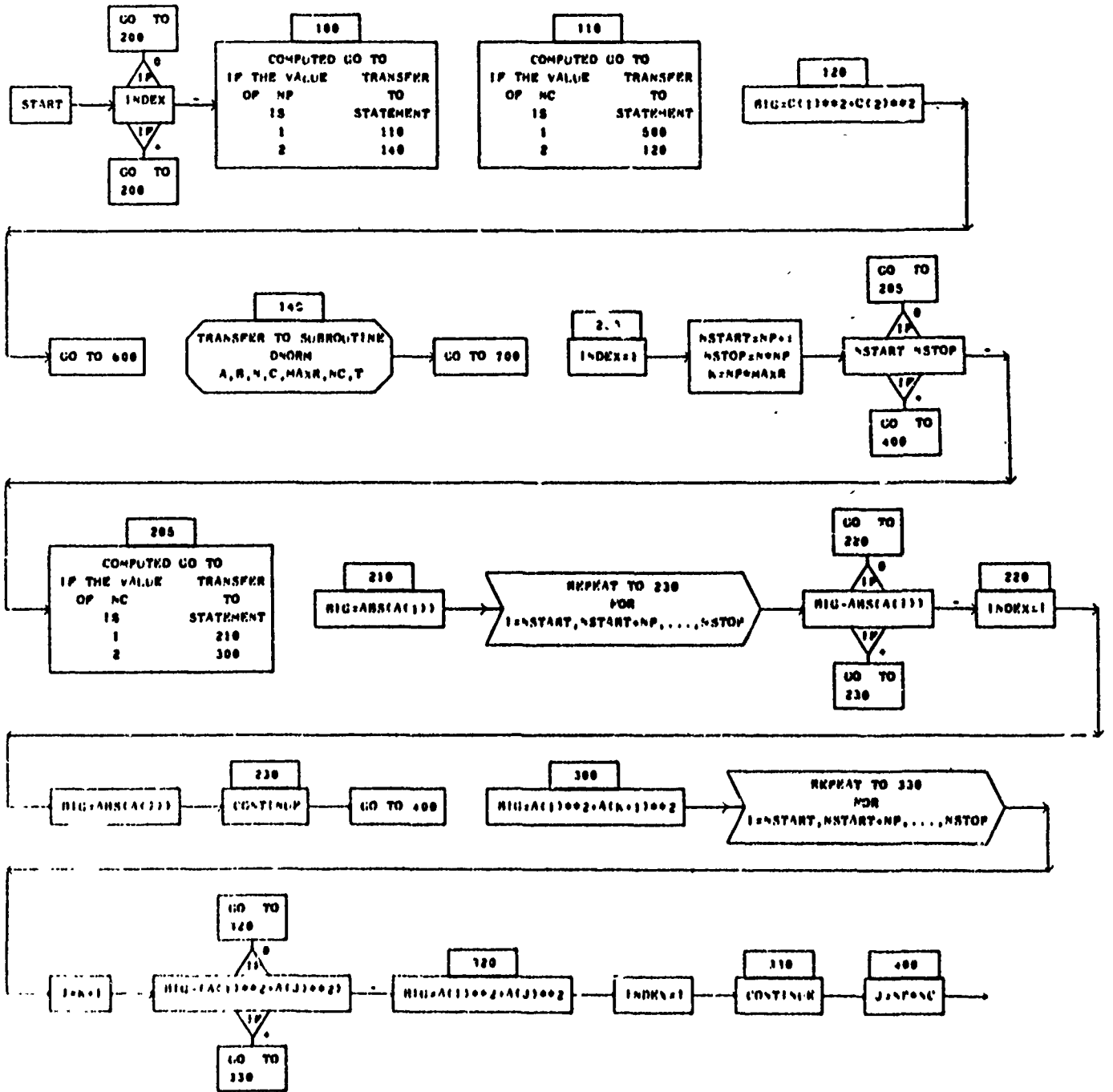


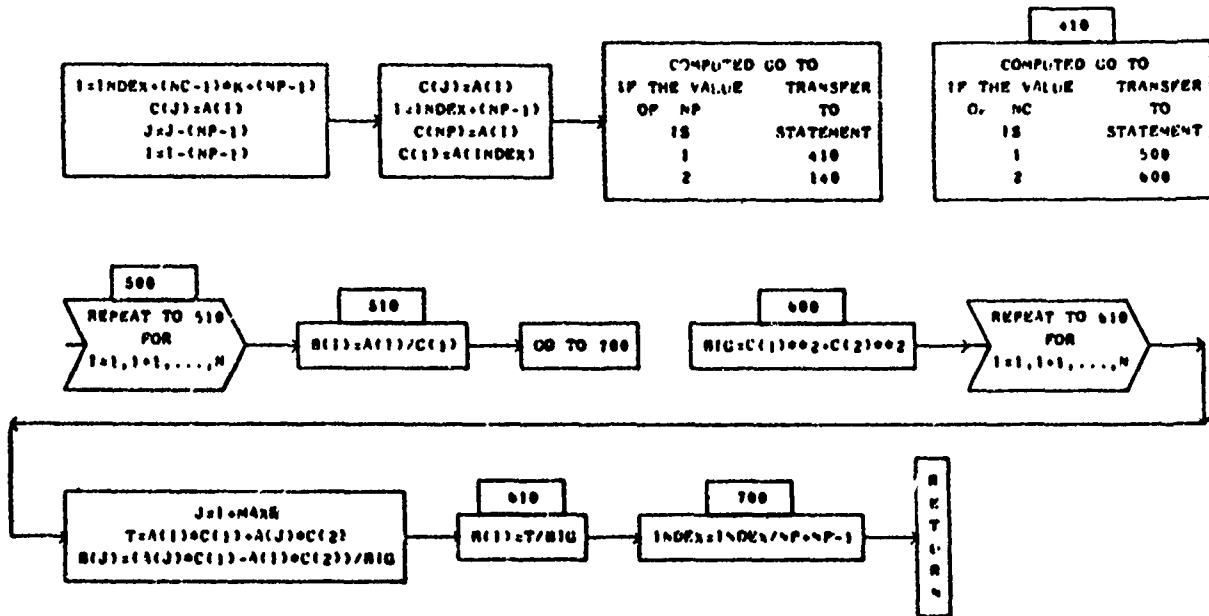


NORHE

D I M E N S I O N E D V A R I A B L E S

SYMBOL	STORAGES	SYMBOL	STORAGES	SYMBOL	STORAGES	SYMBOL	STORAGES	SYMBOL	STORAGES
A	1	B	1	C	1	T	2		

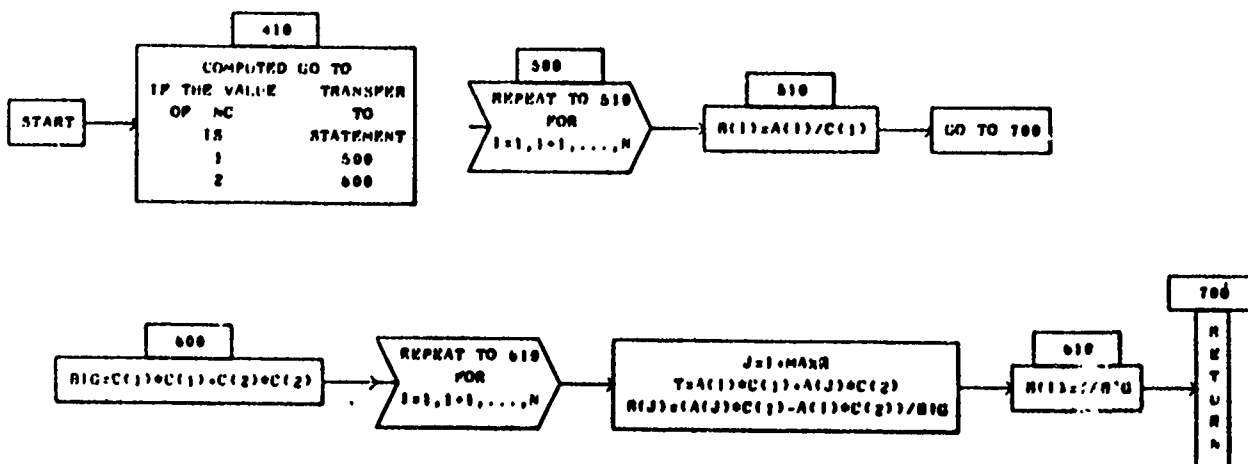




DNORME

SUBROUTINE DNORM (A,B,N,C,MAXR,NC,T)

PAGE 1



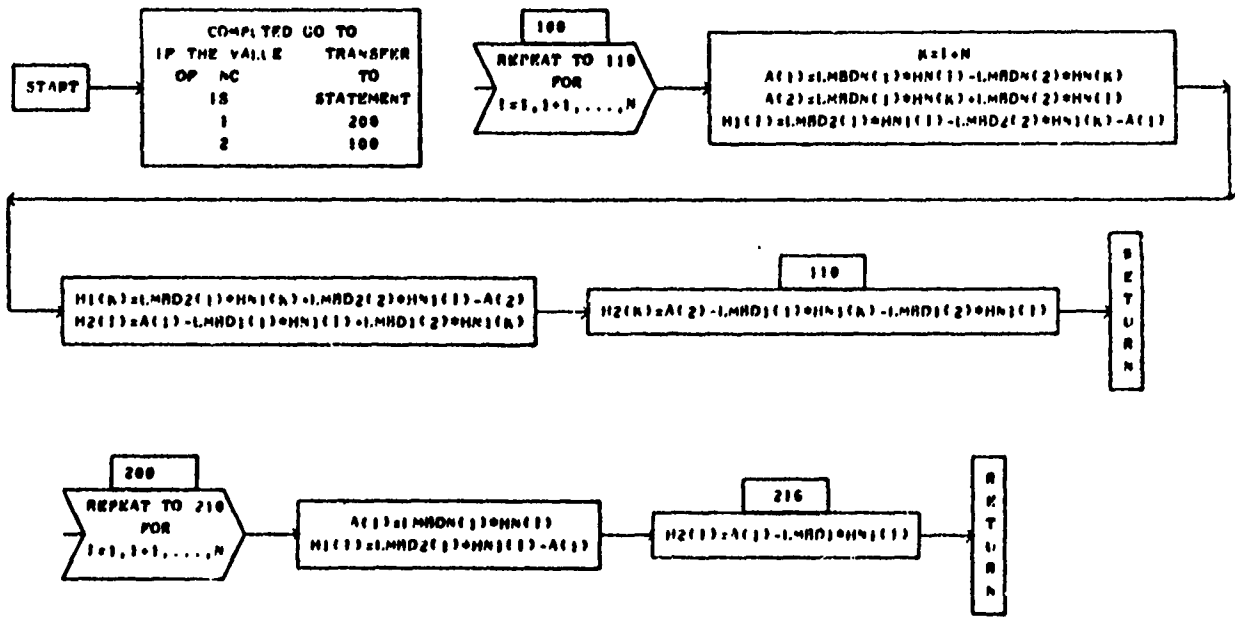
POH3

D I M E N S I O N E D V A R I A B L E S

SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE
LMBDN	1	LMD1	1	LMD2	1	MN	1	MN1	1
M1	1	M2	1	A	2				

SUBROUTINE POH (LMBDN,LMD1,LMD2,MN,MN1,M1,M2,N,NC)

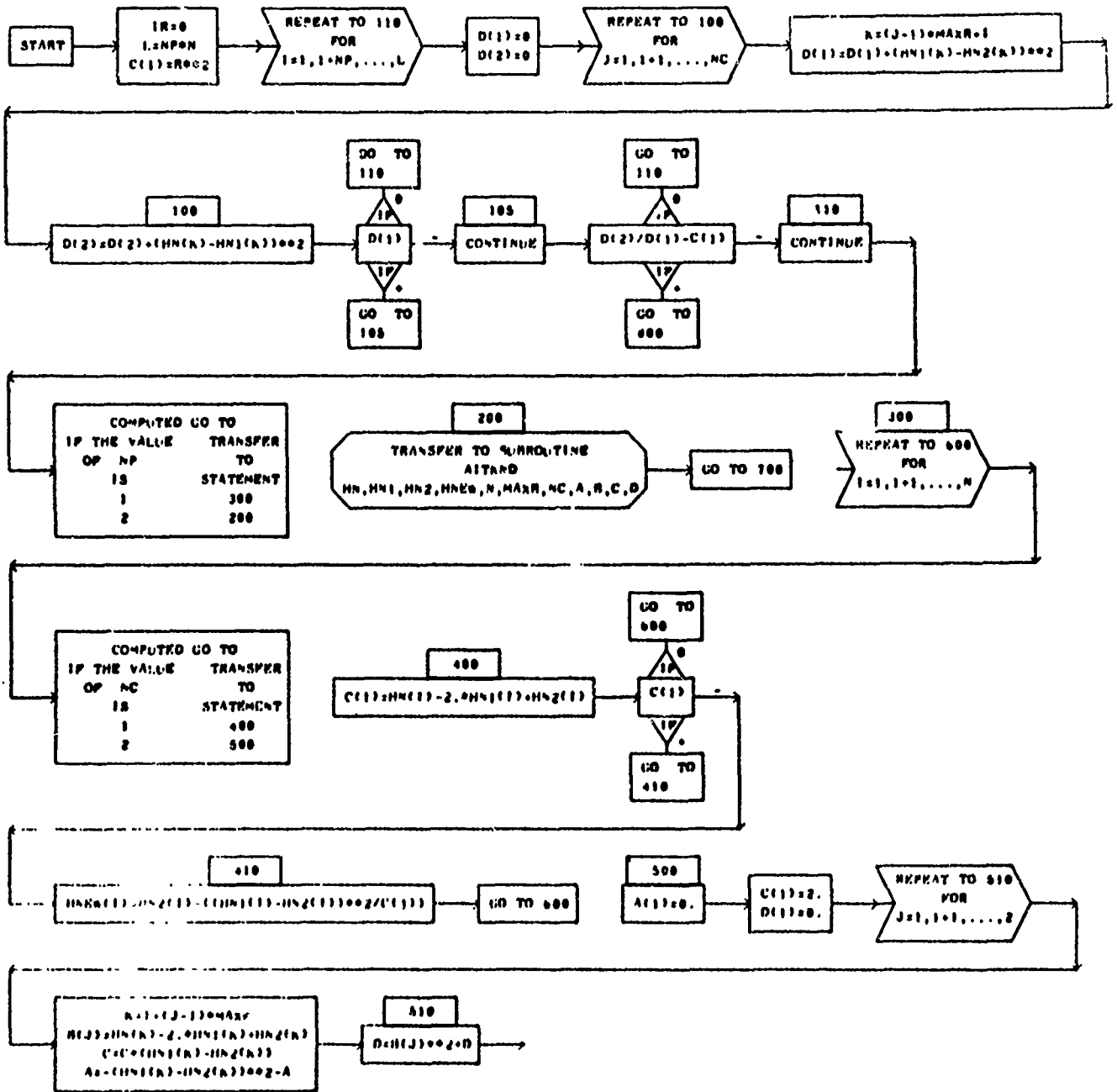
PAGE 1

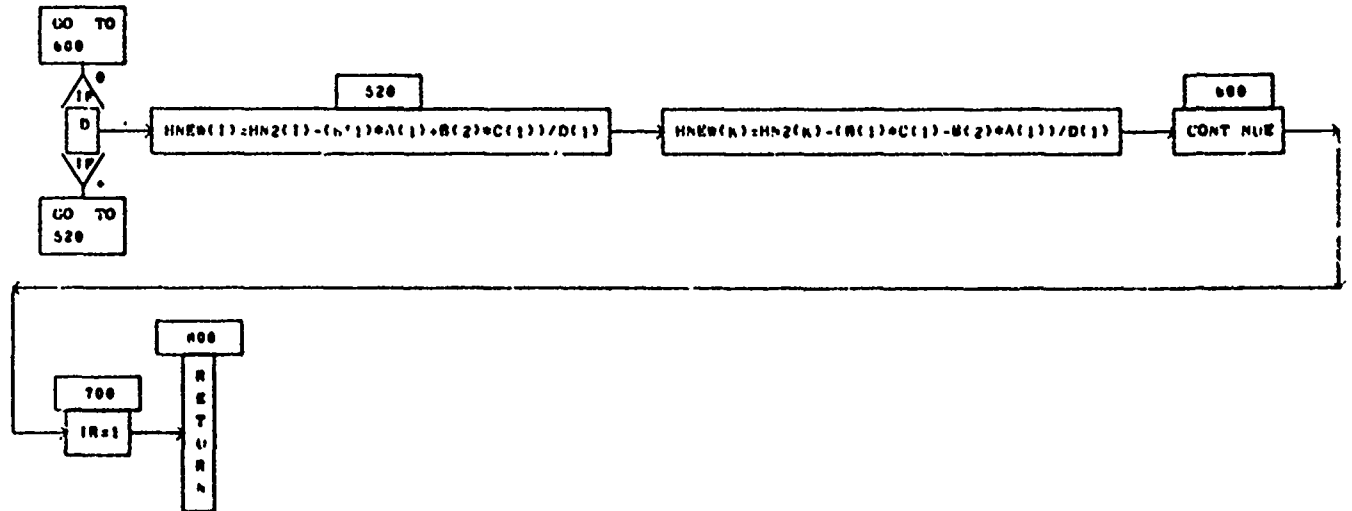


AIKNS

D I M E N S I O N E D V A R I A B L E S

SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE
MN	1	MN1	1	MN2	1	MNEB	1	A	2
B	4	C	2	D	2				

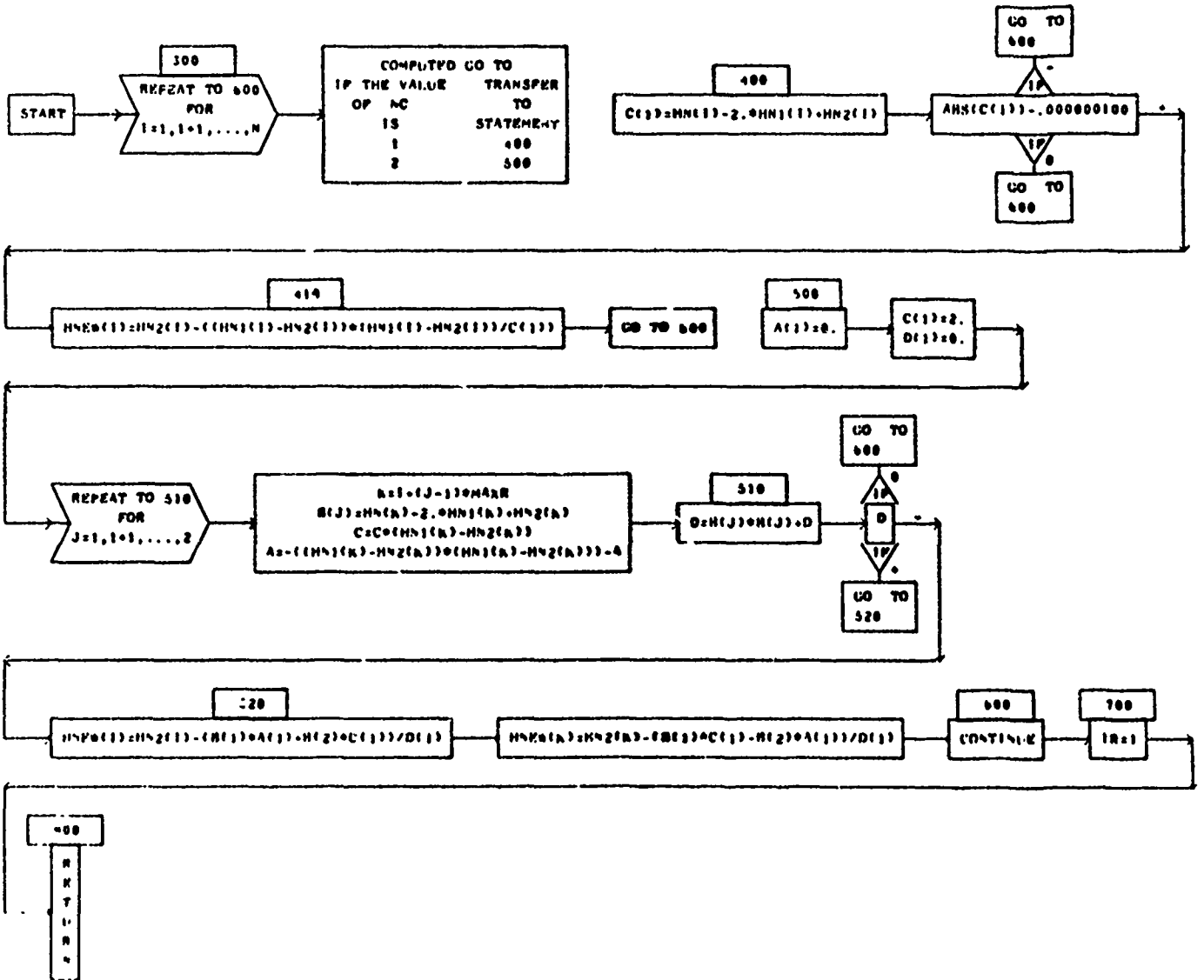




ATTEND

D I M E N S I O N S V A R I A B L E S

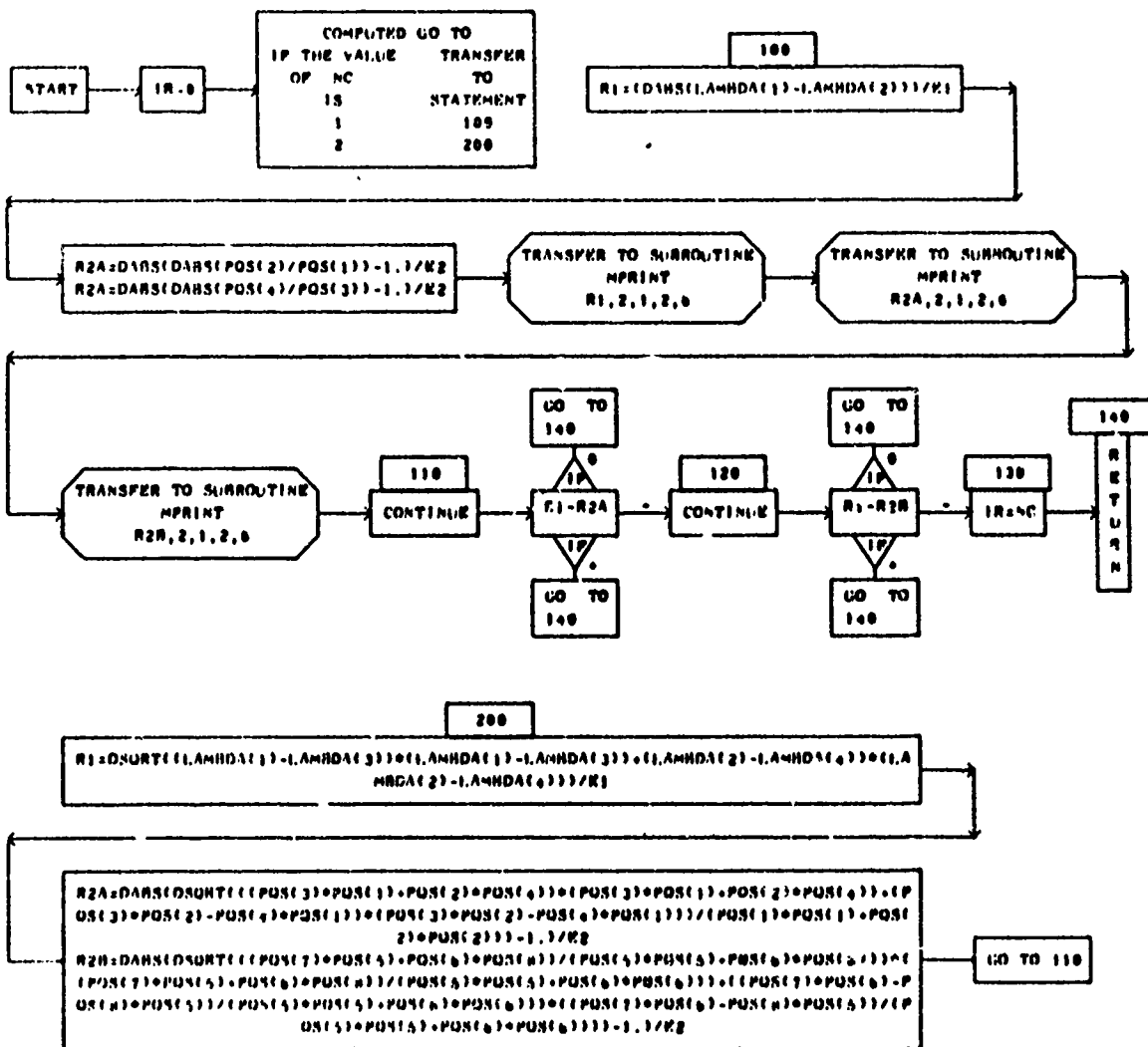
SYMBOL.	STORAGE	SYMBOL.	STORAGE	SYMBOL.	STORAGE	SYMBOL.	STORAGE	SYMBOL.	STORAGE
HN	1	HN1	1	HN2	1	HNEW	1	A	1
B	2	C	1	D	1				



120188

D I M E N S I O N E D V A R I A B L E S

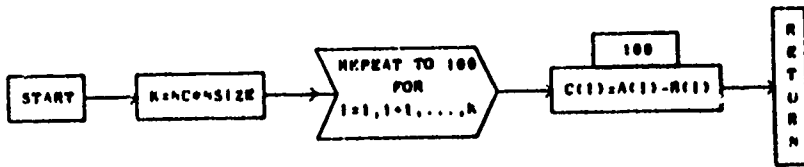
SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE
LAMBDA	1	PDS	1						



MADE

SUBROUTINE MADE (A,B,C,NSIZE,NC)

PAGE 1



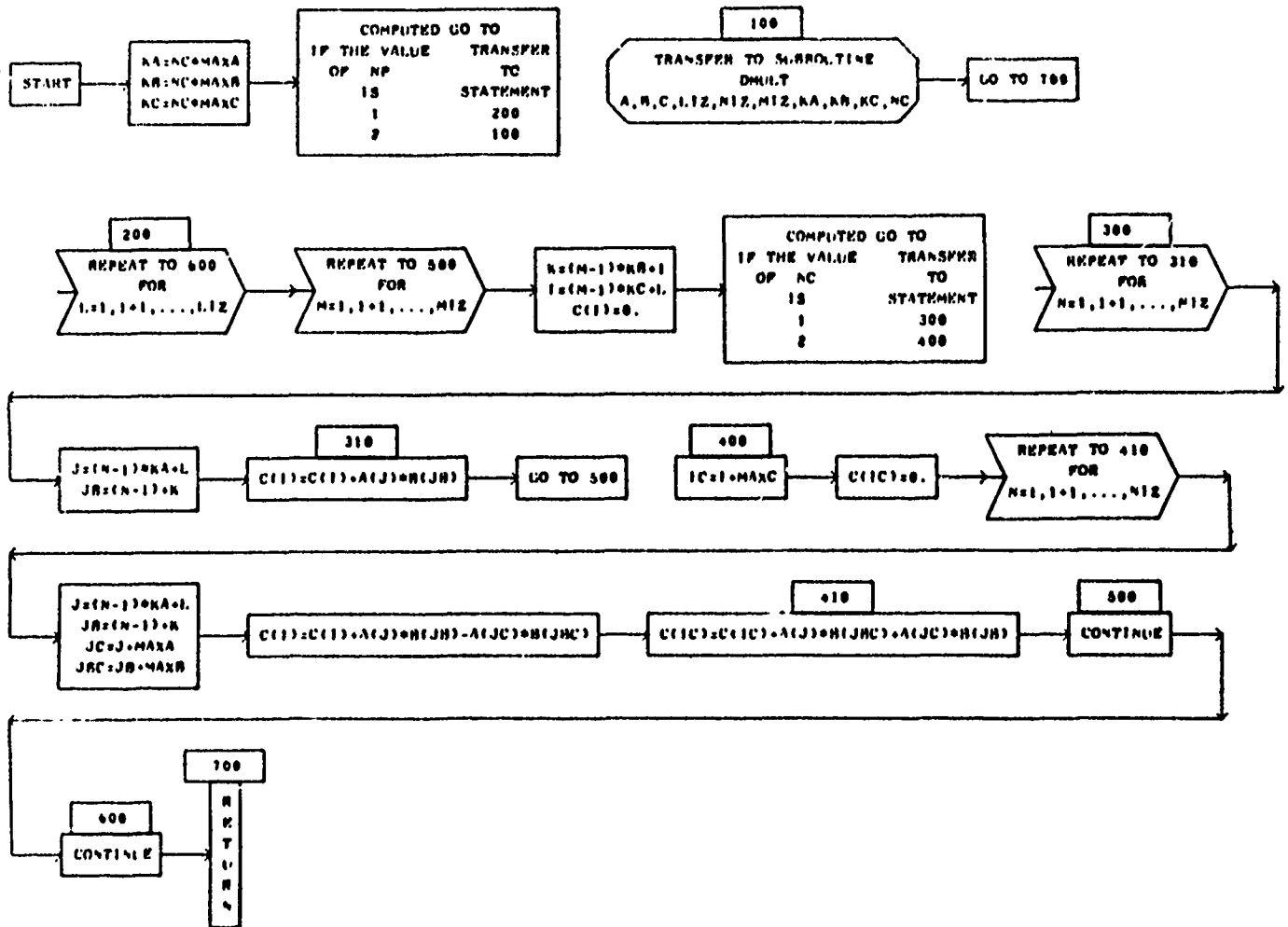
MULTS

D I M E N S I O N E D V A R I A B L E S

SYMBOL	STORAGES	SYMBOL	STORAGES	SYMBOL	STORAGES	SYMBOL	STORAGES	SYMBOL	STORAGES
A	1	B	1	C	1				

SUBROUTINE MULT (A,B,C,I1Z,N1Z,M1Z,MAXA,MAXB,MAXC,NC,NP)

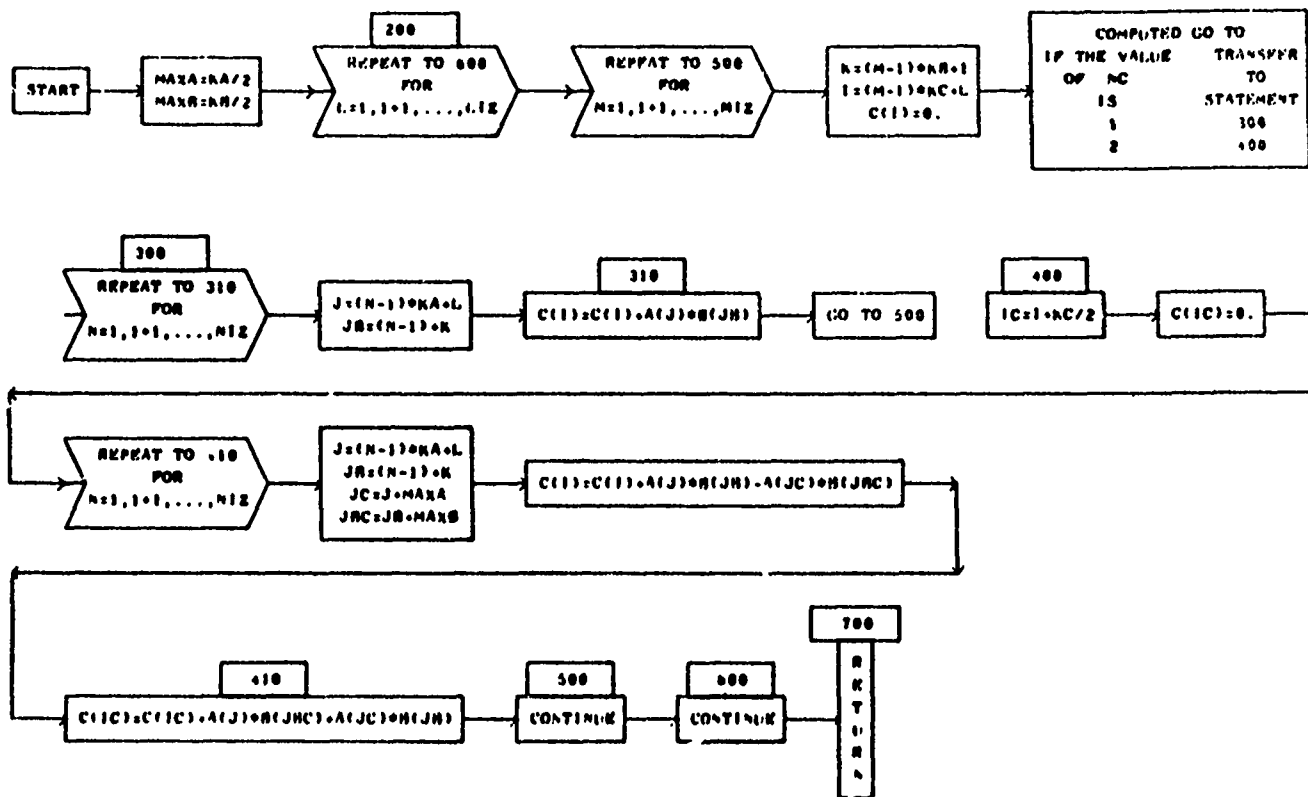
PAGE 1



DMULTS

SUBROUTINE DMULT (A,B,C,LIZ,NIZ,MIZ,NA,NB,NC,NC)

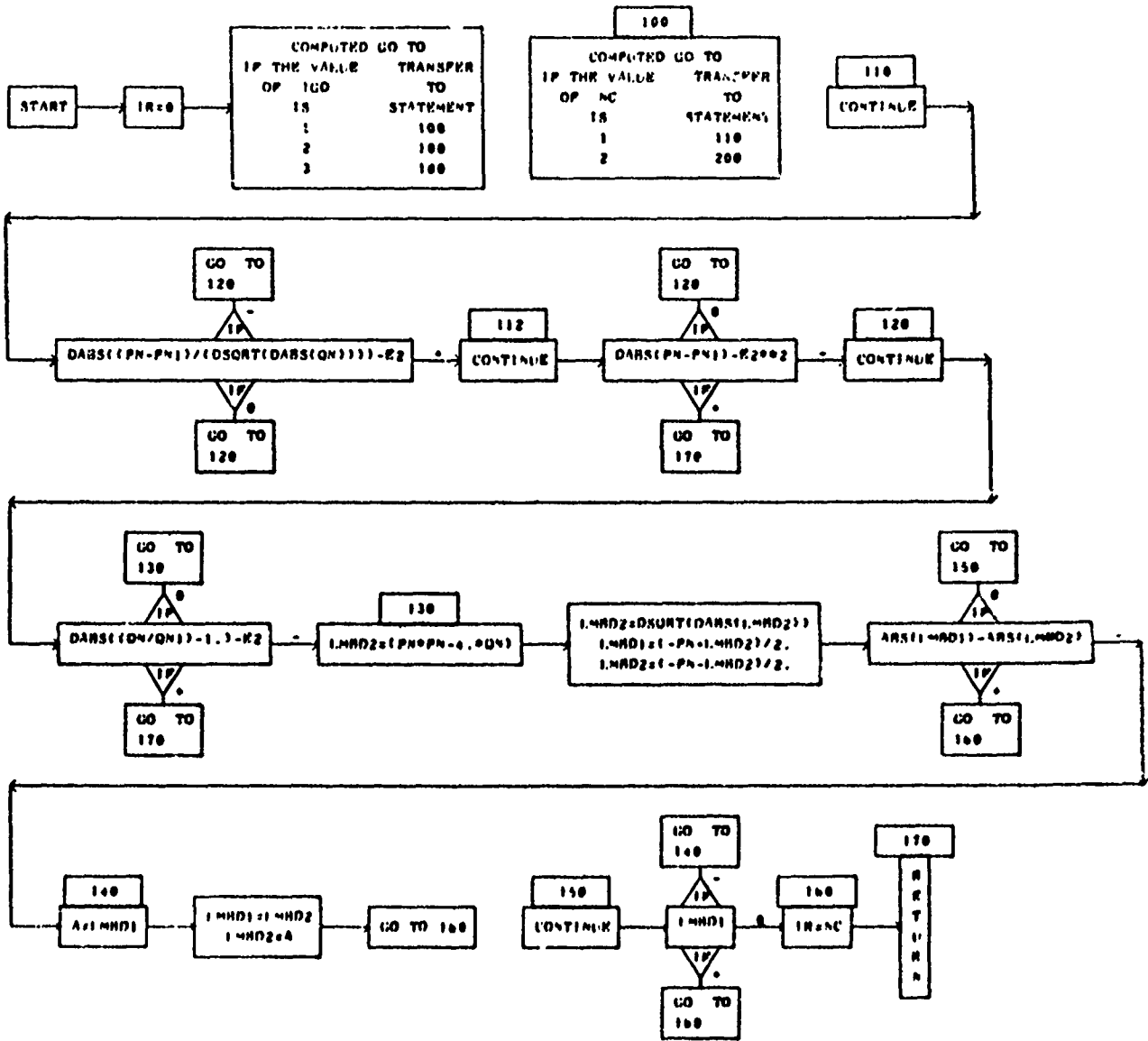
PAGE 1

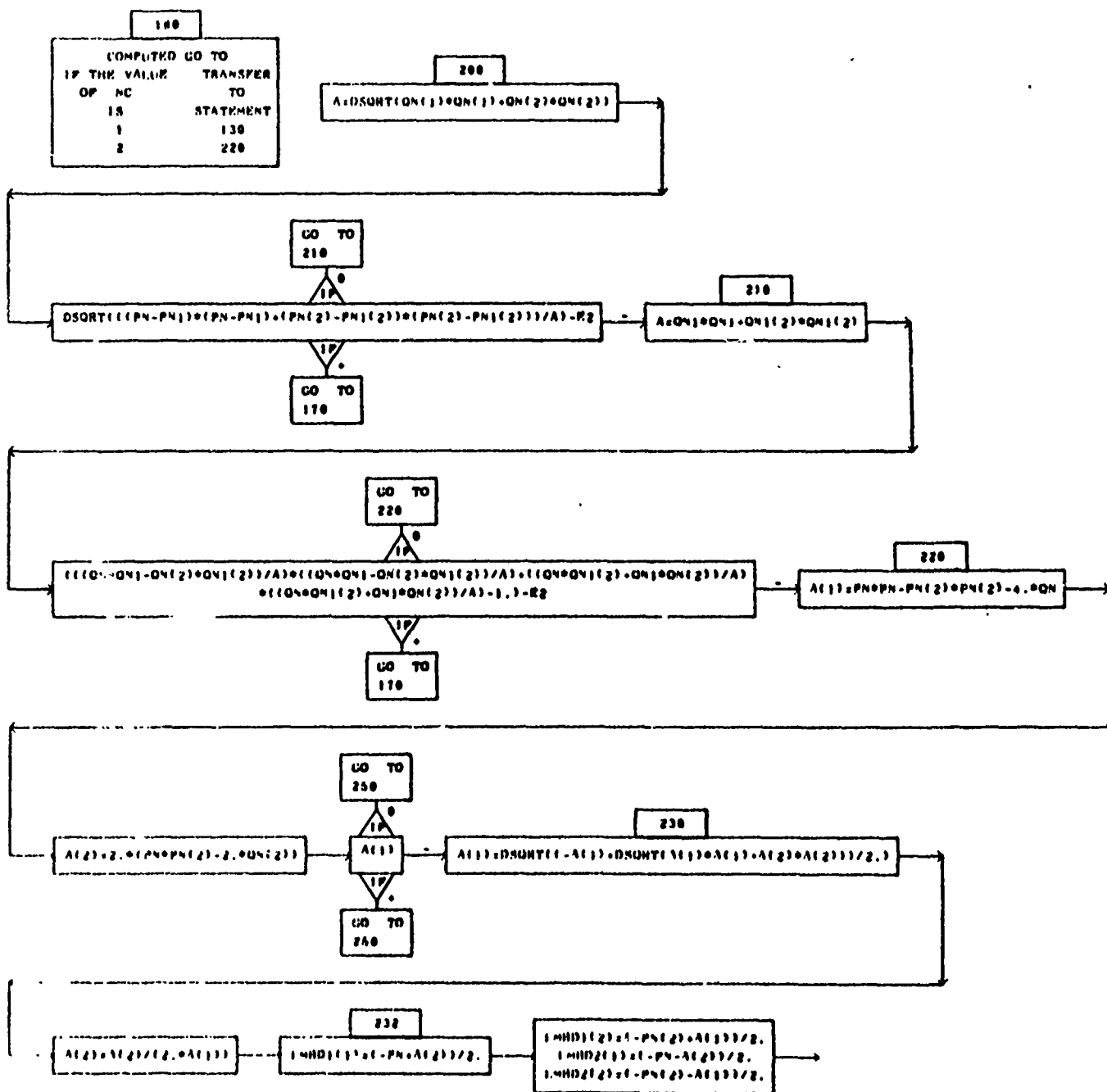


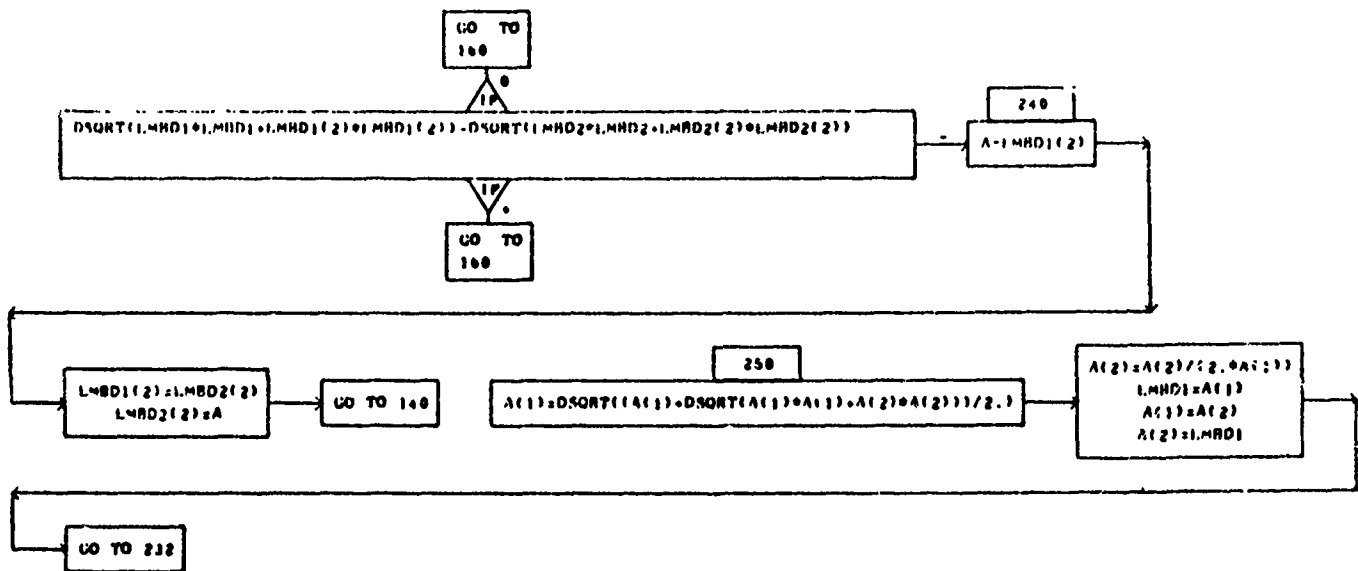
POLMS

D I M E N S I O N E D V A R I A B L E S

SYMBOL.	STORAGES	SYMBOL.	STORAGES	SYMBOL.	STORAGES	SYMBOL.	STORAGES	SYMBOL.	STORAGES
PN	1	PH1	1	ON	1	ON1	1	E2	1
LMRD1	1	LMRD2	1						







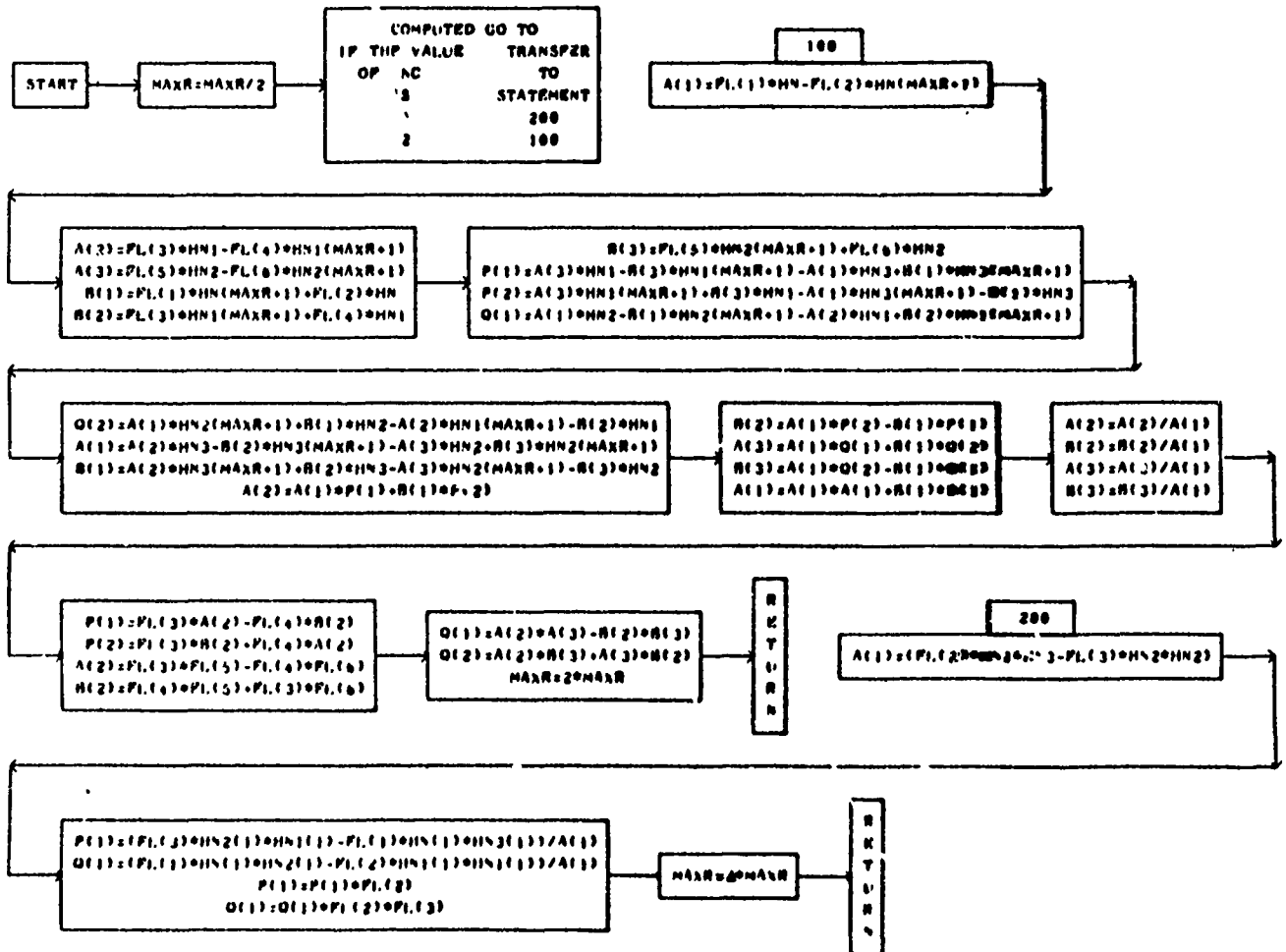
F05

D I M E N S I O N E D V A R I A B L E S

7/MNO.	STORAGES	SYMBOL	STORAGES	SYMBOL	STORAGES	SYMBOL	STORAGES	SYMBOL	STORAGES
PL	1	MN	1	MN1	1	MN2	1	MN3	1
P	1	Q	1	A	3	R	3		

SUBROUTINE F0 (PL, MN, MN1, MN2, MN3, P, Q, NC, NAME)

PAGE 1



CLOSES

SUBROUTINE CLOSE, COMPUTES 2 CLOSE ROOTS.

U = MATRIX, DIMENSIONED (MAXR,2*NC+MAXR)

H = STARTING GUESS, DIMENSIONED ((MAXR,2*NC+4)+2*NC+4)

NSIZE = SIZE OF MATRIX

MAXR = DIMENSIONED NUMBER OF ROWS OF U AND H

MAXTRY = MAXIMUM NUMBER OF DOUBLE PRECISION ITERATIONS.

EPS1 = SINGLE ROOT CONVERGENCE CRITERIA

EPS2 = DOUBLE ROOT CONVERGENCE CRITERIA

R = ATKENS CONVERGENCE CRITERIA

IRR = ERROR RETURN INDICATOR. =1, OVERFLOW

=2, DIVIDE CHECK

=3, BOTH OVERFLOW AND DIVIDE

CHECK.

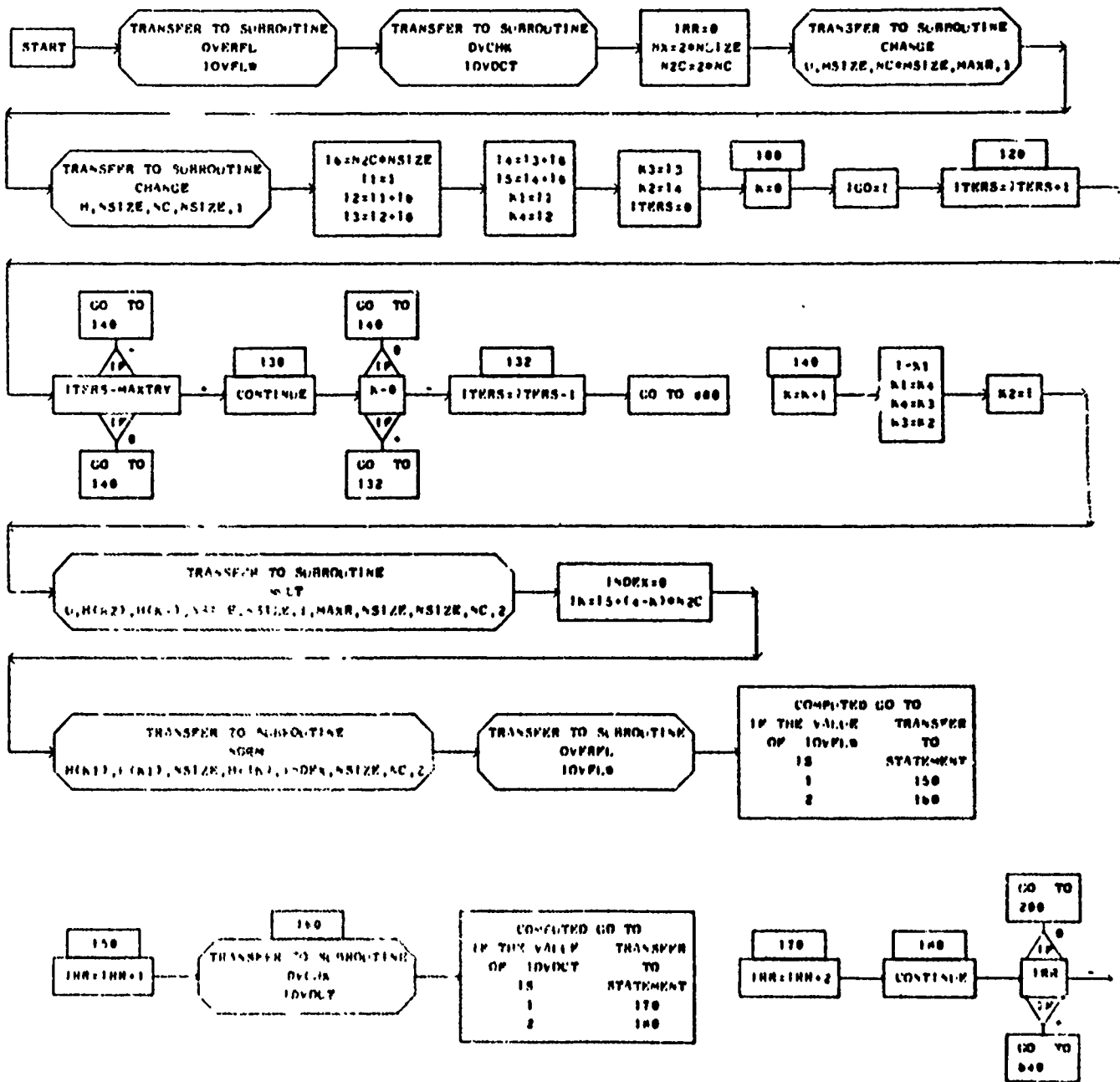
ITERS = NUMBER OF ITERATIONS PERFORMED, - FOR DOUBLE ROOT

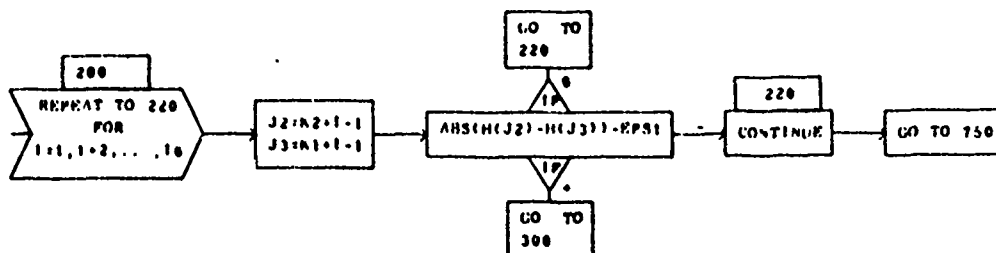
+ FOR SINGLE ROOT

NC = 1, REAL 2, COMPLEX

D I M E N S I O N E D V A R I A B L E S

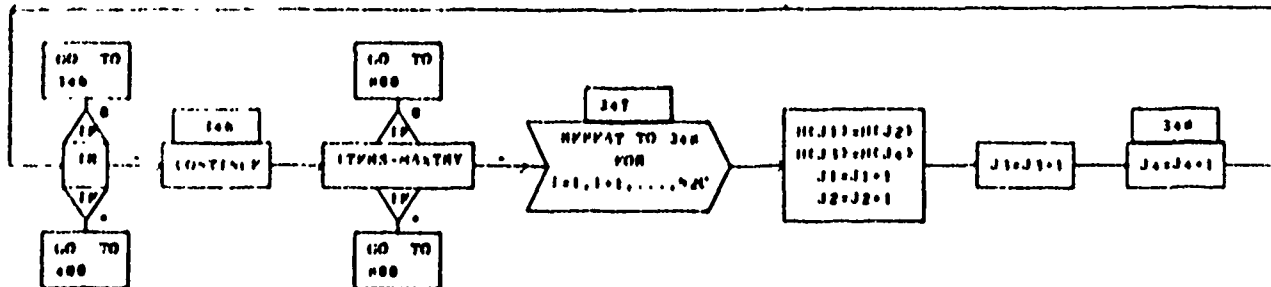
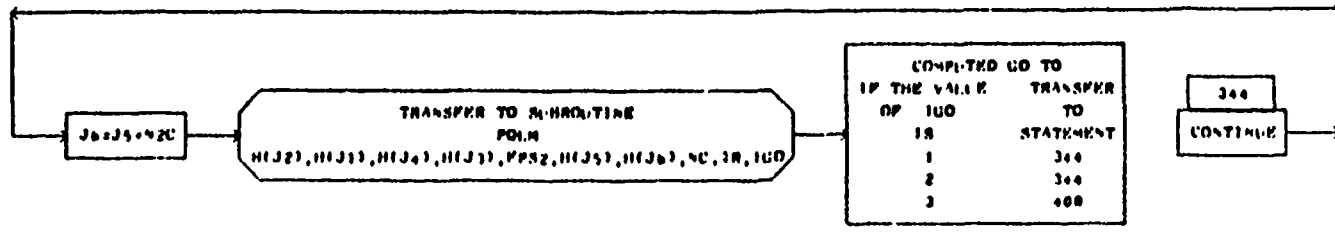
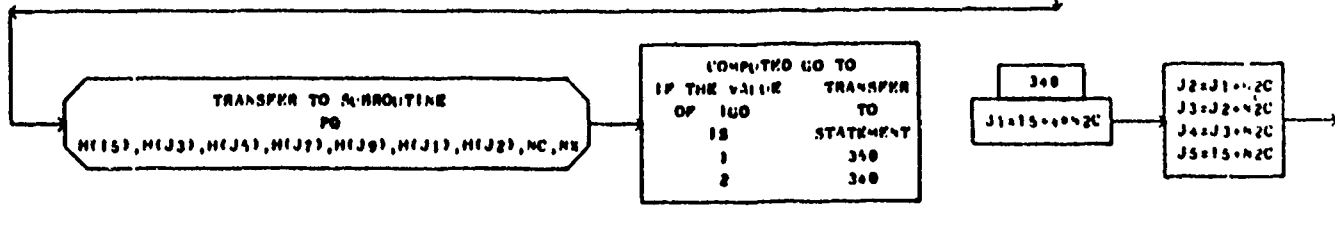
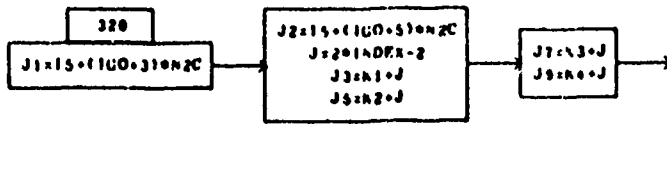
SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE
U	1	H	1	VALUE	1				

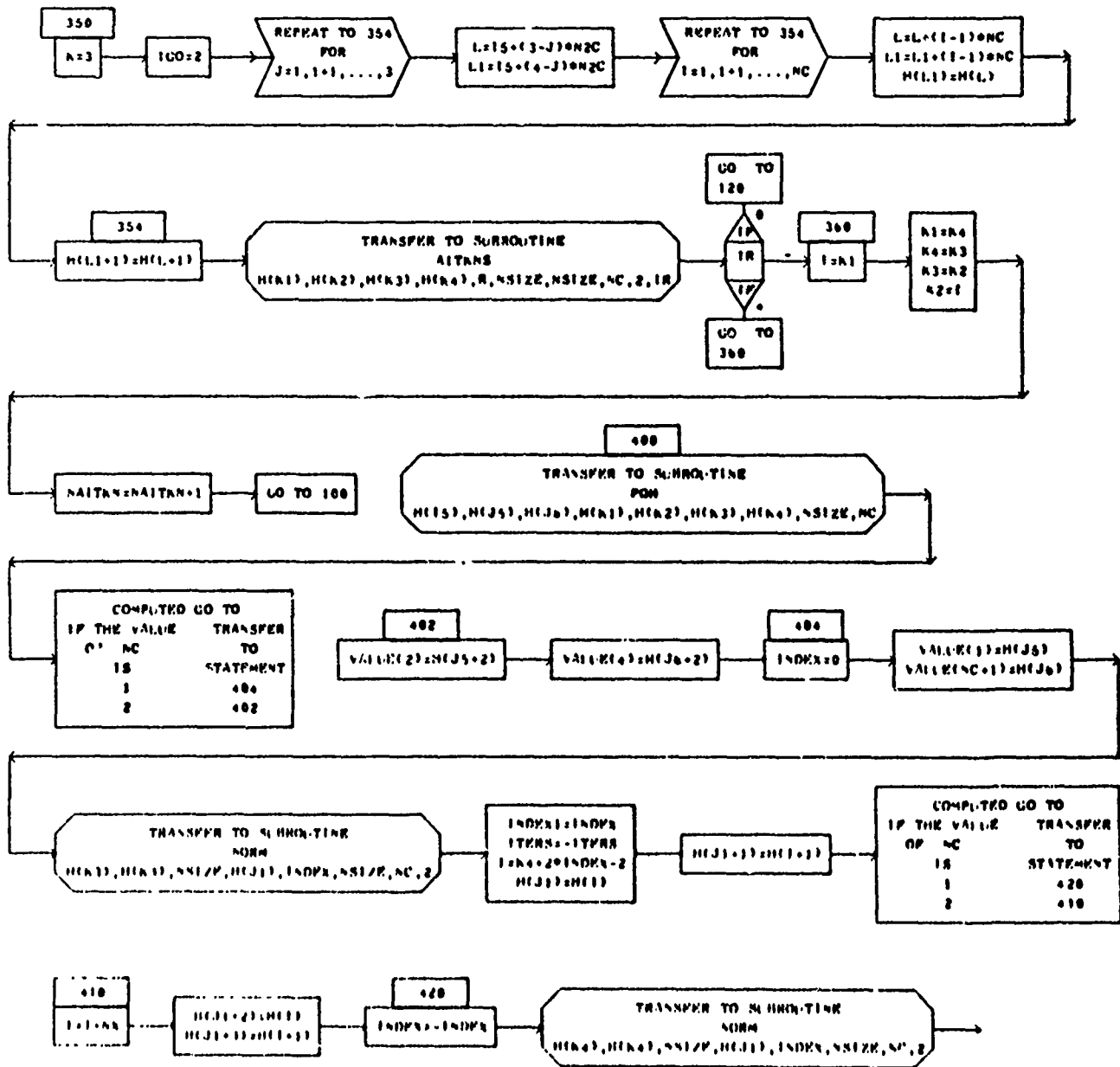


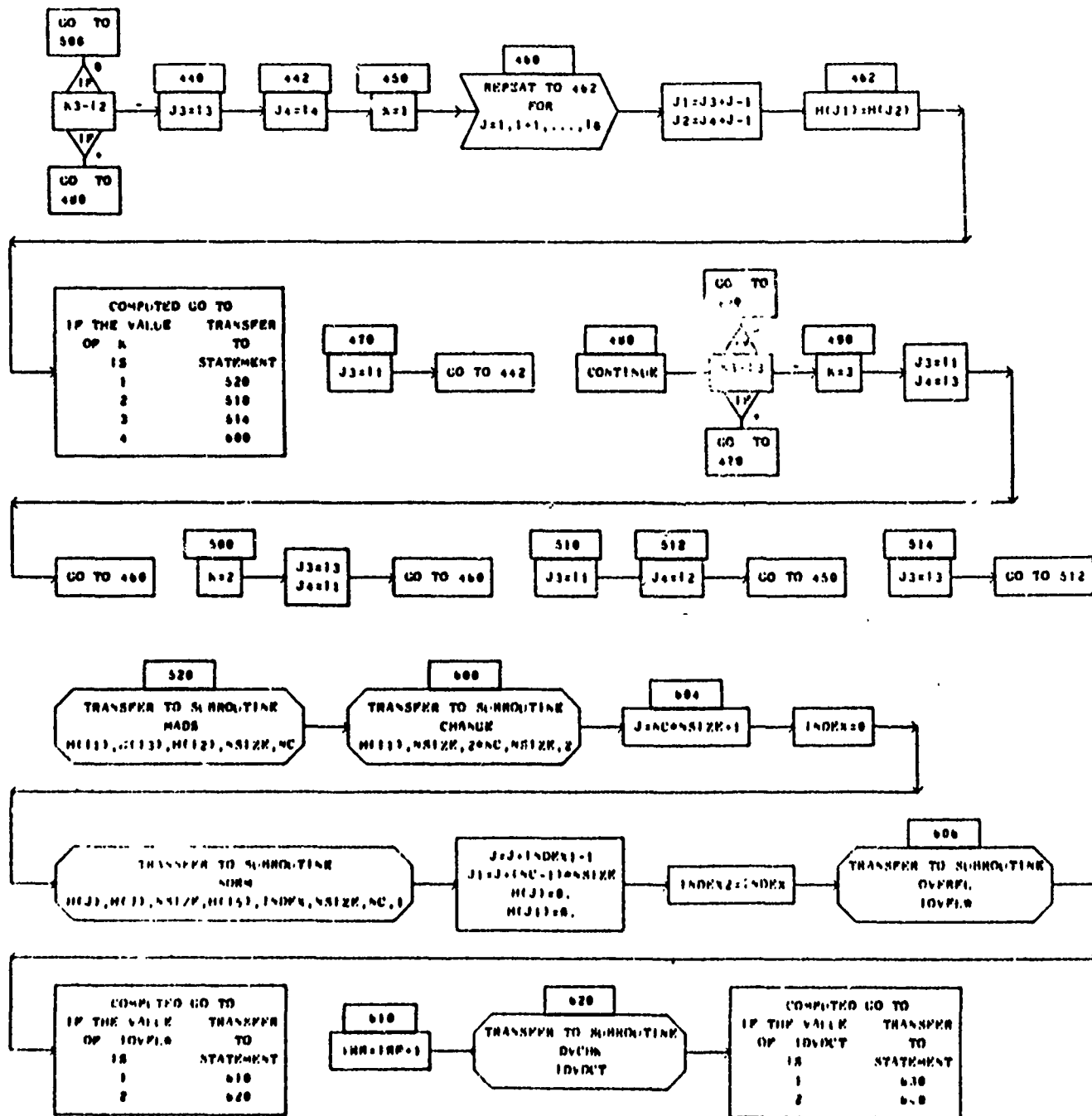


300

COMPUTED GO TO		
IF THE VALUE	TRANSFER	TO
OF K	IS	STATEMENT
1	120	
2	120	
3	120	
4	320	

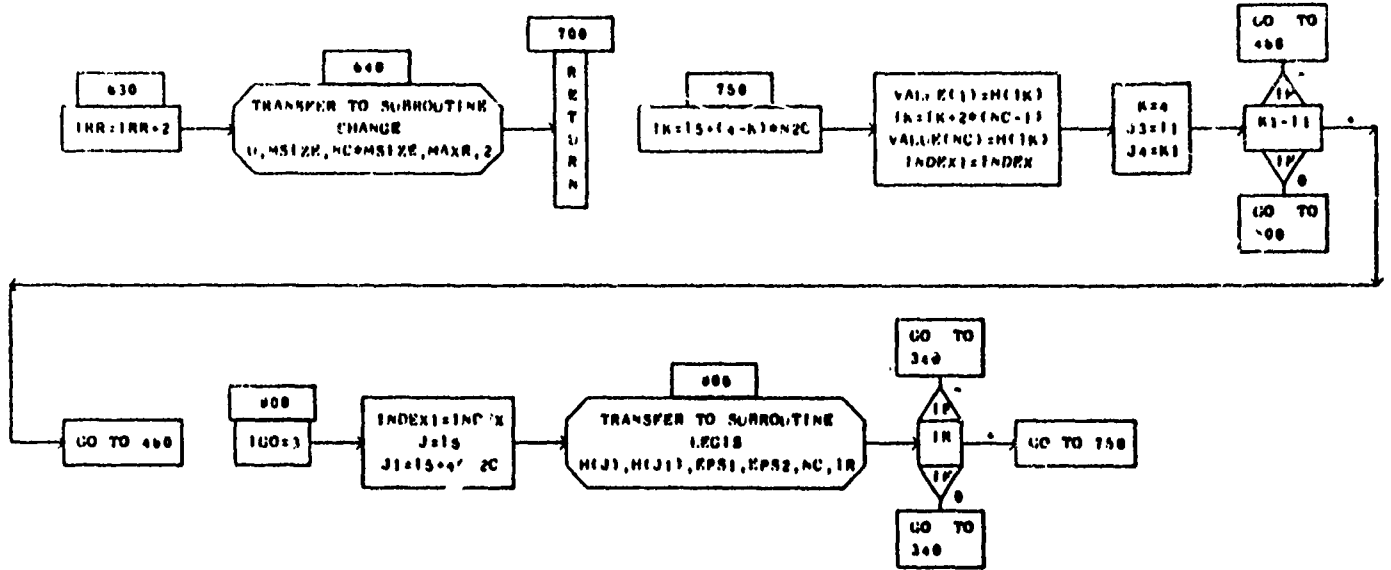






SUBROUTINE CLOSES (U,H,NSIZE,MAXR,R,EPS1,EPS2,NC,IRR,MAXTRY,ITERS,

PAGE 5

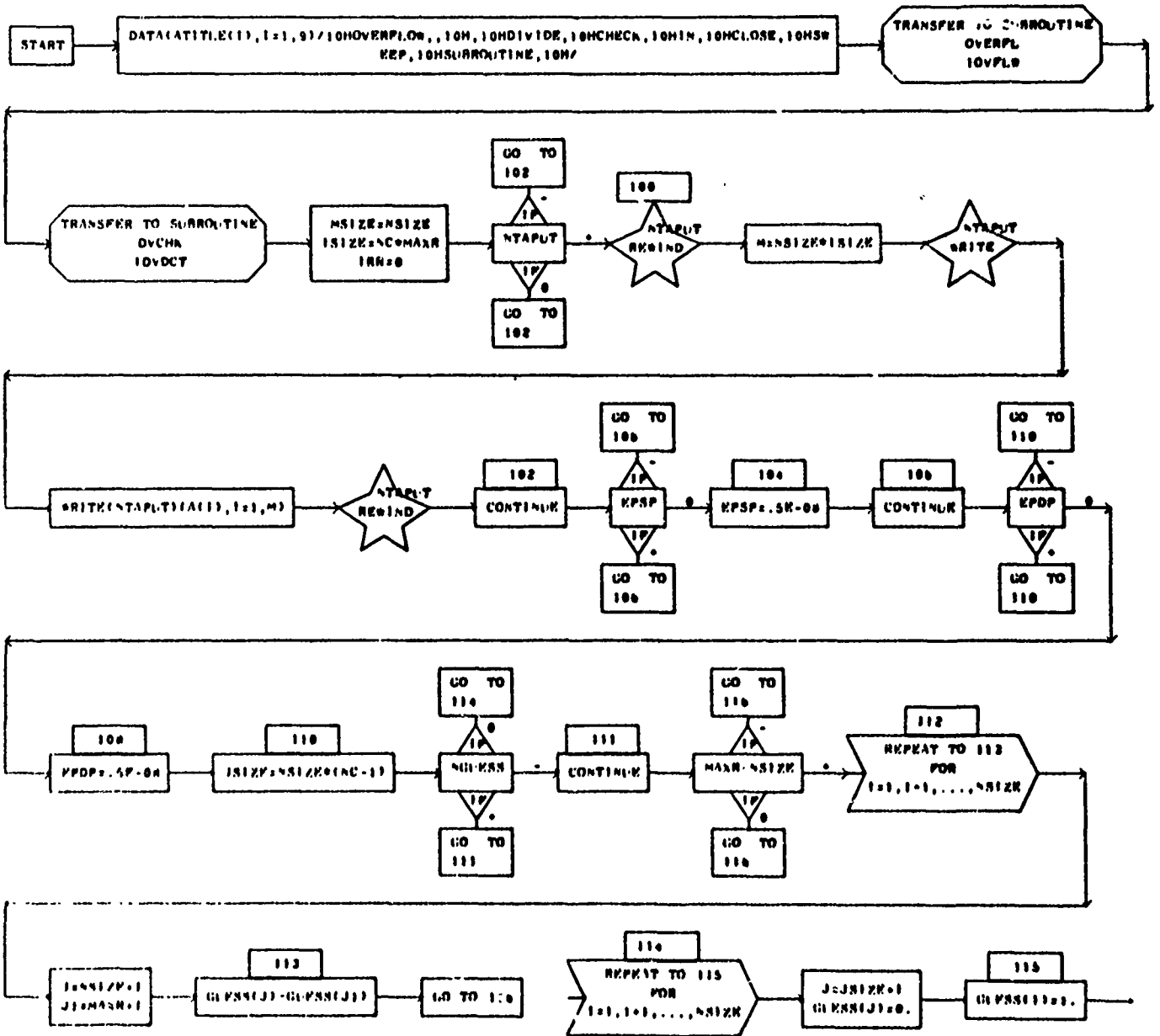


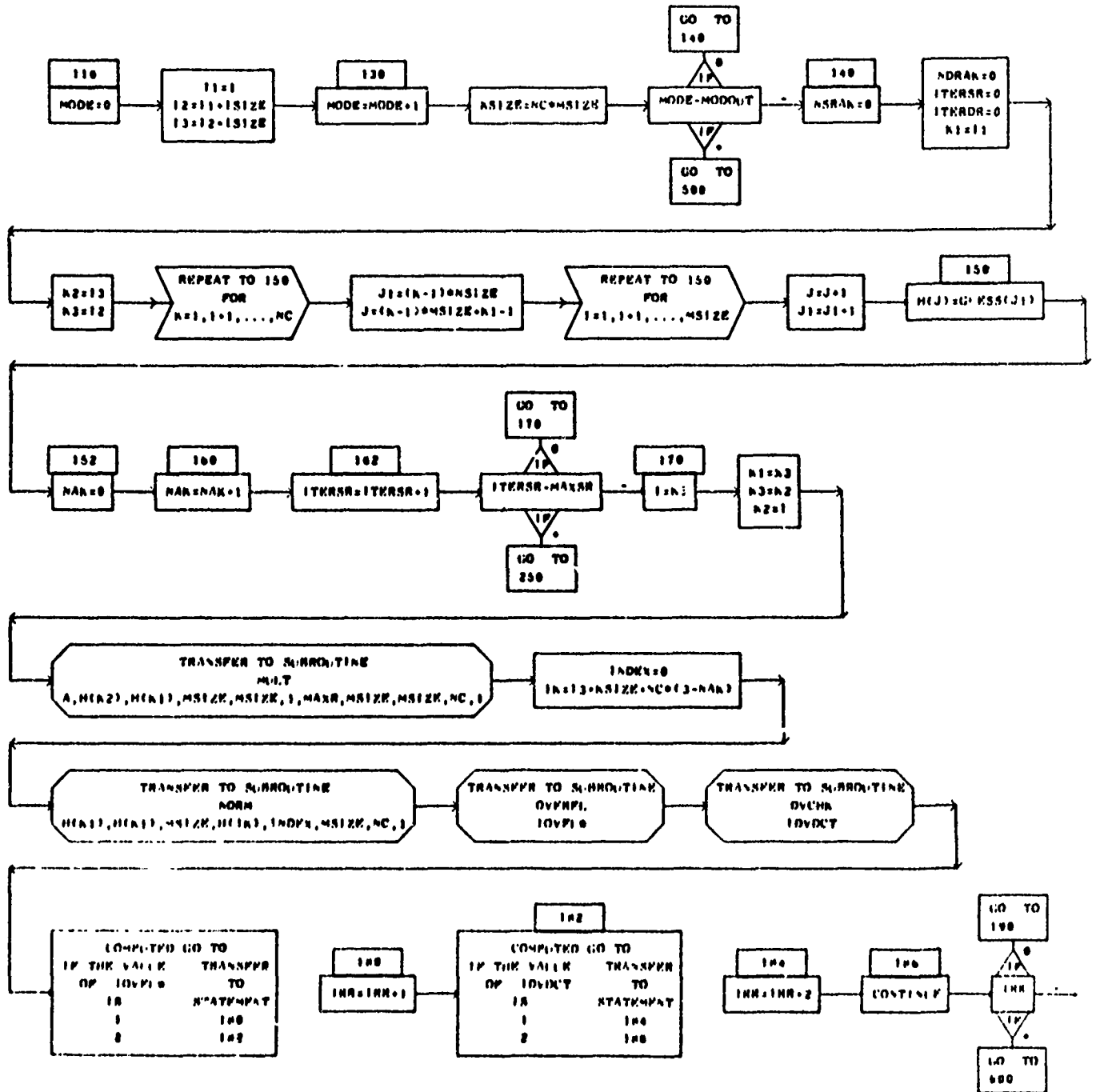
METERS

A IS STORED IN CORE AT A. (MAXR X NONPENSIZ 1)
 NTAPUT IS A UTILITY TAPE, FOR CHECK VECTORS IF DESIRED.
 EPSP = EPSILON ONE = SINGLE PRECISION CONVERGENCE TEST NUMBER
 EDPD = EPSILON TWO = DOUBLE PRECISION
 NC = 1, IF REAL NP = 1, IF SINGLE PRECISION
 2, IF COMPLEX = 2, IF DOUBLE ..
 NGUES = 6, IF FIRST GUESS IS TO BE A COLUMN OF ONES.
 MODOUT = NO. OF MODES TO BE COMPUTED.
 NAKSR = NO. TIMES AITENS ACCELERATION WAS USED IN SINGLE PRECISION.
 NAKDR = DOUBLE
 MAXSR = MAXIMUM ITERATIONS ALLOWED IN SINGLE PRECISION.
 MAXDR = DOUBLE
 IRR = ERROR RETURN = 1, FOR OVERFLOW
 2, FOR DIVIDE CHECK
 3, FOR BOTH OVERFLOW AND DIVIDE CHECK
 NSIZE = NO. OF ROWS AND COLUMNS OF A
 RSP = R, AITENS ACCELERATION CONVERGENCE CONTROL, FOR SINGLE PRECIS.
 RDP = R AITENS ACCELERATION CONVERGENCE CONTROL, FOR DOUBLE PRECIS.
 NARR = DIMENSIONED NUMBER OF ROWS OF A AND GUESS

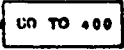
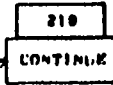
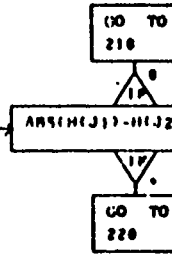
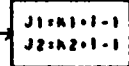
D I M E N S I O N E D V A R I A B L E S

SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE
A	1	GUESS	1	N	1	METER	1	NAKSR	1
NARR	1	AITENS	9	VECTOR	1	VALUE	1		

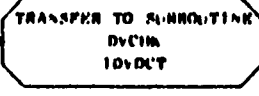
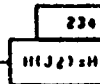
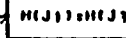
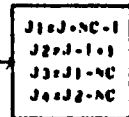
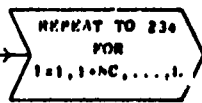
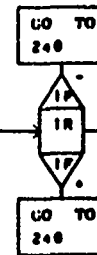
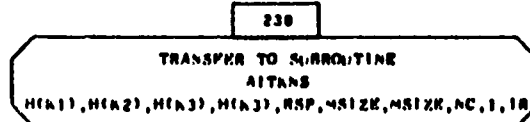




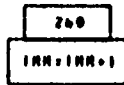
190		
COMPUTED GO TO	IF THE VALUE	TRANSFER
OF NAK	IS	TO
1	1	160
2	2	200
3	3	200



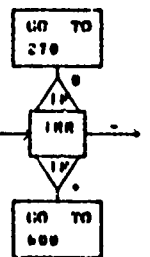
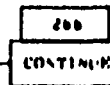
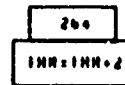
220		
COMPUTED GO TO	IF THE VALUE	TRANSFER
OF NAK	IS	TO
1	1	160
2	2	160
3	3	230

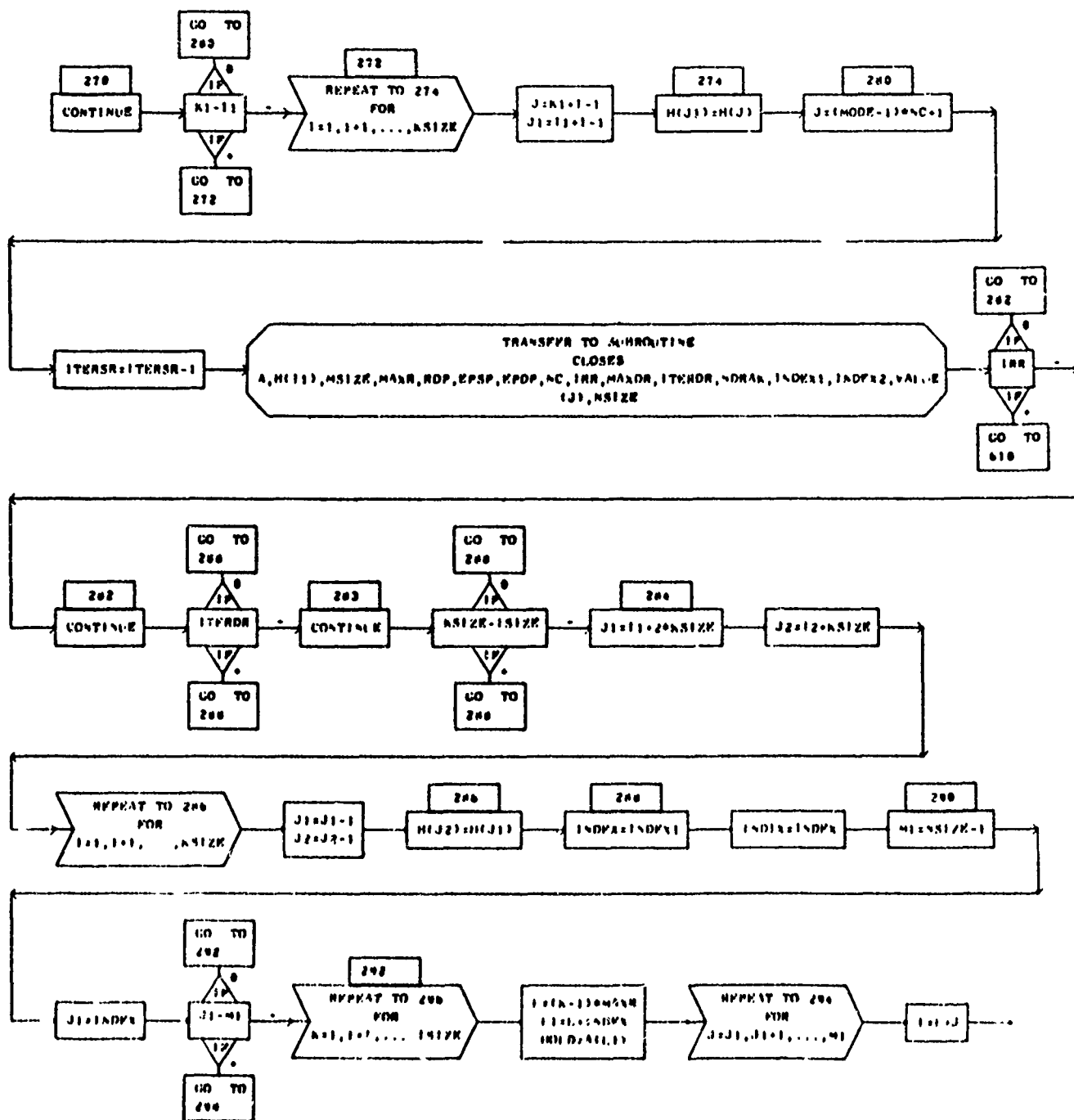


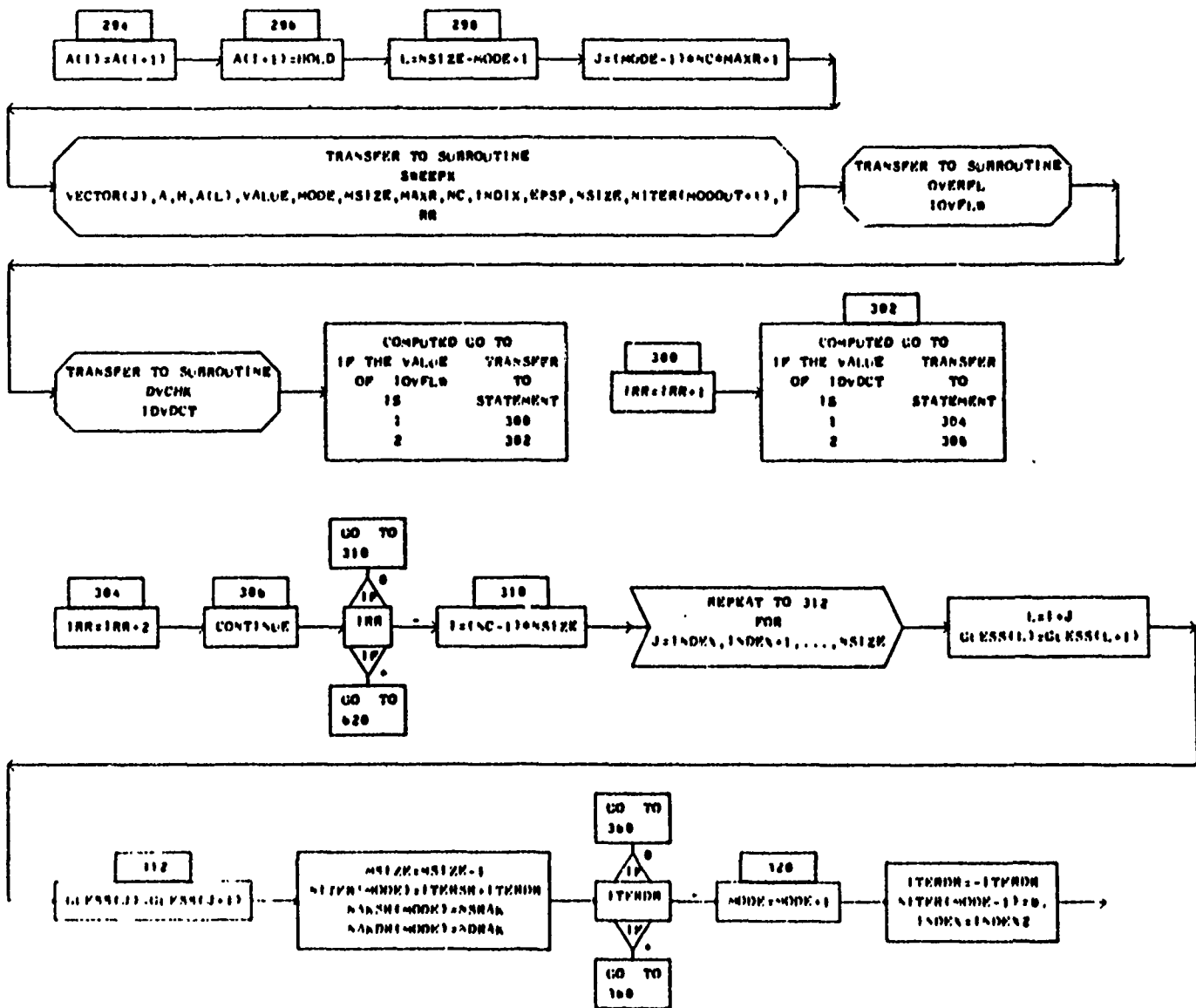
260		
COMPUTED GO TO	IF THE VALUE	TRANSFER
OF IOVPL0	IS	TO
1	1	264
2	2	262

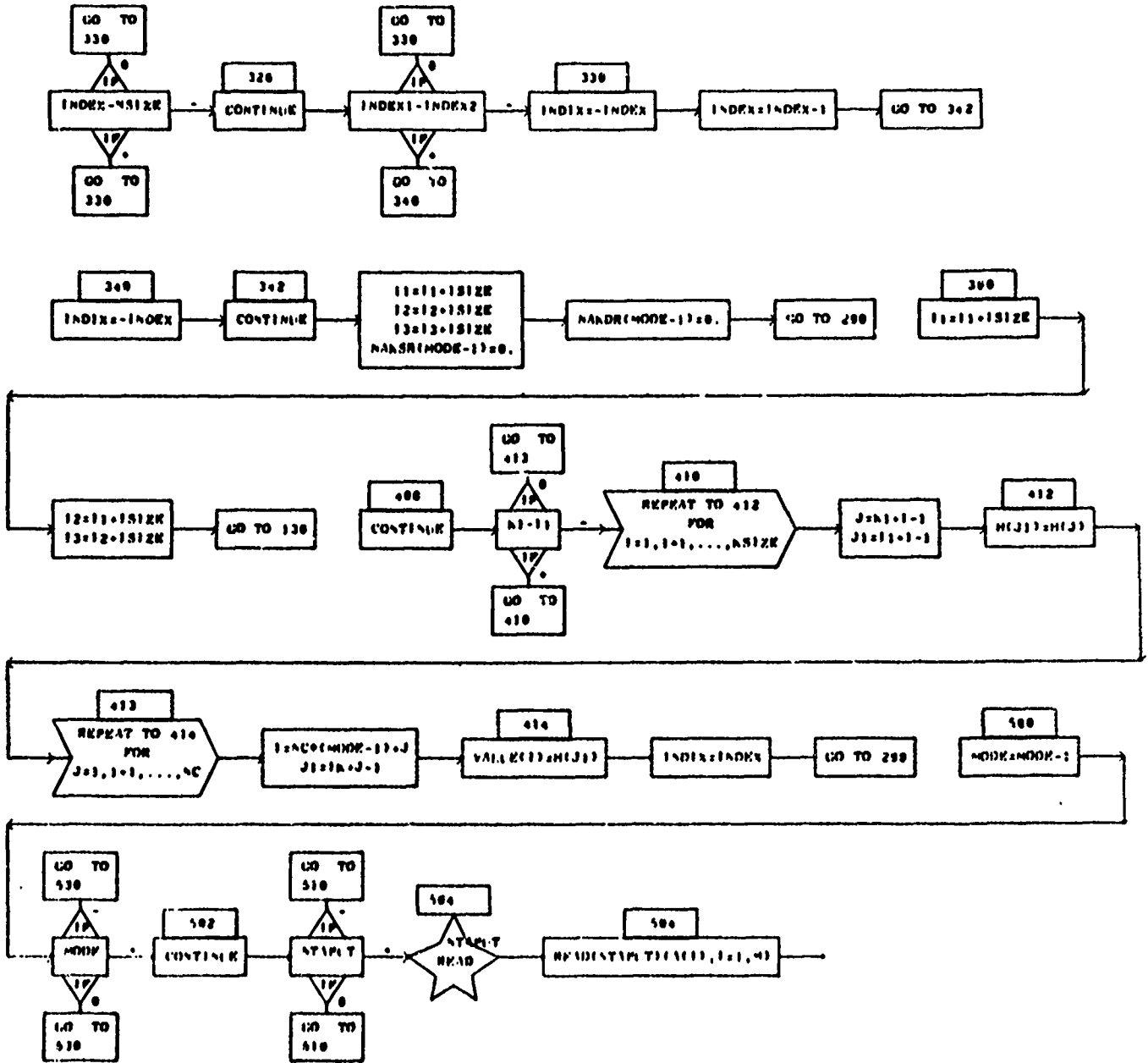


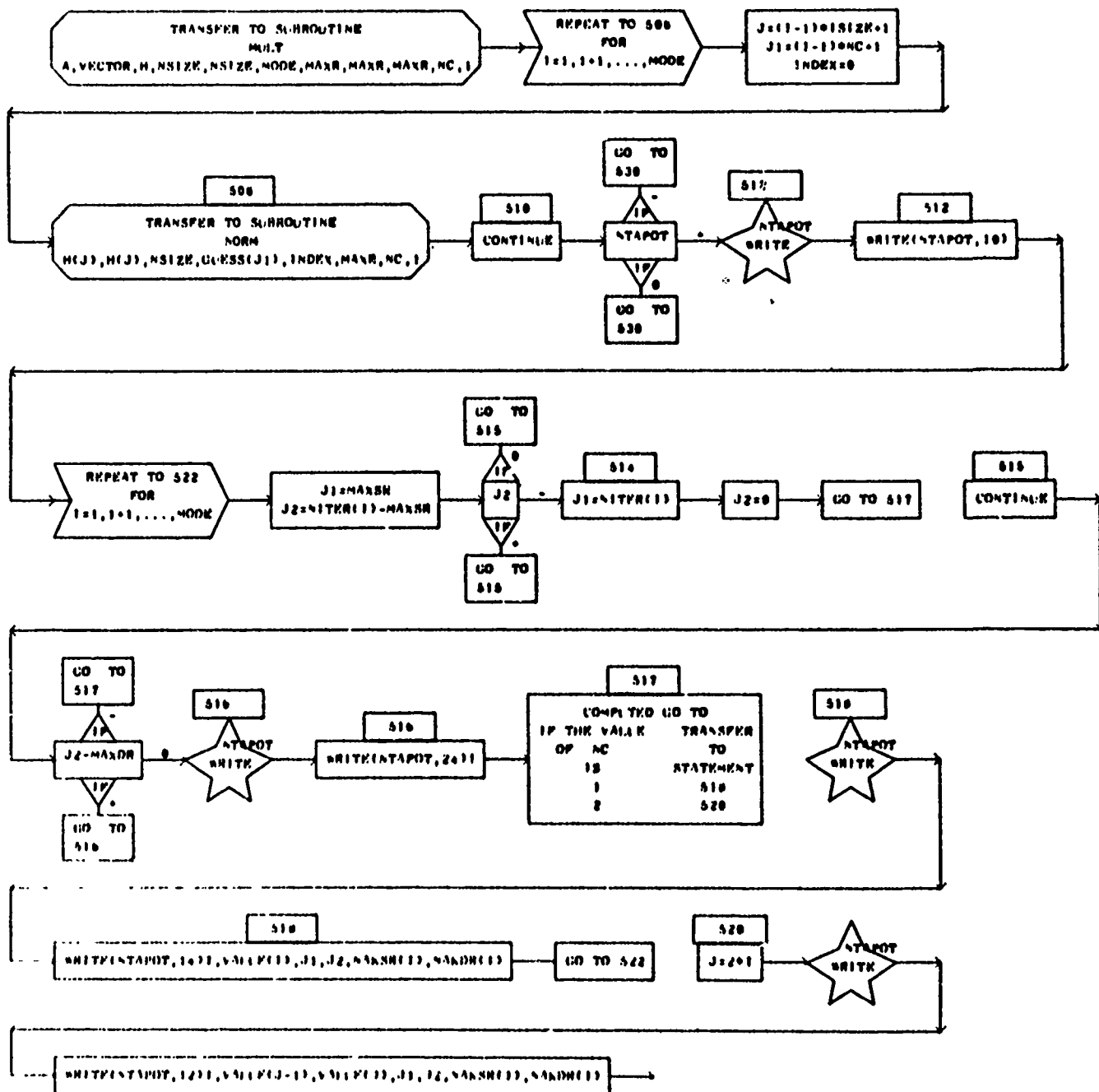
262		
COMPUTED GO TO	IF THE VALUE	TRANSFER
OF IOVDIT	IS	TO
1	1	264
2	2	260

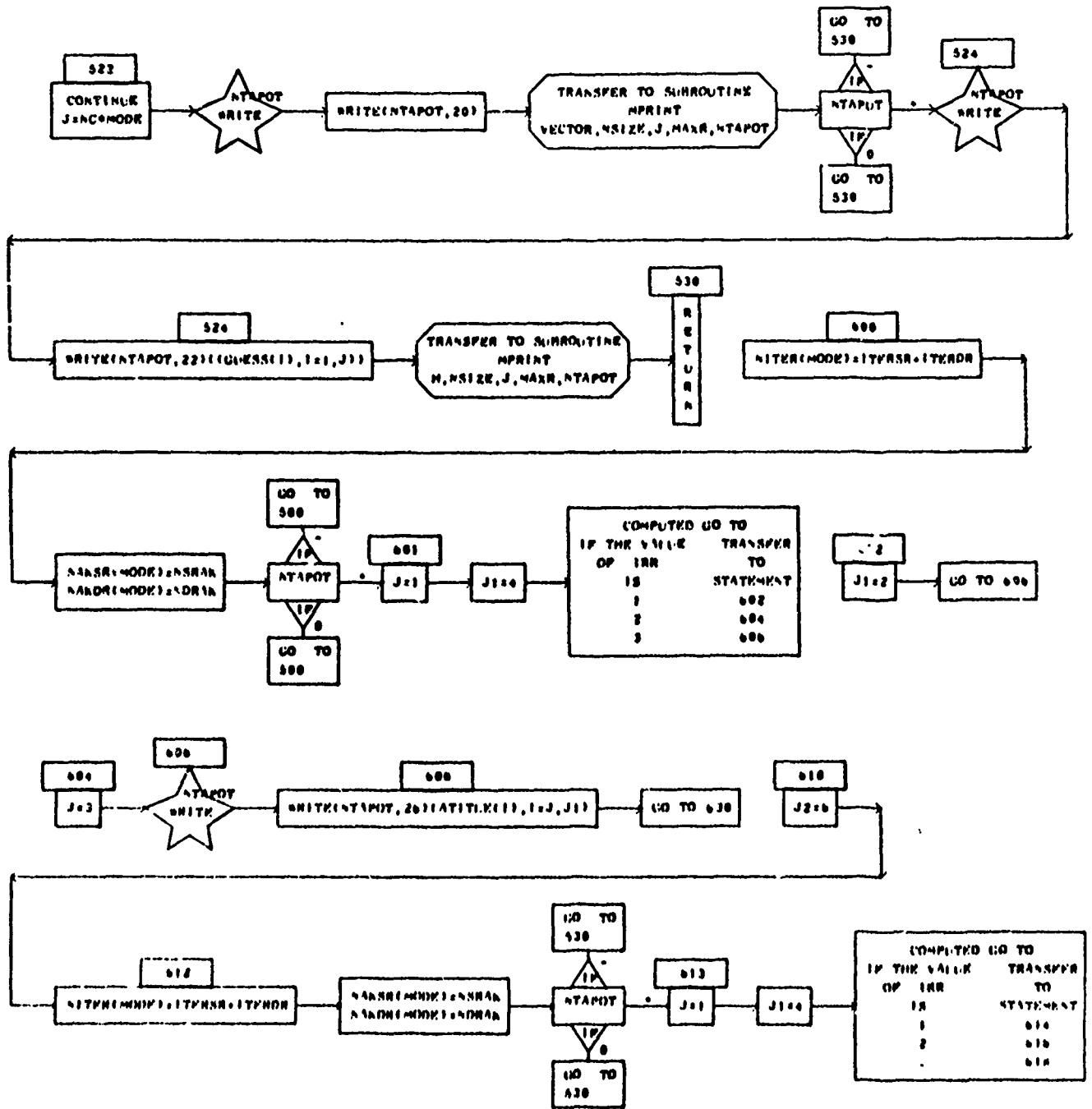


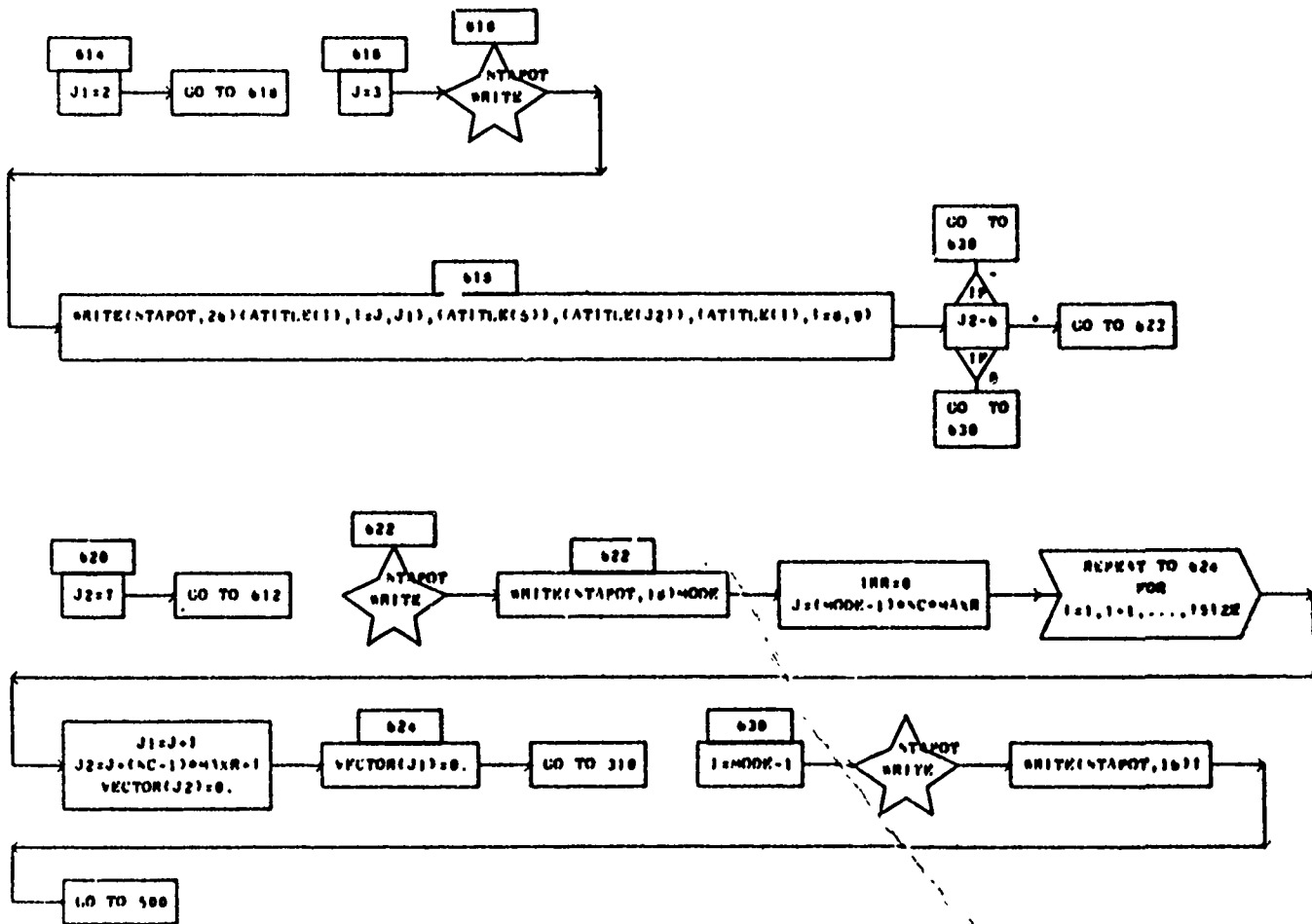












SKEEPS

SKEEPS SUBROUTINE

COMPUTES TRUE MODE AND SKEEPS IT FROM THE MATRIX. (REAL OR COMPLEX)

HTRUE = TRUE MODAL COLUMNS, AS COMPUTED. U = DYNAMIC MATRIX.

H = SERIES OF MODIFIED MODAL COLUMNS. P = COLUMN OF EIGENVALUES.

US = SERIES OF MODIFIED MODAL ROWS OF U.

MODE = MODE NO. BEING COMPUTED. N = SIZE

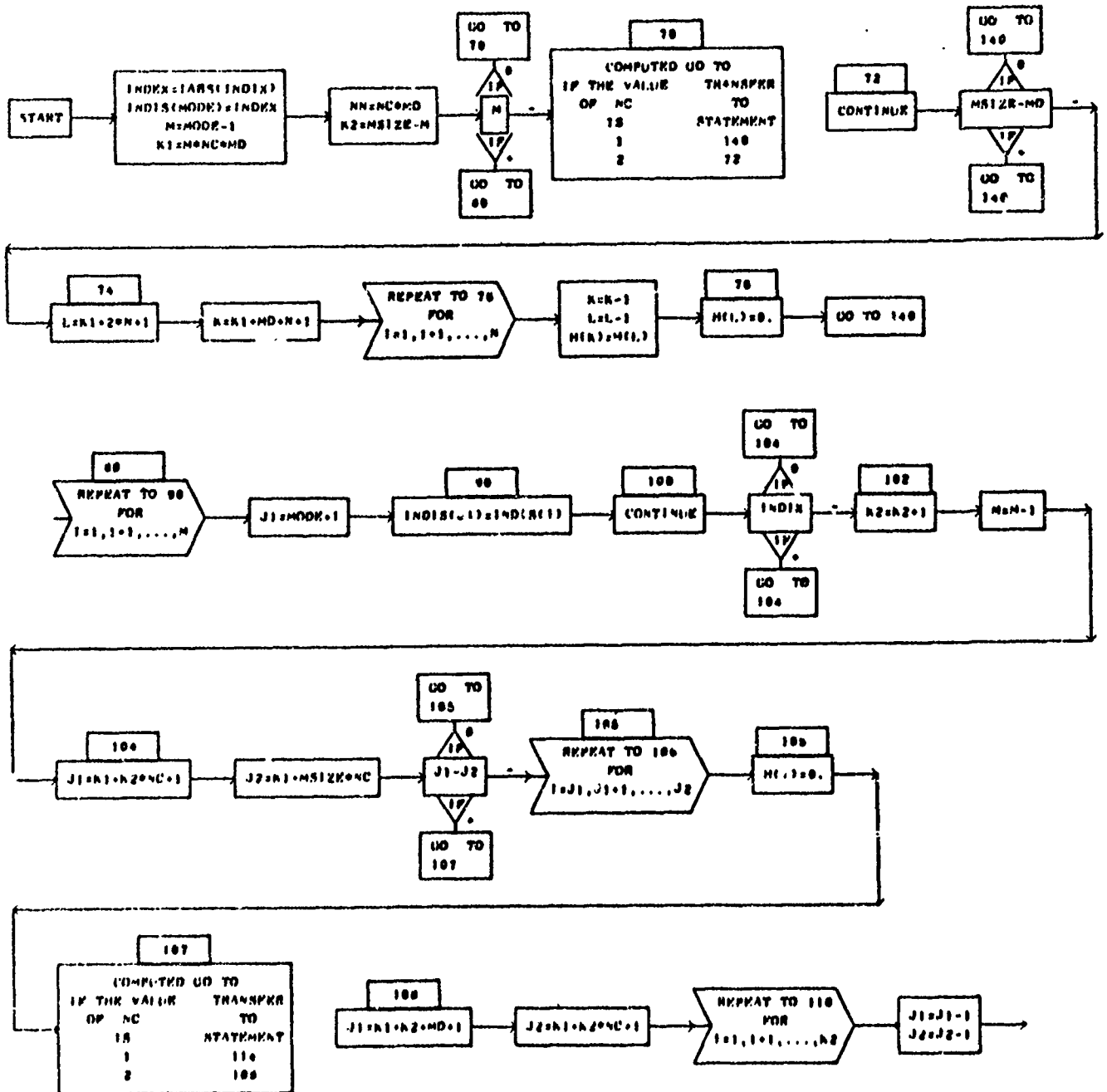
NO = DIMENSIONED NUMBER OF ROWS OF U, S, H, HTRUE

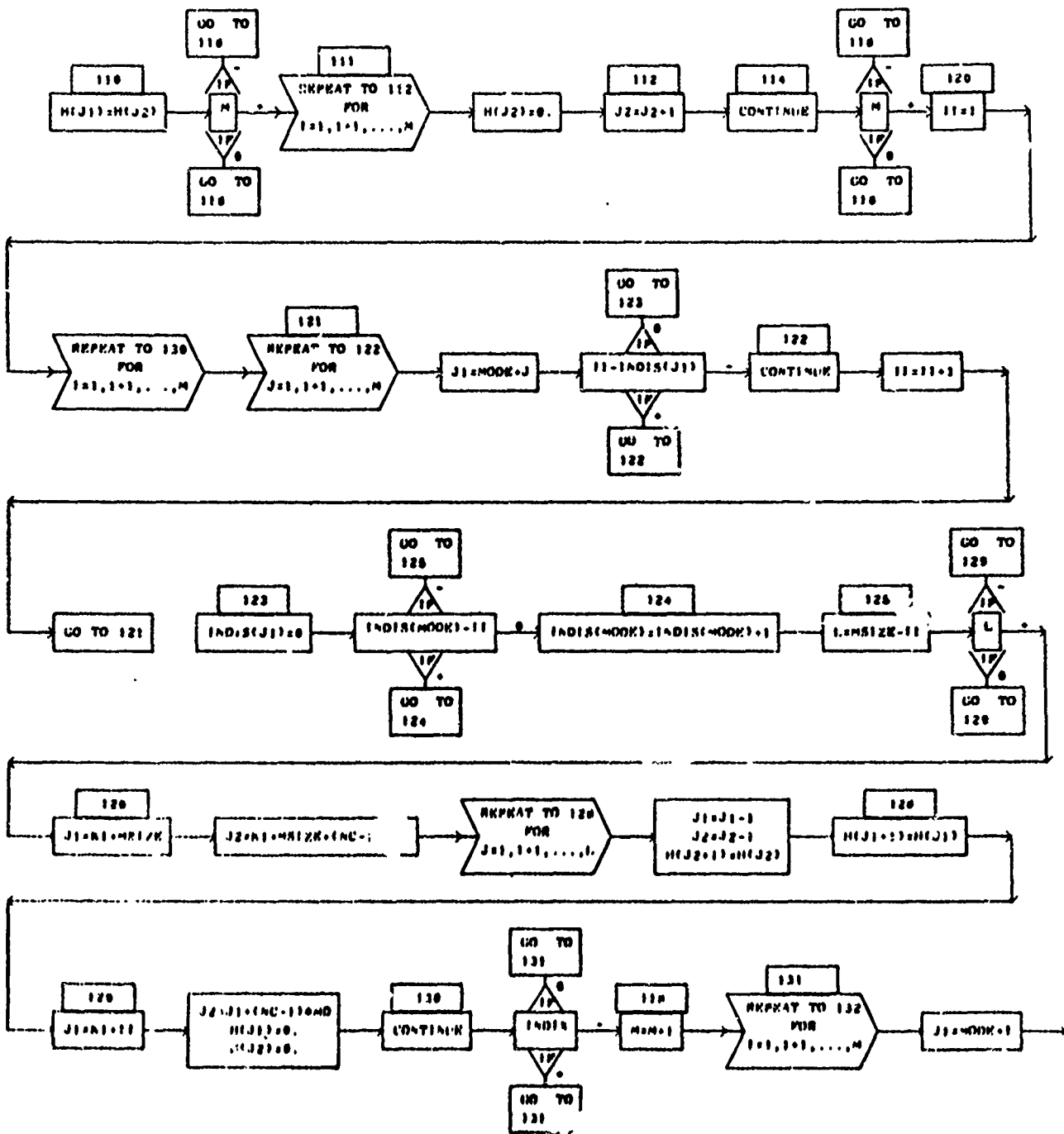
NR = 1 IF PROBLEM IS REAL.

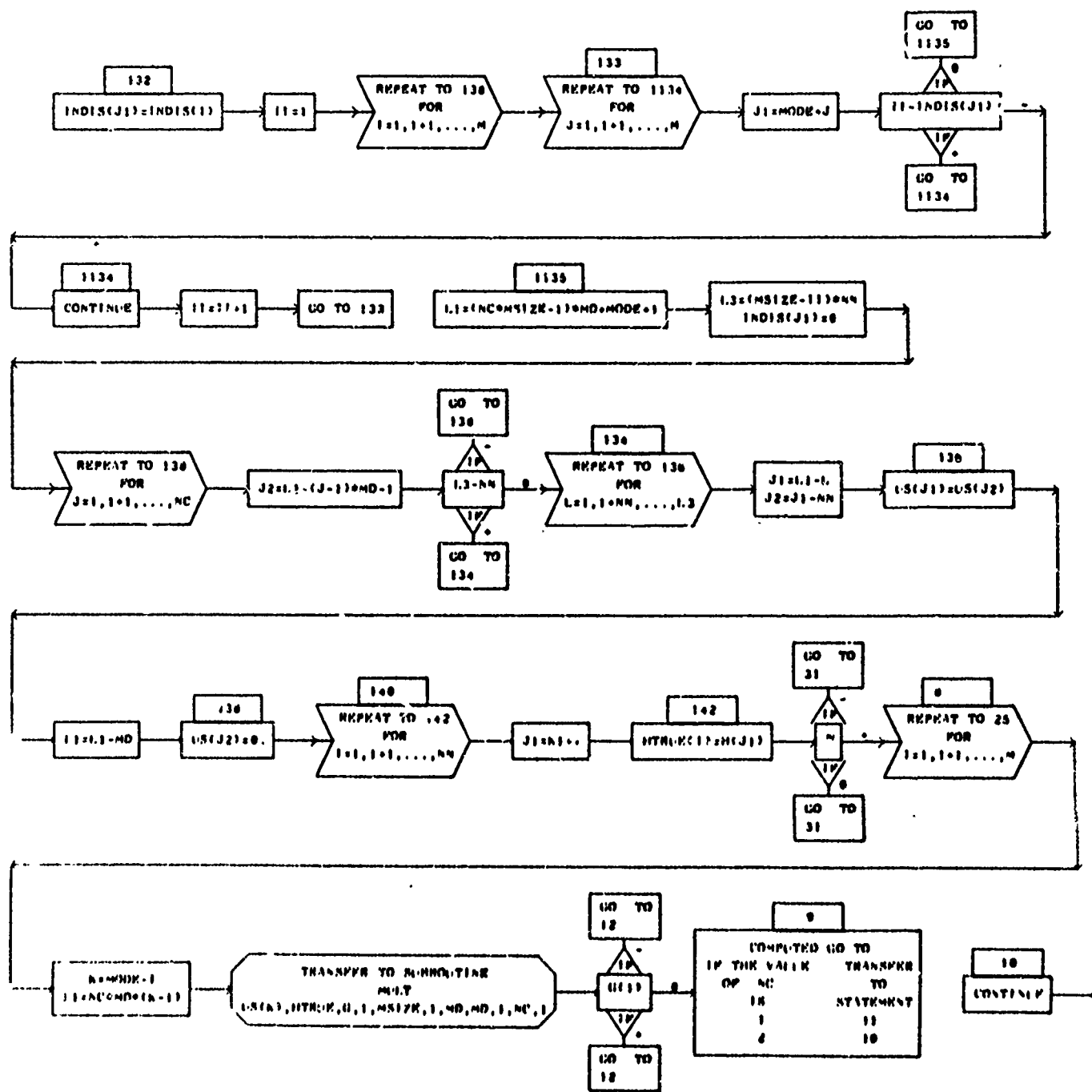
= 2 IF PROBLEM IS COMPLEX.

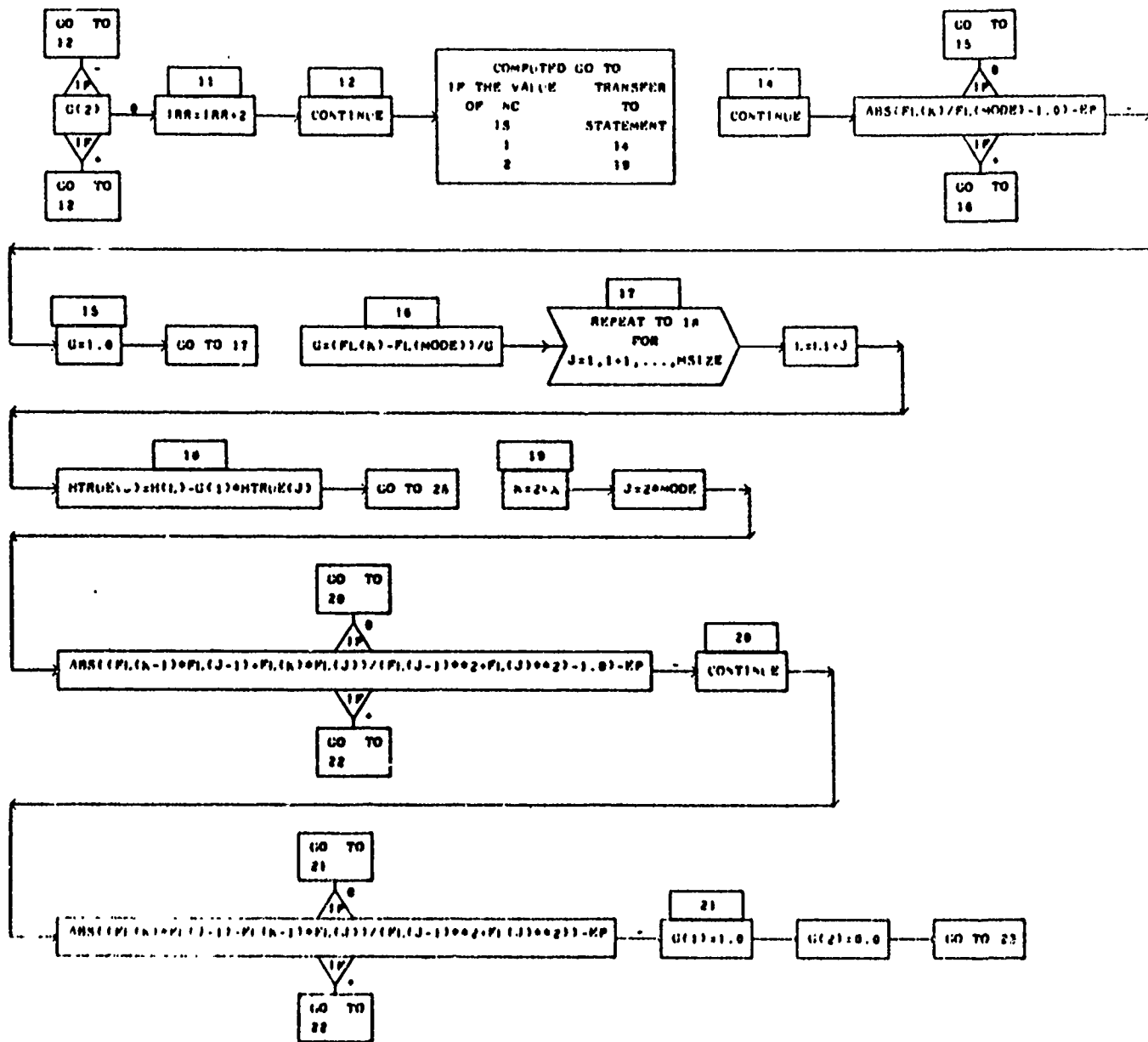
DIMENSIONED VARIABLES

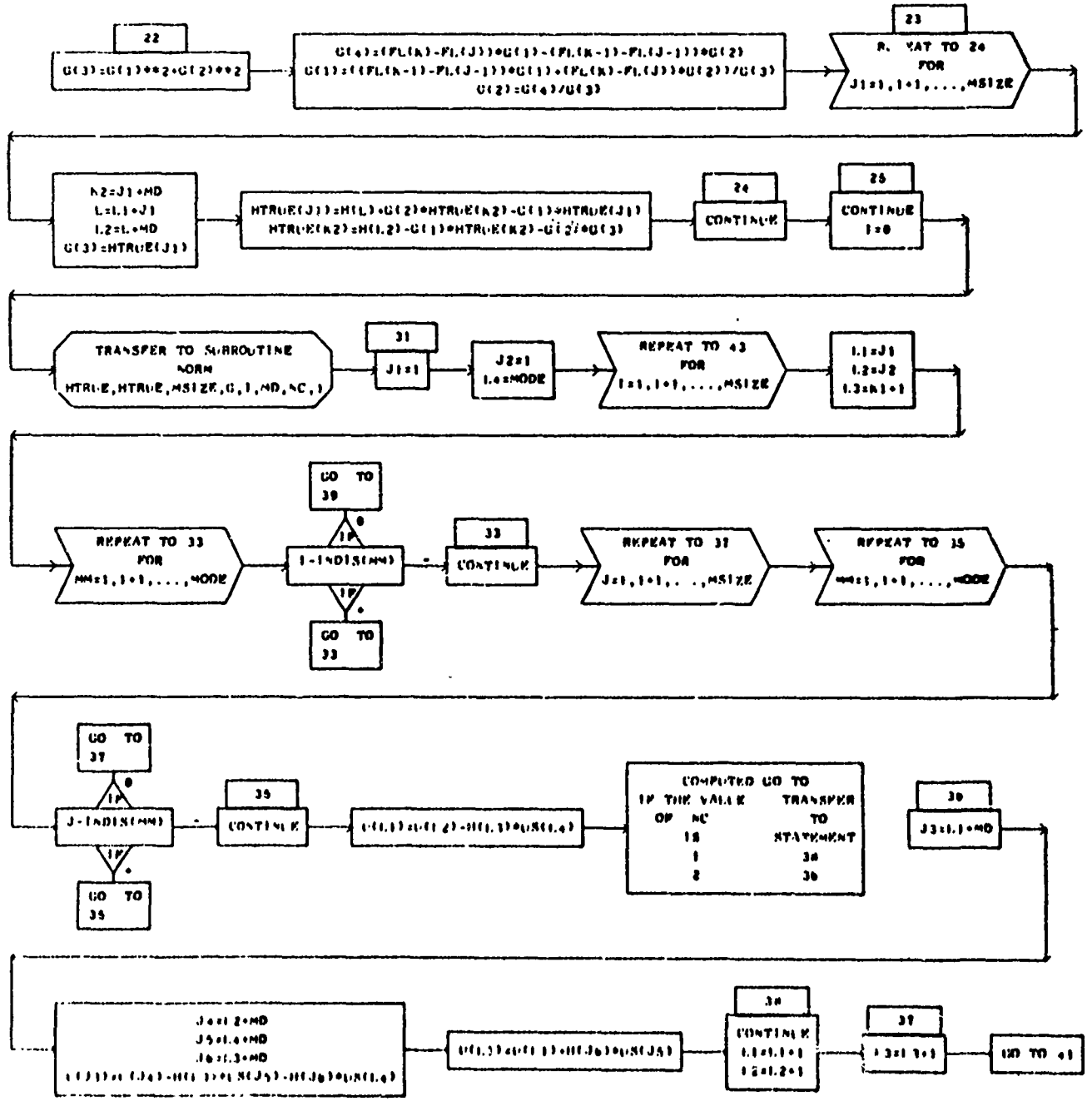
SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE
H	1	US	1	U	1	HTRUE	1	P	1
G	4	INDIS	1						

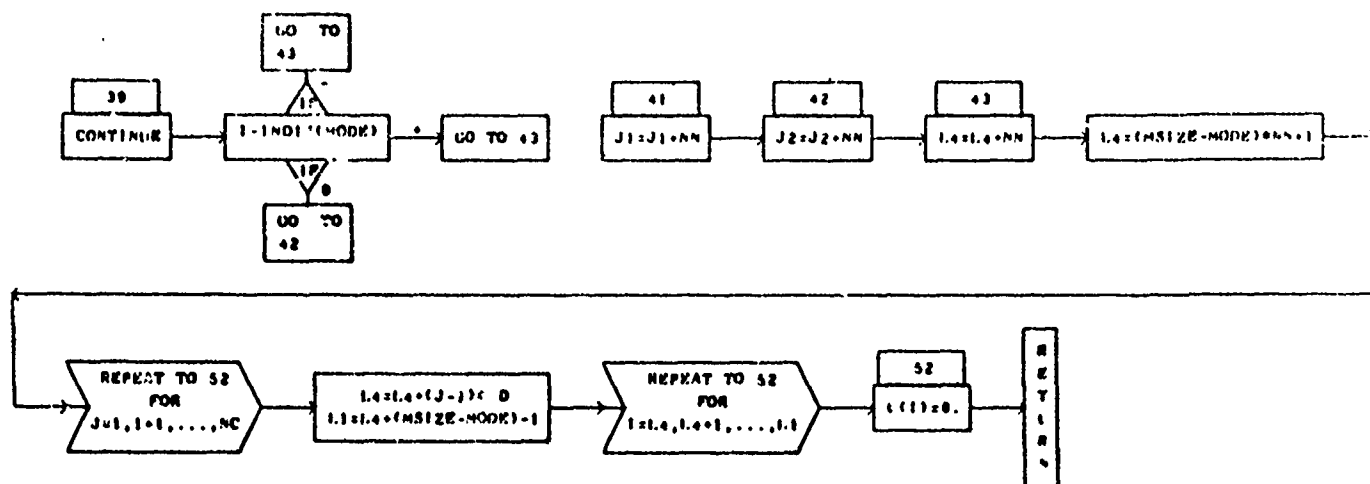












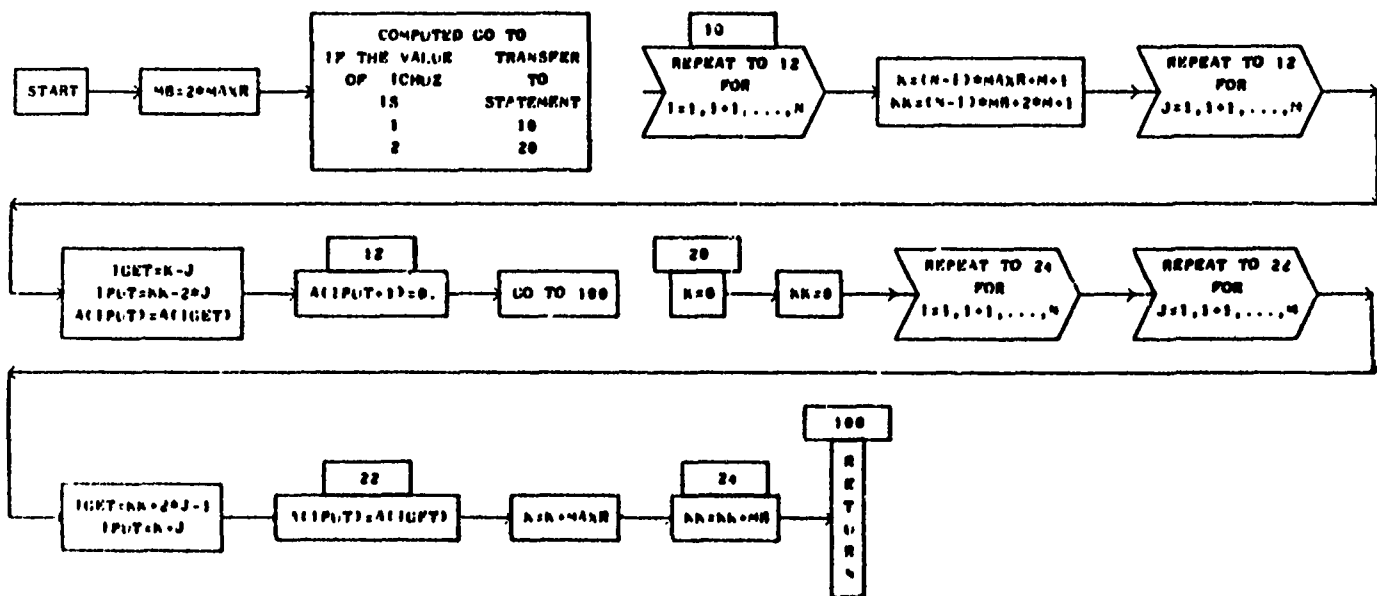
CHANGES

DIMENSIONED VARIABLES

SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE	SYMBOL	STORAGE
4	1								

SUBROUTINE CHANGE (A, M, N, MAXR, ICHU2)

PAGE 1



S E C T I O N 10
N O M E N C L A T U R E

N O M E N C L A T U R E

a	Element of flexibility matrix, in./lb
a_R	Generalized amplitude coefficient of rigid-body modal series, in. or rad
b_r	Reference semichord, ft
C_h	Element of oscillatory aerodynamic influence coefficient matrix, dimensionless
F	Control point force, lb
ζ	Structural damping coefficient, dimensionless
h_o	Control point deflection due to rigid-body motion, in.
h_R	Element in rigid-body modal matrix, in. or dimensionless (see Section II)
h_l	Control point deflection, in.
K	Flexibility matrix normalizing constant, dimensionless
k_r	Reference reduced frequency, dimensionless
M	Element of mass matrix, lb.
\bar{M}	Element of complex mass matrix (includes aerodynamic effects), lb
m	Element of generalized mass matrix, lb., in.-lb, or lb-in ² .
\bar{m}	Element of sum of generalized mass and aerodynamic matrices, lb, in.-lb, or lb-in ² .
Q	Element of generalized aerodynamic force matrix, lb, in.-lb, or lb-in ² .
R	Number of rigid-body modes
s	Reference semispan, ft (i.e., span measured from root to tip)
U	Element of dynamic matrix, in.
V	Velocity, knots
W	Element of aerodynamic weighting matrix, dimensionless

SYMBOLS (continued)

λ Eigenvalue, $\lambda = \lambda_R + i\lambda_I$, in.

ρ Atmospheric density, slugs/ft³

f Frequency, cps

Matrix Notation

[] Square

{ } Column

[]^T Transposed

[I] Unit

UNCLASSIFIED

Security Classification

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11. SUPPLEMENTARY NOTES	12. SPONSORING MILITARY ACTIVITY NAVAL AIR SYSTEMS COMMANDS DEPARTMENT OF THE NAVY WASHINGTON, D.C.	
13. ABSTRACT THIS STUDY COVERS THE DEVELOPMENT OF A SET OF COMPUTER PROGRAM TO PERFORM FLUTTER ANALYSIS BY THE COLLOCATION METHOD. WHILE THIS METHOD HAS BEEN KNOWN FOR SOME TIME, ONLY RECENTLY HAVE ADVANCES IN COMPUTER TECHNOLOGY MADE THE METHOD TECHNICALLY AND FINANCIALLY FEASIBLE. THE INGREDIENTS OF A COLLOCATION FLUTTER ANALYSIS ARE 1) A FLEXIBILITY MATRIX, 2) AERODYNAMIC INFLUENCE COEFFICIENT MATRIX, AND 3) AN EIGENVALUE SOLUTION. THIS STUDY IS PRESENTED IN FOUR VOLUMES. VOLUME I CONTAINS A GENERAL PROGRAM DISCUSSION. VOLUME II CONTAINS THE PROGRAM FLUENC WHICH CALCULATES THE FLEXIBILITY MATRIX. VOLUME III CONTAINS A SET OF THREE PROGRAMS TO CALCULATE AERODYNAMIC INFLUENCE COEFFICIENTS FOR SUBSONIC, TRANSONIC, AND SUPERSONIC FLIGHT REGIMES. VOLUME IV CONTAINS THE PROGRAM COFA WHICH SETS UP AND SOLVES THE FLUTTER EIGENVALUE MATRIX.		

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